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Material Qualification and Equivalency for Polymer Matrix Composite Material Systems: Updated Procedure

September 2003

Final Report

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16. Abstract

This document presents an updated qualification plan methodology that will provide the detailed background information and engineering practices to help ensure the control of repeatable base material properties and processes that are applied to both primary and secondary structures for aircraft products using composite materials. This document includes recommendations for the original qualification as well as procedures to statistically establish equivalence to the original data set. The document describes in detail the procedures to generate statistically based design allowables for both A- and B-basis applications. Specific test matrices are presented that produce lamina-level composite material properties for various loading modes and environmental conditions for aircraft applications not exceeding 200°F. This document only covers the initial material qualification at the lamina level and does not include procedures for laminate or higher-level building block tests. The general methodology, however, is applicable to a broader usage.

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ABBREVIATIONS AND ACRONYMS

AC	Advisory Circular
ACO	Aircraft Certification Office
AMS	Aerospace Material Specification
ASTM	American Society for Testing and Materials
CFR	Code of Federal Regulations
CLC	Combined Loading Compression
CPT	Cured Ply Thickness
CTD	Cold Temperature Dry
CV	Coefficient of Variation
DAR	Designated Airworthiness Representative
DER	Designated Engineering Representative
DMA	Dynamic Mechanical Analysis
DMIR	Designated Manufacturing Inspection Representative
DSC	Differential Scanning Calorimetry
ETD	Elevated Temperature Dry
ETW	Elevated Temperature Wet
FAA	Federal Aviation Administration
FAW	Fiber Areal Weight
FV	Fiber Volume fraction
HPLC	High Performance Liquid Chromatography
IR	Infrared spectroscopy
MIDO	Manufacturing Inspection District Office
MNR	Maximum Normed Residual
MOL	Material Operational Limit
NIST	National Institute of Standards and Technology
OEM	Original Equipment Manufacturer
OSL	Observed Significance Level
QA	Quality Assurance
QC	Quality Control
RTD	Room Temperature Dry
RTW	Room Temperature Wet
SACMA	Suppliers of Advanced Composite Materials Association
SAE	Society of Automotive Engineers
T_g	Glass Transition Temperature

EXECUTIVE SUMMARY

This document presents the detailed background information and engineering practices that provides the basis for a qualification methodology to help ensure the control of repeatable base material properties and processes that are applied to both primary and secondary structures for aircraft products using composite materials. This document includes recommendations for the original qualification as well as procedures to statistically establish equivalence to the original data set. The document describes in detail the procedures to generate statistically based design allowables for both A- and B-basis applications. Specific test matrices are presented that produce lamina-level composite material properties for various loading modes and environmental conditions for aircraft applications not exceeding 200°F. This document only covers the initial material qualification at the lamina level and does not include procedures for laminate or higher-level building block tests. The general methodology, however, is applicable to a broader usage.

1. INTRODUCTION.

This document presents the detailed background information and engineering practices that provides the basis for a qualification methodology to help ensure the control of repeatable base composite material properties and processes for use in aircraft products. These engineering procedures apply to the original material qualification and provide a benchmark for subsequent material and process control. Over time, changes to the material, process, tooling, and facility require a review, and it may be required that some (or all) of these tests be repeated.

1.1 SCOPE.

This methodology includes recommendations for an original qualification as well as procedures to statistically establish equivalence to the original data set. This report describes in detail the procedures to generate statistically based design allowables for both A- and B-basis applications. Specific test matrices are presented that produce lamina-level composite material properties for various loading modes and environmental conditions. This document only covers the initial material qualification at the lamina level and does not include procedures for laminate or higher-level building block tests. Specifically, it covers qualification methodology for no-bleed prepreg systems manufactured using vacuum bagging techniques (autoclave or oven cure) only. However, the methodology described is this plan is applicable to broader usage.

1.2 FIELD OF APPLICATION.

The report describes material qualification methodology for epoxy-based carbon or fiberglass preimpregnated materials cured and processed at 240°F or higher. Additionally, it establishes testing methods and process controls necessary to certify composite materials used for airframe components under Title 14 Code of Federal Regulations (CFR) Part 23 requirements. In some cases, unique characteristics of a material system or its application may require testing beyond that described in this document. In these situations, Aircraft Certification Offices (ACOs) may require additional testing to demonstrate compliance to the applicable Federal Aviation Regulations.

