

# TECHNICAL NOTES

NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS.

No. 99.

NOTES ON THE STANDARD ATMOSPHERE.

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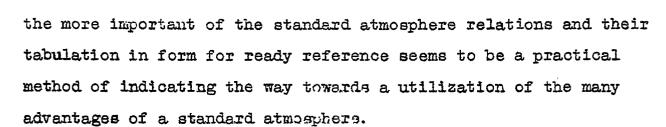
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#### Summary.

This report contains the derivation of a series of relations between temperature, pressure, density and altitude in a "stand-ard atmosphere" which assumes a uniform decrease of temperature with altitude. The equations are collected and given with proper constants in both metric and English units for the temperature gradient adopted by the National Advisory Committee for Aeronautics. A table of values of temperature pressure and density at various altitudes in this standard atmosphere is included in the report.

## Introduction.

Certain interesting and significant relations exist between pressure, density, temperature, and altitude in a "standard atmosphere" which assumes a linear decrease of temperature with altitude. Such an atmosphere is in extensive use in Europe and ha recently been adopted by the National Advisory Committee for Aero nautics for Official use in the United States. The derivation of



The nomenclature followed throughout this report is standard, i.e.:

p = pressure,

 $\rho = \text{mass-density},$ 

T = temperature, absolute,

R = gas constant for air,

a = temperature gradient,

y = altitude.

### Standard Atmosphere.

A discussion of Standard Atmosphere may be found in National Advisory Committee for Aeronautics Report No. 147, by W. R. Gregg. A few brief remarks will be made for the benefit of those who do do not have a copy of that report available for reference.

"Standard Atmosphere," as the name implies, is an atmosphere in which fixed values of pressure, temperature and density are adopted, more or less arbitrarily, for each altitude. Such an atmosphere is required in comparing the performance of aircraft and aircraft power plants. The most satisfactory of all proposed standards is that based on the so-called "Toussaint's Rule," which assumes the air temperature to decrease uniformly with alt.



tude from  $15^{\circ}$ C at sea level to  $-50^{\circ}$ C at 10,000 meters, or, expressed in symbols

where a has the value of .0055 in the metric system (T in  $^{\circ}$ C, y in meters) and the value .003567 in the English system (T in  $^{\circ}$ F, y in feet); and  $^{\circ}$ To is the temperature at sea-level, i.e.:  $273 + 15 = 288^{\circ}$ C (or,  $418.6^{\circ}$ F).

While it is desirable that a standard atmosphere be a close approximation to actual conditions, this requirement should not be stressed. The chief purpose of a standard atmosphere is to supply a basis for comparison of performance and not to specify the temperature and pressure obtaining at a given absolute altitude at all times. It so happens that "Toussaint's Rule" expresses with considerable accuracy the average annual conditions for latitude  $40^{\circ}$  in the United States. This is not altogether accidental since the temperature gradient is based on averages, but it is very doubtful if the standard atmosphere ever expresses the true conditions at a given instant. Nevertheless, the "standard atmosphere" when properly understood and used is of great value in aeronautics.

Table 2, taken from National Advisory Committee for Aeronautics Report No. 147, gives values of t,  $\left(\frac{T}{T_0}\right)$ ,  $\left(\frac{p}{p_0}\right)$   $\left(\frac{\rho}{\rho_0}\right)$  for a series of values of y in both the metric and the English units. It should be noted that the standard air density used in the United States and England is based on a temperature of  $60^{\circ}F$ 



instead of 59°F. This introduces a slight density difference which may lead to confusion in certain cases unless the proper value be used. The difference is negligible in engineering calculations, however.

#### Fundamental Relations.

Since for all practical purposes air may be considered as a "perfect gas," the fundamental relations are the assumed

$$T = T_0 - ay \qquad (1)$$

the perfect gas law

$$p = p + r + \dots + r + q = q$$

or,

$$\left(\frac{p}{p_0}\right) = \left(\frac{\rho}{\rho}\right) \left(\frac{T}{T_0}\right) \dots \left(\frac{2a}{T_0}\right)$$

and

From these three relations there may be derived a series of equations which are of great value to the engineer. The derivation of equations (4) to (8) are original, although equations similar to (4) and (5) were derived by pistolesi in "Bollettino Tecnicio N.18) of the Italian Air Service, and an equation somewhat similar to (7) appears in R & M 324 of the Pritish Advisory Committee for Aeronautics.

Since the preparation of these notes, articles containing similar equations have appeared in the "Bulletin Technique" (Service Technique de l'Aeronautique) No. 4, March, 1922, and in the Aeronautical Journal for May, 1922.

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### Derived Relations.

(a) Between temperature and pressure.

