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TECHNICAL NOTES

NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

No. 920

BEARING STRENGTHS OF BARE AND ALCLAD XA75S-T

AND 24S-T81 ALUMINUM ALLOY SHEET

By R. L. Moore and C. Wescoat Aluminum Company of America

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Washington December 1943



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INTRODUCTION

A report was recently issued covering an investigation of the bearing properties of the wrought aluminum alloys commonly used in aircraft construction (reference 1). Since this work was undertaken, two new materials, XA75S-T and 24S-T81, have been developed to the commercial stage for aircraft use. The object of this investigation was to determine the bearing yield and ultimate strengths of these new materials in the form of bare and alclad sheet.

PROCEDURE AND MATERIAL

The test procedure used in these determinations was the same as that previously described (reference 1). Figure 1 is a photograph of the test setup. Briefly, the tests involved loading single thicknesses of 0.064—inch sheet, 2-inches wide and cut parallel to the direction of rolling, in bearing on a 0.250—inch—diameter steel pin. The proportions of specimens used were the same as found to be satisfactory in previous tests. Measurements of the hole elongation were made with a filar micrometer microscope. Tests were made in triplicate for edge distances of 1.5.2, and 4 times the pin diameter.

The material used for these tests was nominally 0.064-inch sheet. The 245-T81 samples were commercial 245-T sheet which had been artificially aged 12 hours at 375°F.

Tensile properties for the material are shown in table I. The values given may, with one exception, be classed as typical. The exception was the Alclad 245-T81, for which the tensile strength was about 1 percent lower than the tentative minimum value. This difference was

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not considered sufficient, however, to affect the ratios of bearing to tensile properties determined.

RESULTS AND DISCUSSION

Individual bearing test results are shown in table
II. The bearing yield strength values were obtained from
the bearing stress—hole elongation curves shown in figures
2 to 5, using an offset from the initial straight—line
portion of the curves equal to 2 percent of the pin diam—
eter (0.005 in.). Indicated also in table II are the
types of failure obtained. Failures by the tearing out
of a portion of the sheet above the pin were predominate
for edge distances of 1.5 and 2 pin diameters, and by up—
setting or crushing the metal above the pin for edge dis—
tances of 4 diameters.

Ratios of average bearing to tensilo proporties are shown in table III. The ratios for both forms of 24S-T81 are in generally good agreement with those obtained for 24S-T and the other high strength aluminum alloys in previous tests (reference 1). Although the ratios for the XA75S-T are slightly higher in most cases than for the 24S-T81, it seems advisable and not unduly conservative to place XA75S-T in the same class as 24S-T81 and the other high strength alloys, as far as ratios of bearing to tensile properties are concerned. The following ratios are proposed as typical for these newer materials.

	Fdgo distanco =				
	1.50	2.0D or groator			
Bearing strongth Tonsilo strongth	1.5	1.9			
Boaring yield strength Tensile vield strength	1.4	1.6			

In the report previously referred to these ratios are identical to those suggested for the other high strength aluminum alleys. Although bearing yield and

ultimate stfengths do not show marked directional characteristics, it should be emphasized, as before, that the ratios given are based on tests parallel to the direction of rolling and should be applied only to tensile properties for this direction. This distinction is, of course, not necessary in the case of the 24S-T81 because this alloy does not exhibit directional characteristics in either bearing or tension.

CONCLUSIONS

The results of this investigation of the bearing properties of bare and alclad XA75S-T and 24S-T81 sheet seem to warrant the following conclusions:

- l. The bearing strength data obtained in this investigation are representative of materials falling within the tentative specified limits for commercial production. Table I gives a summary of tensile properties and table II gives the results of the bearing tests.
- 2. Average ratios of bearing to tensile strengths and bearing yield to tensile yield strengths are given in table III for tests parallel to the direction of rolling. The ratios observed for the two forms of 24S-T81 are essentially the same as previously reported for 24S-T and the other high strength aluminum alloys. The ratios for the XA75S-T are slightly higher in most cases than for the 24S-T81, although, until more data are available, it is believed that the same ratios of bearing strengths to tensile strengths should be used.
- The following ratios of bearing to tensile properties are proposed as typical for bare and alclad XA75S-T and 24S-T81 sheet. Although bearing yield and ultimate strengths do not show marked directional characteristics, it should be emphasized that when directional properties exist in tension, the ratios given apply only to the with-grain direction.

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	Edge distance =				
	1.5D	2.0D or greater			
Bearing strength Tensile strength	1,5	1.9			
Bearing yield strength Tensile yield strength	1,4	1.6			

Aluminum Research Laboratories,
Aluminum Company of America,
New Kensington, Pa., August 11, 1943.

REFERENCES

- 1. Moore, R. L., and Wescoat, C.: Bearing Strengths of Some Wrought-Aluminum Alloys. T.N. No. 901, NACA, Aug. 1943.
- 2. Anon: Tentative Methods of Tension Testing of Metallic Materials (E8-42), 1942 Book of A.S.T.M. Standards, Part I.