1.3 APPLICABLE DOCUMENTS.

- MIL-HDBK-17-1E, 2E, 3E—Military Handbook for Polymer Matrix Composites
- SAE AMS 2980/0-5—Technical Specification: Carbon Fiber Fabric Epoxy Resin Wet Lay-Up Repair
- FAA CFR 14: Aeronautics and Space
- FAA Advisory Circular 20-107A: Composite Aircraft Structures
- FAA Advisory Circular 21-26: Quality Control for the Manufacture of Composite Materials

2. APPLICABLE FEDERAL AVIATION ADMINISTRATION (FAA) REGULATIONS AND RECOMMENDATIONS.

This methodology was developed as a means to show compliance with 14 CFR Part 23 requirements. Specifically, this document provides material qualification methodology to show compliance with the following 14 CFR Part 23 paragraphs.

2.1 APPLICABLE FEDERAL REGULATIONS.

- § 23.601 General

The suitability of each questionable design detail and part having an important bearing on safety in operations must be established by tests.

- § 23.603 Materials and Workmanship

  (a) The suitability and durability of materials used for parts, the failure of which could adversely affect safety, must -

  (1) Be established by experience or tests;

  (2) Meet approved specifications that ensure their having the strength and other properties assumed in the design data;

  and

  (3) Take into account the effects of environmental conditions, such as temperature and humidity, expected in service.

  (b) Workmanship must be of a high standard.

- § 23.605 Fabrication Methods

  (a) The methods of fabrication used must produce consistently sound structures. If a fabrication process (such as gluing, spot welding, or heat-treating) requires close control to reach this objective, the process must be performed under an approved process specification.

  (b) Each new aircraft fabrication method must be substantiated by a test program.

- § 23.613 Material Strength Properties and Design Values

  (a) Material strength properties must be based on enough tests of material meeting specifications to establish design values on a statistical basis.

(b) Design values must be chosen to minimize the probability of structural failure due to material variability. Except as provided in paragraph (e) of this section, compliance with this paragraph must be shown by selecting design values that ensure material strength with the following probability:

(1) Where applied loads are eventually distributed through a single member within an assembly, the failure of which would result in loss of structural integrity of the component; 99 percent probability with 95 percent confidence.

(2) For redundant structure, in which the failure of individual elements would result in applied loads being safely distributed to other load carrying members; 90 percent probability with 95 percent confidence.

(c) The effects of temperature on allowable stresses used for design in an essential component or structure must be considered where thermal effects are significant under normal operating conditions.

(d) The design of the structure must minimize the probability of catastrophic fatigue failure, particularly at points of stress concentration.

(e) Design values greater than the guaranteed minimums required by this section may be used where only guaranteed minimum values are normally allowed if a "premium selection" of the material is made in which a specimen of each individual item is tested before use to determine that the actual strength properties of that particular item will equal or exceed those used in design.

2.2 APPLICABLE ADVISORY CIRCULAR (AC) RECOMMENDATIONS.

The following FAA advisory circulars present recommendations for showing compliance with FAA regulations associated with composite materials. These circulars are considered essential in the certification process for composite aircraft components as well as for establishing quality control provisions for material receiving and manufacturing.

2.2.1 AC 20-107A—Composite Aircraft Structure.

This AC sets forth an acceptable, but not the only, means of showing compliance with the provisions of 14 CFR Parts 23, 25, 27, and 29 regarding airworthiness-type certification requirements for composite aircraft structures, involving fiber-reinforced materials, e.g., carbon (graphite), boron, aramid (Kevlar), and glass-reinforced plastics. Guidance information is also presented on associated quality control and repair aspects.

2.2.2 AC 21-26—Quality Control for the Manufacture of Composite Structures.

This AC provides information and guidance concerning an acceptable means, but not the only means, of demonstrating compliance with the requirements of 14 CFR Part 21, Certification Procedures for Products and Parts, regarding quality control (QC) systems for the manufacture of

composite structures involving fiber-reinforced materials, e.g., carbon (graphite), boron and aramid (Kevlar), and glass-reinforced polymeric materials. This AC also provides guidance regarding the essential features of QC systems for composites as mentioned in AC 20-107A. Consideration will be given to any other method of compliance the applicant elects to present to the FAA.