Dividing (2) by (3) and substituting ( $T_0$  - ay) for T

$$\frac{dp}{p} = -\frac{g \, dy}{RT} = -\frac{g \, dy}{R(T_O - ay)}$$

Integrating

$$\frac{aR}{g} \log \left(\frac{p}{p_0}\right) = \log \left(\frac{T}{T_0}\right)$$

and

$$\left(\frac{T}{T_O}\right) = \left(\frac{p}{p_O}\right)^{\frac{aR}{g}}$$
 ....(4)

The value of the exponent is obviously independent of the system of units. In the English system a = .003567 and R = 53.34g or 1716.3. Therefore

$$\frac{aR}{g} = 0.190$$

and

$$\left(\frac{\mathbf{p}}{\mathbf{p}_{0}}\right) = \left(\frac{\mathbf{T}}{\mathbf{T}_{0}}\right)^{5 \cdot 255} \qquad (4b)$$

(b) Between density and pressure:

From (2a) and (4a)

$$\left(\frac{p}{p_0}\right)^{0.81}$$
 ....... (5a)

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$$\left(\frac{p}{p_0}\right) = \left(\frac{\rho}{\rho_0}\right)^{1/235} = \cdots$$
 (5b)

(c) Between temperature and density:

From (4) and (5)

$$\left(\frac{T}{T_0}\right) = \left(\frac{\rho}{\rho_0}\right)^{4 \cdot abs}$$
 (6a)

or

$$\left(\frac{\rho}{\rho_0}\right) = \left(\frac{T}{T_0}\right)^{4\cdot 255} \qquad (6b)$$

(d) Between density and altitude:

From (1) and (6)

$$\left(\frac{\rho}{\rho}\right)^{0.235} = \left(1 - \frac{a}{T_0} y\right) \dots (7a)$$

$$\left(\frac{\rho}{\rho_0}\right) = \left(1 - \frac{a}{T_0}y\right)^{4\cdot 255} \dots \dots (7b)$$

(e) Between pressure and altitude:

From (1) and (4)

$$\left(\frac{p}{p_0}\right)^{\frac{aR}{g}} = \left(1 - \frac{a}{T_0} y\right) \dots (8)$$

$$\left(\frac{p}{p_0}\right)^{0.19} = \left(1 - \frac{a}{T_0}y\right) \dots$$
 (8a)

or

$$\left(\frac{p}{p_0}\right) = \left(1 - \frac{a}{T_0} y\right)^{5-255} \cdots \cdots (8b)$$

A modified form of the well-known Halley's equation which is frequently used, is included for convenience:

$$y = 2.3026 \text{ H} \left(\frac{T + T_0}{2 \cdot T_0}\right) \log_{10} \left(\frac{p_0}{p}\right) \dots$$
 (9)

In this equation H is the height of the "homogeneous atmosphere," i.e., the height to which the atmosphere would have to extend if its density were uniform throughout and of the value required to produce standard pressure at sea-level. This height is 7991 meters, or 26,217 feet.

TABLE 1.

### Collected Formulae and Constants.

	: General Equations and Constants.	: Motric System	:* English System :
******	p <sub>o</sub>	76C nm: (103Z3 lg/m²)	:29.921 in.kg.(2116 1bs/ft <sup>2</sup> )
	ρ	.00125	.00237
	Gravity - g	: 980 6 cm/sec <sup>2</sup>	: 32.172 ft/sec <sup>2</sup>
	T	280 <sup>1</sup> c 0065	418.6°F 003567
	. R	29.27 g	53.34 g
1	: $T = T_0 - ay$	$T = T_00065 y$	: $T = T_0003567y$
2.		$p = \rho RT$	P = PRT
3.	•	$dp = -g \rho dy$	: - : dp = - g ρdy
4.	$\left(\frac{\underline{T}}{\underline{T}_{o}}\right) = \left(\frac{\underline{p}}{\underline{p}_{o}}\right)^{\underline{\underline{e}}\underline{R}}$	$\left(\frac{T}{T_0}\right) = \left(\frac{p}{p_0}\right)^{0.19}$	$\left(\frac{\mathbf{T}}{\mathbf{T}_{0}}\right) = \left(\frac{\mathbf{p}}{\mathbf{p}_{0}}\right)^{0 \cdot 19}$
	$\left(\frac{p}{p_0}\right) = \left(\frac{T}{T_0}\right)^{\frac{g}{aR}}$	$\left(\frac{p}{p_0}\right) = \left(\frac{T}{T_0}\right)^{5 \cdot 25}$	$\left(\frac{p}{p_0}\right) = \left(\frac{T}{T_0}\right)^{5 \cdot 25}$
5.	$\left(\frac{\rho}{\rho_{o}}\right) = \left(\frac{p}{p_{o}}\right)^{1 - \frac{aR}{g}}$	$\left(\frac{\rho}{\rho_{o}}\right) = \left(\frac{p}{p_{o}}\right)^{o \cdot s_{1}}$	$\left(\frac{\rho}{\rho_0}\right) = \left(\frac{p}{p_0}\right)^{c \cdot s_1}$
:	$\left(\frac{p}{p_o}\right) = \left(\frac{\rho}{\rho_o}\right)^{\frac{g}{g-aR}}$	$\left(\frac{p}{p_o}\right) = \left(\frac{\rho}{\rho_o}\right)^{2-235}$	$\left(\frac{p}{p_o}\right) = \left(\frac{\rho}{\rho_o}\right)^{1.235}$
6.	$\left(\frac{T}{T_0}\right) = \left(\frac{\hat{\rho}}{\rho_0}\right)^{\frac{aR}{g-aR}}$	$\left(\frac{T}{T_0}\right) = \left(\frac{\rho}{\rho_0}\right)^{0.235}$	$\left(\frac{T}{T_0}\right) = \left(\frac{\rho}{\rho_0}\right)^{0.235}$
•	$\left(\frac{\rho}{\rho}\right) = \left(\frac{\mathbf{T}}{\mathbf{T}_{0}}\right)^{\frac{\mathbf{g}-\mathbf{a}\mathbf{R}}{\mathbf{a}\mathbf{R}}}$	$\left(\frac{\rho}{\rho_o}\right) = \left(\frac{T}{T_o}\right)^{4 \cdot 255}$	$\left(\frac{\rho}{\rho_0}\right) = \left(\frac{T}{T_0}\right)^{4\cdot 255}$
7.	$\left(\frac{\rho}{\rho_o}\right)^{\frac{aR}{g-aR}}\left(1-\frac{a}{T_o}y\right)$	$\left(\frac{\rho}{\rho}\right)^{0.235} = (100002257y)$	$\left(\frac{\rho}{\rho_0}\right)^{0.235} = (10000068787)$
			$\left(\frac{\rho}{\rho}\right) = (1000006878y)^{4 \cdot 255}$
:	g	$\left(\frac{p}{p_0}\right)^{0.19} = (100002257y)$	· ·
	•	$\left(\frac{p}{p_0}\right) = (100002257y)^{5 \cdot 255}$	. [
٧.	$y = 2.3026 \text{ H} \left(\frac{\text{T+T}_0}{2\text{T}_0}\right)$	$y = 18400 \left( \frac{T_{1}T_{0}}{2T_{0}} \right) \log_{10} \left( \frac{P_{0}}{P} \right)$	$\sum_{\mathbf{y} \in 60370} \left( \frac{\mathbf{T} + \mathbf{T}_0}{\mathbf{Z} \mathbf{T}_0} \right) \log_{\mathbf{T}_0} \left( \frac{\mathbf{p}_0}{\mathbf{p}} \right)$
:	$\log_{10}\left(\frac{p_0}{p}\right)$	e de la companya de l	** * * * * * * * * * * * * * * * * * *