TABLE-I. - TENSILE PROPERTIES OF XA75S-T AND 24S-T81

SHEET USED FOR BEARING TESTS

[Nominal thickness, 0.064 in.]

Alloy, and temper	Sample number	Ultimate strength (lb/sq in.)	Yield strength (offset = 0.2 percent) (lb/sq in.)	Elongation in 2 in. (percent)
XA75S-T Alclad XA75S-T ⁱ 24S-T81 Alclad 24S-T81 ¹	52618 52611 59381 39225	72,500 72,200 72,200 63,500	63,800 62,100 65,100 57,900	14.0 13.0 6.5 7.0

Note: The above values are results of single tests in withgrain direction. Type of specimen shown in fig. 2 of reference 2. ¹5 percent alclad coating on each side.

TABLE III .- AVERAGE RATIOS OF BEARING TO TENSILE STRENGTH

FOR XA75S-T AND 24S-T81 SHEET

Alloy and temper	Edge distance = 1.5 x pin diam.			Edge distance = 2 x pin diam.			Edge distance = 4 x rin dism.		
	BS TS	BYS TS	EEYS TYS	BS TS	BYS TS	ESS TYS		TTS	ers Tys
XA75S-T Alclad XA75S-T 24S-T81 Alclad 24S-T81	1.45	1.22	1.51 1.42 1.42 1.46	·2.08	1.50 1.38 1.43 1.46	1.61	2.35	1.50 1.47 1.46 1.51	1.71

Note: All bearing tests on 1/4—in. diam. steel pin (D/t = 4). Specimens 2 in. wide loaded parallel to direction of grain.

BS - bearing strength

BYS - bearing yield strength (offset = 0.02 x pin diam. = 0.005 in.)

TS - tensile strength (with grain)

TYS - tensile yield strength (offset = 0.02 percent) (with grain)

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TABLE II. - BEARING STRENGTES OF XA75S-T AND 24S-T81 SHEET

[Nominal thickness, 0.064 in.]

• ;		Bearing strengths (lb/sq in.)								
Alloy and temper	Test number	Edge dis 1.5 x pin Ultimate	diam.	Type of fathuro ²	Edge di: 2 x pir Ultimate	diam.	Type of failuro ²	Edge dis 4 x pir Ultimate	diam.	Type of failure
X475S-T	1 2 3 4v,	125,600 123,800 125,000 124,800	97,000 96,000 96,000 96,300	S S	162,500 159,400 163,100 161,700	108,000 110,000	S S	178,800 206,300 182,500 189,200	114,500 118,000	B B B
Alclad XA75S-T	3 2 3 Av.	117,500 116,600 116,600 116,900	89,000 87,000 88,000 88,000	S	148,500 151,500 150,300 150,100	101,000	្រ [180,400 165,400 164,100 170,000	106,500 106,500	B B B
24S-T51	1 2 3 av.	106,000 104,600 102,400 104,300	94,000 93,000 91,000 92,700	S S	1\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\	102,000 104,000	S S	186,900 179,000 152,100 172,700	106,500 103,500	B
Alclad 245-T81	3 1 2 3 Av.	97,500 96,800 98,700 97,700	84,000 84,000 85,000 84,500	· S S	132,300 132,300 127,800 130,800	93,000 91,000		146,800 162,700 162,000 157,200	97,500 96,000 94,000 95,800	B B

Note: All tests on 1/4 in. diam. steel pin (D/t = 4). Specimens 2 in. wide loaded parallel to direction of grain.

Stress corresponding to offset of 2 percent of hole diameter from initial straight-line portion of bearing stress-hole elongation curves shown in figs. 2 to 5 (0.005 in. offset for 1/1-in. diam.pin).

Type of failure: B - Bearing, S - shear.

35 percent alclad costing on each side.