3. COMPOSITE TEST METHODS AND SPECIMEN GEOMETRY.

This section specifies the composite test procedures, specimen manufacturing procedures, panel size recommendations, environmental conditioning, and specimen geometry to be used in a typical material qualification by referring to existing standards. Drawings for each specimen's geometry are provided with dimensions and tolerances for conformity purposes. Any specific additions or changes to the referenced test standard were also summarized. Although the Society of Automotive Engineers Aerospace Material Specification 2980/0-5 applies to field repair wet lay-up systems, the general format of that qualification program has been adopted for this document.

All specimens shall be fabricated according to the appropriate process specification to the geometry defined in this section and FAA conformity established by an FAA Manufacturing Inspection District Office (MIDO) employee. The FAA may delegate this to a Designated Airworthiness Representative (DAR) or a Designated Manufacturing Inspection Representative (DMIR). For the purposes of material properties qualification, each of the following paragraphs serves as the engineering definition of the specimen in the same way as would a drawing.

3.1 SPECIMEN MANUFACTURING.

This section describes recommendations for manufacturing test panels used for the development of design allowables for a specific preimpregnated material system. Whenever possible, the manufacturing methods to produce the test panel should be identical in process to those used on production parts to the greatest extent practical with the following exceptions:

- Caul plates may be used during panel manufacturing to produce desired surface flatness as required by appropriate American Society for Testing and Materials (ASTM) or Suppliers of Advanced Composite Material Association (SACMA) test methods. These caul plates may not be practical on actual part production but may be required to produce test panels of acceptable quality to yield material design properties.

- Peel-ply should not be used for the surface finish for bonding of tabs. It should be noted that the use of peel-ply might have a negative impact on the accuracy of test results. Peel-ply may absorb resin and change cured ply thickness, fiber volume fraction, and void content of the panel. If used, investigation to the effect of peel-ply should be conducted prior to beginning actual qualification testing.

- Each panel manufactured for testing should have a traceable reference edge to be used during specimen preparation. These reference edges should be used throughout the specimen preparation procedure.

Detailed guidelines for manufacturing test panels for qualification testing are given in appendix C.

3.1.1 Number of Specimens.

The number of specimens required for qualification is dependent on the purpose for the material system. If a redundant load path exists within the design, a B-basis number may be used to substantiate the design allowable. If a single load path exists, an A-basis number must be used. The number of specimens for basis allowable generation is dependent on the method of sampling, i.e., robust sampling for A- and B-basis allowables or reduced sampling for B-basis allowables. Robust sampling will generally yield a higher and more stable B-basis allowable.

3.1.2 Panel Sizes.

Recommended panel sizes are given in appendices A and B for robust and reduced sampling design allowables, respectively, for a typical unidirectional tape and fabric weave material system. These panel sizes are recommended to generate subpanels to be used for individual specimens as well as provide enough material for physical and humidity-aged conditioning travelers. These panel sizes also allow for a limited number of extra specimens in case of accidental errors.

3.1.2.1 Robust Sampling Panel Sizes and Quantity Requirement.

Appendix A lists the required panel sizes for each test method as well as the anticipated number of specimens for each batch of material for both unidirectional tape and fabric weave materials. Robust sampling generally requires five unique batches of prepreg material with a total of 11 specimens per batch per loading condition (see section 4.5.1).

3.1.2.2 Reduced Sampling Panel Sizes and Quantity Requirement.

Appendix B lists the required panel sizes for each test method as well as the anticipated number of specimens for each batch of material for both unidirectional tape and fabric weave materials. Reduced sampling generally requires three unique batches of prepreg (see section 4.5.2) with a total of six specimens per batch per loading condition.

3.1.3 Panel Manufacturing.

Each panel manufactured for testing should have a traceable reference edge to be used during subpanel and specimen preparation. Detailed guidelines for producing these reference edges are given in appendix C. The reference edge of the original panel should be maintained until individual specimens are produced.