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TABLE 2.

Air Dry Metric					Sta	Standard Atmosphere.			Gra						
					<del></del>				<del></del>	English					
y meters	;	°C	:	$\left(\frac{T_{0}}{T_{0}}\right)$	:	$\left(\frac{\mathbf{p}}{\mathbf{p_0}}\right)$	$\left(\frac{\rho}{\rho_{o}}\right)$	::	y feet	:	o <sub>F</sub> :	$\left(\frac{T}{T_{o}}\right)$	$\binom{2}{p_0}$	:	$\left(\frac{\rho}{\rho_{o}}\right)$
0	:	15.0	•	1.000	:	1.000:	1.000	::	0	:	59.0 :	1.000	1.000	:	1.000
500	:	11.7	:	-989	:	.940	.951	::	2000	:	51.9	.986	.928	:	.943
1000	:	8.5	:	.977	:	.886	.908	::	4000	:	44.7	.972	.862	:	.888
1500	:	5.2	:	.966	:	.834	.865	::	6000	:	37.6	.959	.800	:	.837
2000	:	2.0	:	.955	:	. 784	. 823	::	8000	:	30.5	.945	.741	:	.786
2500	:	-1.2	:	.944	:	.737	.781	::	10000	:	23.5	.931	.686	:	<b>.7</b> 38
3000	:	-4.5	:	.932	:	.692	. 741		12000	:	16.2	.917	.635	:	. 693
3500	:	-7.7	:	.921	:	649	.706		14000	:	9.1	.904	.587	:	. 649
4000	:	-11.0	:	.910	:	.608	. 669	::	16000	:	1.9	.890	.542	:	.608
4500	:	-14.2	:	.898	:	.569	.635		18000	:	-5.2	.876	.498	:	.569
5000	:	-17.5	:	.887	:	.533	.600	::	20000	:	-12.3	-862	.459	:	.531
6000	:	-24.0	:	.865	:	.466	. 539	:;	22000	:	-19.5	.849	.421	:	.496
7000	:	-30.5	:	.842	:	.405	.479		24000	:	-26.6	.835	: .386	:	.463
8000	:	-37.0	:	.819	:	.351	<b>4</b> 29	::	26000	:	-33.7	.821	.353	:	.432
9000	:	-43.5	:	.797	:	.303	381	::	28000	:	-40.9	.807	324	:	.402
10000	:	-50.0	:	.774	:	.262	.337	;;	30000	:	-48.0	.794	297	:	.374
$\left(\frac{T}{T_0}\right) = (100002257y)$					::	$ \frac{T}{T_0} = (1000006878y) $									
T <sub>o</sub> = 288°C						::	T <sub>o</sub>	r <sub>o</sub> = 418.6°F							
$p_0 = 76 \text{ cm. Hg. g } \rho_0 = 1.225 \text{ kg/m}^3$							::						Po		
· -						::	: ,						lbs/f.		