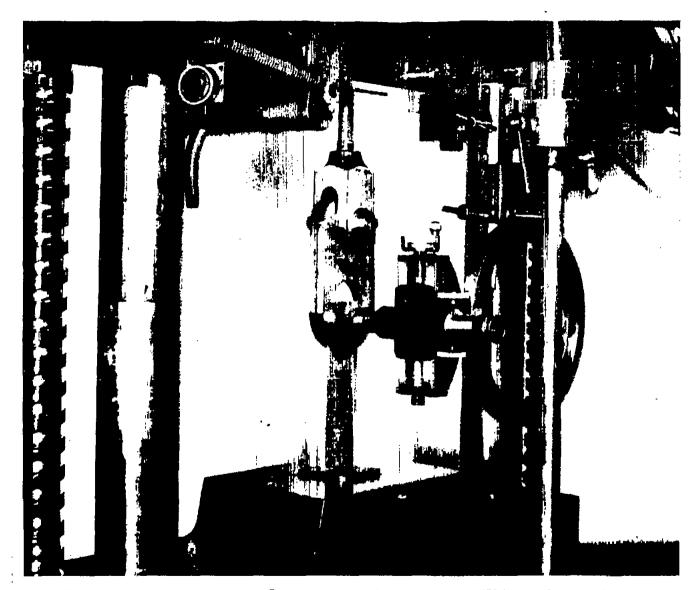
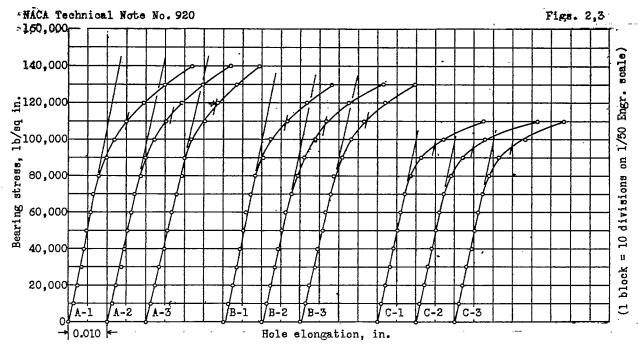
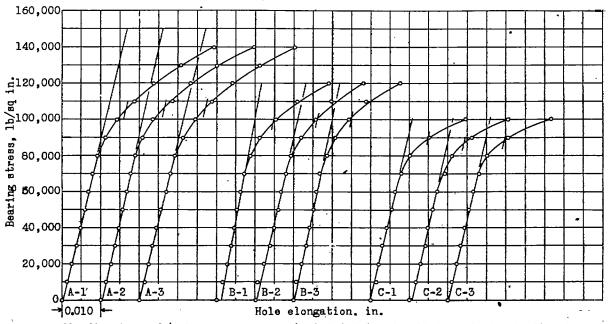


Figure 1.- Arrangement for bearing tests using Filar micrometer microscope for measurements of hole elongation.



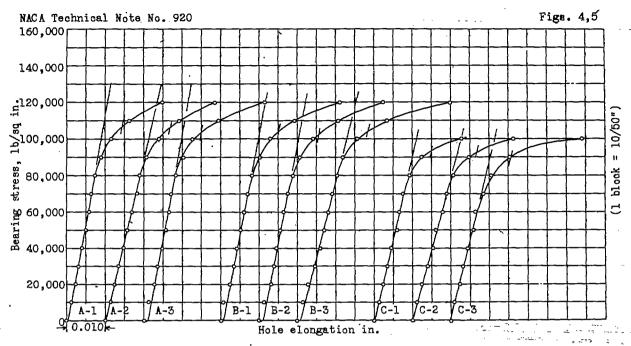
Pin daimeter = 1/4 in. Sheet thickness = 0.064 in. Specimen width = 2 in. A-1,A-2 and A-3: edge distance = $4\times$ pin diameter B-1,B-2 and B-3: edge distance = $2\times$ pin diameter C-1,C-2 and C-3: edge distance = $1.5\times$ pin diameter

Figure 2.- Bearing stress-hole elongation curves for aluminum alloy sheet, bare XA75S-T. Test 12-29.



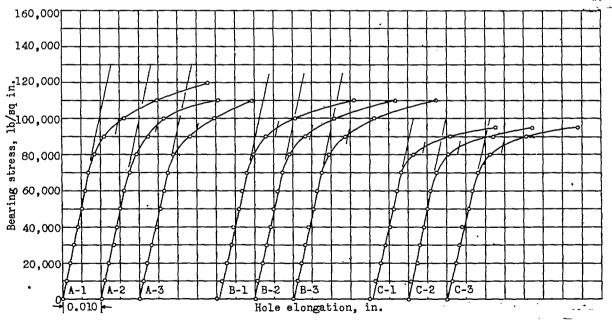
Pin diameter = 1/4 in. Sheet thickness = 0.064 in. Specimen width = 2 in. A-1,A-2,A-3: edge distance = 4× pin diameter B-1,B-2,B-3: edge distance = 2x pin diameter C-1,C-2,C-3: edge distance = 1.5× pin diameter

Figure 3.- Bearing stress-hole elongation curves for aluminum alloy sheet, Alciad IA75S-T. Test 12-29.



Pin diameter = 1/4 in. Sheet thickness = 0.064 in. Specimen width = 2 in. A-1,A-2 and A-3: edge distance = 4x pin diameter B-1,B-2 and B-3: edge distance = 2x pin diameter C-1,C-2 and C-3: edge distance = 1.5x pin diameter

Figure 4.- Bearing stress-hole elongation curves for aluminum alloy sheet, bare 24S-T81. Test 12-29.



Pin diameter = 1/4 in. Sheet thickness = 0.064 in. Specimen width = 2 in. A-1,A-2 and A-3: edge distance = $4\times$ pin diameter B-1,B-2 and B-3: edge distance = $2\times$ pin diameter C-1,C-2,and C-3: edge distance = $1.5\times$ pin diameter

Figure 5.- Bearing stress-hole elongation curves for aluminum alloy sheet, Alclad 24S-T81. Test 12-29.