To include the effect of processing variability within the qualification data, the manufacturing process to produce the test panels should be representative of multiple process cycles. Panels manufactured for each loading condition, test method, and batch of qualification testing should be representative of a minimum of two independent processing cure cycles. For example, the B-basis hot-wet testing for in-plane shear strength is composed of three batches of material with six

replicates from each batch. The replicates within these tests should be traceable to a minimum of two independent processing cycles. Figures 1 and 2 describe a typical methodology used for specimen selection as well as panel manufacturing for both robust and reduced sampling design allowables, respectively. This selection process is essential to the statistical analysis used to develop design allowables and to account for prepreg batch and processing variability inherent in the material systems being qualified, which is employed in section 5.3 of this document. Details on the specific number of specimens required for both the robust and reduced sampling may be found in sections 4.5.1 and 4.5.2, respectively.

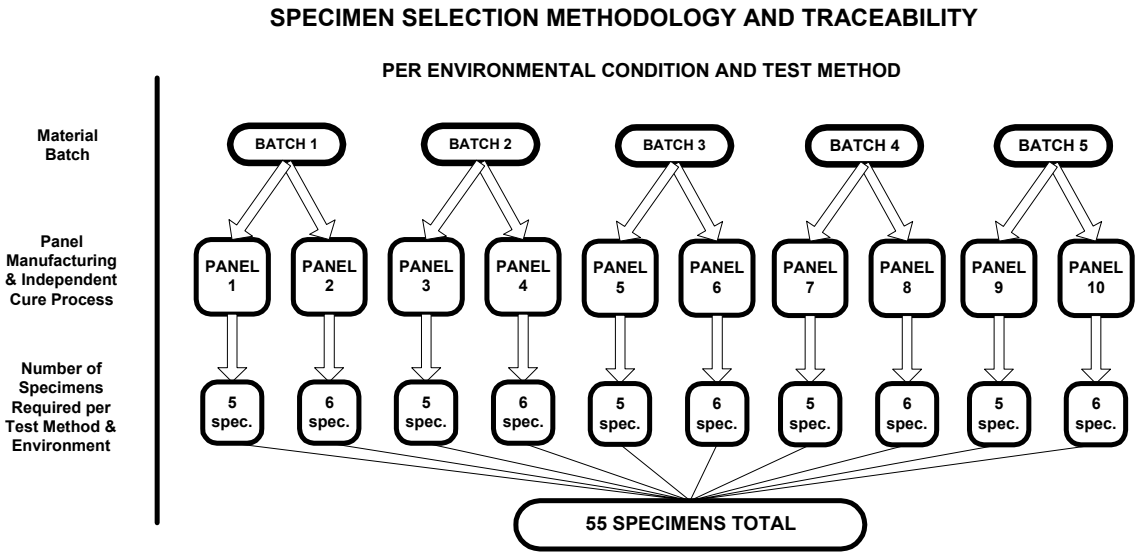


FIGURE 1. ROBUST SAMPLING

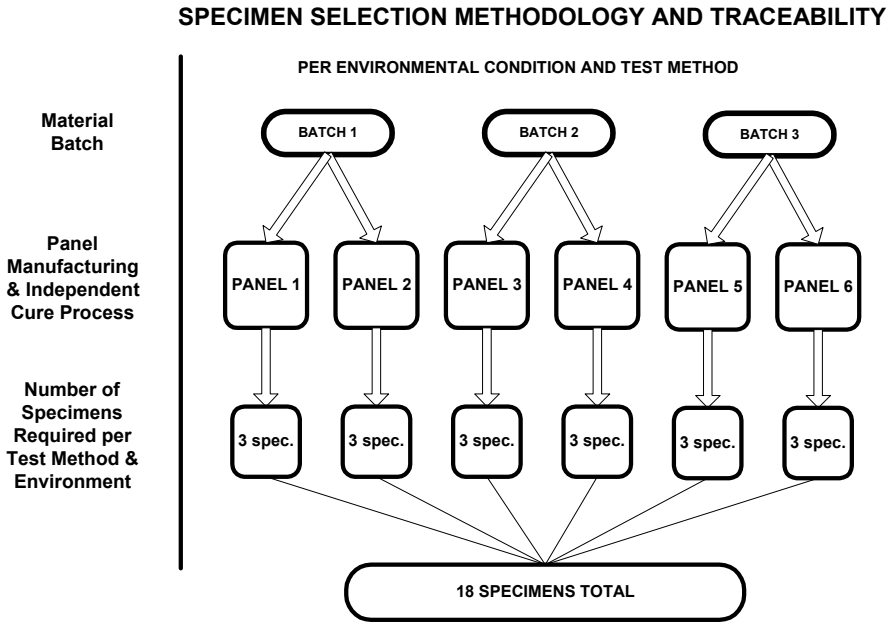


FIGURE 2. REDUCED SAMPLING

3.1.4 Tabs.

Where tabs are added to the specimen for the purpose of introducing loads, they shall be bonded to the specimen using epoxy adhesive that cures at or below the panel cure temperature. If the epoxy adhesive cure temperature is at or near the panel cure temperature, the epoxy adhesive cure time should not be longer than the panel cure time. This is to avoid adding undesirable postcure to the panel. Strain compatible tabbing material should be used, which commonly consists of glass or graphite woven fabric. Strain compatible tabbing material is defined as tabbing material that will yield acceptable specimen failure modes. In some cases, it is necessary to control the adhesive bondline and tab thickness to achieve acceptable specimen failure modes. The subpanel reference edge should be used during the tabbing process to ensure proper tab alignment [1].

3.1.5 Specimen Machining.

Care should be used in cutting the subpanels to maintain fiber orientation with respect to the reference edges as defined in section 3.1.3 and appendix C. To ensure that this is maintained, a subpanel cut should always be based upon the original manufacturing panel reference edge. This can be accomplished by using locator pins or test indicators during cutting. The subpanel reference edge should also be used as a reference for the sectioning of individual specimens. Precautions should be taken to ensure that accumulation of fiber direction error does not exceed 0.25°. This error-accumulation effect is one of the main reasons for small panel sizes (as indicated in appendices A and B).

In general, specimens are sectioned from subpanels using a water-cooled diamond saw, with care taken not to overheat the specimen, which may result in matrix charring. Specimens are then generally surface ground to their final dimensions to achieve desired dimensional tolerances and surface finish.

All dimensional tolerances must be achieved according to the specifications provided in section 3.4 for each test method. In cases where dimensional tolerances are not met, the specimens may be reworked.

3.1.6 Specimen Selection.

For each material or property, batch replicates should be sampled from at least two different test panels covering at least two independent processing cycles, per section 3.1.3. Guidelines for specimen selection from each batch or panel are presented in figures 1 and 2. Specimens taken from each individual panel should be selected randomly. Test specimens should not be extracted from panel areas having indications of questionable quality either visually or as determined from nondestructive inspection techniques.

3.1.7 Specimen Naming.

An individual specimen-naming system should be devised to guarantee traceability to the original subpanel, panel, test method, test condition, batch, and processing cycle. Evidence of traceability should be established by an FAA MIDO representative, DAR, or DMIR. Skewed

lines may be drawn across each subpanel with a permanent marker or paint pen before specimen sectioning to allow subpanel or panel reconstruction after testing, as shown in figure 3. These may be very important when tracking outliers within the material data after testing.

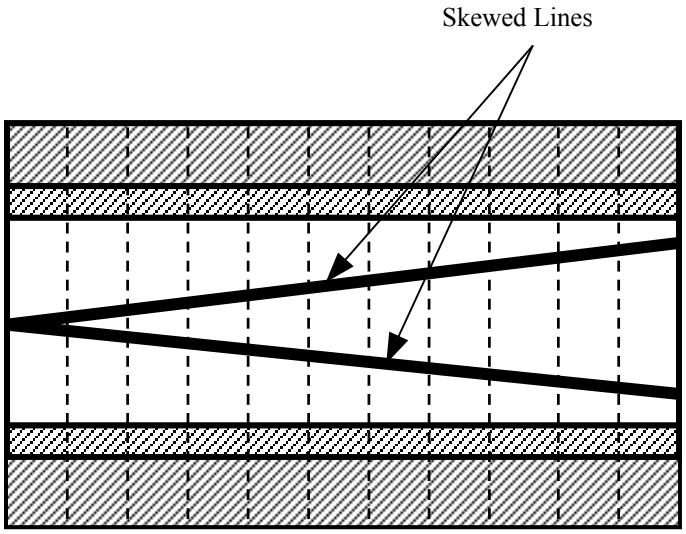


FIGURE 3. SKEWED LINES DRAWN ACROSS SUBPANEL USED FOR RECONSTRUCTION

3.1.8 Strain Gage Bonding.

ASTM E 1237 should be used as a general guide for strain gage installation with the following recommendations specific to composite materials:

- Isopropyl alcohol should be used for any wet abrading or surface cleaning.
- 280- to 600-grit sandpaper should be used for abrading the surface, taking care not to sever or expose any fibers.
- Specimens that are humidity conditioned prior to testing should be gaged after the conditioning has taken place. Humidity-aged specimens may be exposed to ambient conditions for a maximum of 2 hours for application of the gages.
- If soldering lead wiring, care must be taken not to burn the matrix of the test coupon.
- If possible, gage sizes should be selected such that the gage area is greater than three times the repetitive pattern of the weave. This may not be possible with some test methods; however, the gage area must be greater than a single repetitive pattern of the weave.

3.1.9 Specimen Dimensioning and Inspection.

All dimensions to be used in the calculations of mechanical and physical properties should be recorded as specified in figures 9-17. These dimensions must meet the dimensional requirements stated in the appropriate drawing figures. All thickness measurements should be made with point or ball micrometers and all width measurements with calipers. The accuracy of all measuring instruments should be traceable to the National Institute for Standards and Technology (NIST) or the applicable national organization standards of that country. In the case of tabbed specimens, all measurements should be taken after the bonding of tabs and final specimen machining. For humidity-aged specimens, all dimensioning should be recorded prior to the environmental-conditioning process. A minimum of one randomly selected specimen from each subpanel must be inspected for every dimensional requirement stated in the appropriate appendix A figure and for quality of specimen surfaces and tabs. If the randomly selected specimen fails any one of the requirements, every specimen must be inspected for that dimensional requirement. The specimens that do not meet any dimensional requirement must be reinspected after rework has been done. The FAA Form 8130-9 must be used to indicate any deviation to an FAA-approved test plan.

3.2 ENVIRONMENTAL CONDITIONING.

Humidity-aged specimens typically use accelerated conditioning to simulate the long-term exposure to humid air and establish a moisture saturation of the material. Accelerated conditioning of the specimens at 85% ±5% relative humidity and 145° ±5°F will be used until moisture equilibrium is achieved. The environmental-conditioning chamber must be calibrated using standards having traceability to the NIST or which have been derived from acceptable values of natural physical constants or through the use of the ratio method of self-calibration techniques. ASTM D 5229 and SACMA SRM 11 provide general guidelines regarding environmental conditioning and moisture absorption.

Specimens to be tested in the dry, as-fabricated condition should be exposed to ambient laboratory conditions until mechanical testing. Ambient laboratory conditions are defined as 65°-75°F. Since moisture absorption or desorption rate of epoxy is very slow at ambient temperature, there is no requirement to maintain relative humidity levels in the mechanical test laboratory.

3.2.1 Traveler Specimens.

To establish the effect of moisture with respect to the mechanical properties, specimens should be environmentally conditioned, per section 3.2. Since the individual specimens may not be measured to determine the percentage of moisture content (due to size and tab effects), traveler coupons of approximately 1″ by 1″ by specimen thickness should be used to establish the weight gain measurements. Individual traveler specimens should be obtained from the representative panel from which the mechanical test specimens were obtained. One traveler specimen per qualification panel per batch is recommended.

3.2.2 Equilibrium Criteria.

Effective moisture equilibrium is achieved when the average moisture content of the traveler specimen changes by less than 0.05% for two consecutive readings within a span of 7 ±0.5 days and may be expressed by

$$\frac{W_i - W_{i-1}}{W_b} < 0.0005$$

where: W_i = weight at current time
W_{i-1} = weight at previous time
W_b = baseline weight prior to conditioning

If the traveler coupons pass the criteria for two consecutive readings, which are taken 7 ±0.5 days apart, the specimens may be removed from the environmental chamber and placed in a sealed bag along with a moist paper towel for a maximum of 14 days until mechanical testing. Strain-gaged specimens may be removed from the controlled environment for a maximum of 2 hours for application of gages in ambient laboratory conditions, as defined in section 3.2. If the moisture diffusivity constant is needed, the samples shall be dried prior to conditioning.

3.3 NONAMBIENT TESTING.

To quantify the effect of temperature with respect to mechanical properties, increased and decreased temperature testing is required (see section 4.3). This increased and decreased temperature testing is usually done using an environmental testing chamber attached to the load frame.

3.3.1 Temperature Chamber.

The temperature chamber used in the environmental testing should be capable of performing all required tests with an accuracy of ±3°F of the required temperature. The chamber must be calibrated using standards having traceability to the NIST or which have been derived from acceptable values of natural physical constants or through the use of the ratio method of self-calibration techniques. The chamber should be of adequate size so that all test fixtures and load frame grips are contained within the chamber. The chamber should also be capable of a heating rate that can reach the desired test temperature within the times specified in the following sections.

3.3.2 Testing at Elevated Temperatures.

Before beginning the testing, the temperature chamber and test fixture should be preheated to the specified temperature.

Each specimen should be heated to the required test temperature as verified by a thermocouple in direct contact with the specimen gage section. The heat-up time of the specimen shall not exceed 5 minutes. The test should start 2^{+1}_{-0} minutes after the specimen has reached the test

temperature. During the test, the temperature, as measured on the specimen, shall be within ±5°F of the required test temperature.

3.3.3 Testing at Subzero Temperatures.

Each specimen should be cooled to the required test temperature as verified by a thermocouple in direct contact with the specimen gage section. The test should start 5^{+1}_{-0} minutes after the specimen has reached the test temperature. During the test, the temperature, as measured on the specimen, shall be within ±5°F of the required test temperature.

3.4 SPECIMEN GEOMETRY AND TEST METHODS.

3.4.1 General.

The test methods and specimen geometry presented in this section refer to the actual qualification procedures and test methods used to establish design allowables for a given material system. The following publications serve as the basis for this qualification plan. The applicable issue of the standard or recommendation at the time of issuance of the qualification plan should be used. In the event a revision of the testing standard or recommendation occurs during the material qualification, the extent to which it affects this qualification plan should be investigated.

The test methods described are intended to provide basic composite properties essential to most methods of analysis. These properties are considered to provide the initial base of the building block approach. Additional coupon-level and subelement tests may be required with larger structural tests to fully substantiate the full-scale design.

3.4.2 Test Methods.

3.4.2.1 ASTM Standards.

- D 3039-00 Tensile Properties of Polymer Matrix Composite Materials
- D 5379-98 Shear Properties of Composite Materials by the V-Notched Beam Method
- D 2344-00 Apparent Interlaminar Shear Strength of Parallel Fiber Composites by Short-Beam Method
- D 792-00 Density and Specific Gravity (Relative Density) of Plastics by Displacement
- D 2584-02 Ignition Loss of Cured Reinforced Plastics
- D 2734-94 Void Content of Reinforced Plastics
- D 3171-99 Fiber Content of Resin—Matrix Composites by Matrix Digestion

3.4.2.2 SACMA Publications.

- SRM 1-94 Compressive Properties of Oriented Fiber-Resin Composites
- SRM 8-94 Short-Beam Shear Strength of Oriented Fiber-Resin Composites
- SRM 18-94 Glass Transition Temperature (T_g) Determination by DMA of Oriented Fiber-Resin Composites

3.4.3 Unidirectional Material Forms.

Unidirectional tape prepreg material consists of fibers arranged in the same direction. Figure 4 shows a typical unidirectional tape system with the associated defined directions. Unidirectional materials are, commonly, the most difficult to produce valid and reproducible results from mechanical tests. Extreme care must be maintained throughout the panel production, specimen preparation, and testing phases to produce viable results for design allowables.

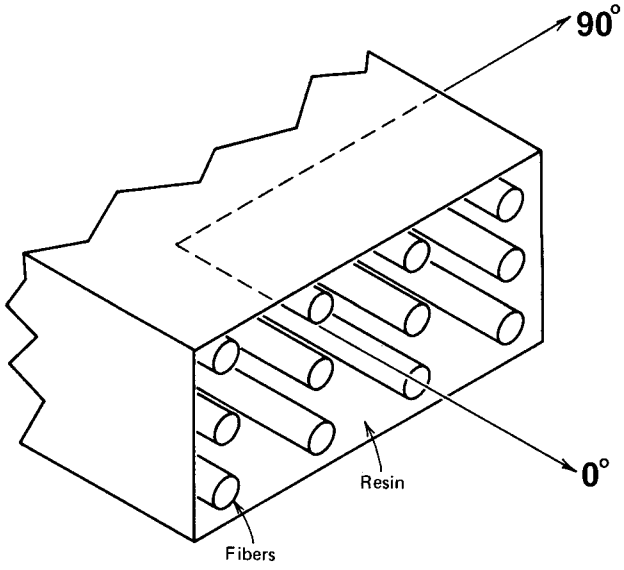


FIGURE 4. UNIDIRECTIONAL TAPE WITH DEFINED DIRECTIONS

3.4.4 Woven Fabric Material Forms.

Woven fabric weaves are characterized by the manner in which the warp and fill (sometimes known as weft) yarns are interlaced to form the fabric. Typically, the warp direction runs parallel to the selvage of the fabric (along the length of the fabric as it comes off the roll). The weaving style of the yarns has a great influence on the properties of the woven fabric. In composite reinforcement applications, weave styles are almost always variations of plain or satin weaves and are described in detail in sections 3.4.4.1 and 3.4.4.2. Figure 5 shows a typical woven fabric with defined directions.

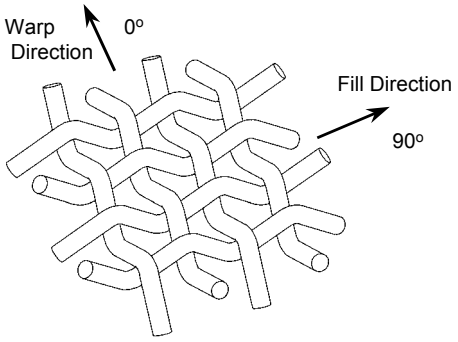


FIGURE 5. WARP AND FILL DIRECTIONS FOR WOVEN FABRIC MATERIAL
(Plain weave shown)

Some controversy exists over the exact methodology that should be applied when qualifying a woven fabric material form. Since most weave patterns have approximately equal yarn counts in both the warp and fill directions, some qualifications have used a $[0/90]_{ns}$ lay-up to produce qualification panels. This type of procedure, although it may reduce the amount of testing required, may produce a nonconservative design allowable if manufacturing procedures are not in place to verify cross-ply lay-up during manufacturing at all times. In a $[0]_n$ lay-up sequence for woven fabric material, the mechanical properties in the fill direction are generally lower than the warp direction due to prepreg manufacturing. For these reasons, the warp and fill directions should be treated as independent directions in the qualification process similar to a unidirectional tape. If the warp and fill direction are not accurately tracked in the composite manufacturing process, the lower of both the warp and fill should be used for the design allowable. If procedures are in place to track the warp and fill directions, the designer may use both warp and fill properties for the design allowables. If the differences are insignificant between warp and fill directions, the strength and modulus values can be pooled (added together) and the calculated basis value, thus, can be used for strength, and the average value can be used for modulus.

3.4.4.1 Plain Weaves.

In a plain weave fabric pattern, warp and fill yarns are interlaced over and under each other in an alternating pattern. Figure 6 shows a typical plain weave architecture of alternating yarns. Plain weave fabrics are ideally suited for flat laminates, where a high degree of drapeability is not required.

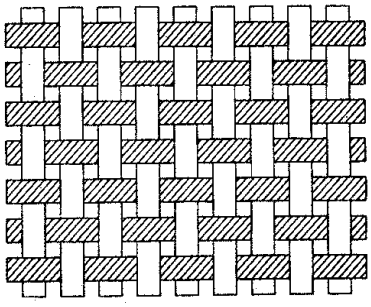


FIGURE 6. PLAIN WEAVE FABRIC CONSTRUCTION

3.4.4.2 Satin Weaves.

A satin weave construction consists of yarns that do not interlace at every yarn intersection. Instead, the yarns in both directions will cross over several intersections and interlace under one, as shown in figure 7. Satin weave fabrics have a higher degree of drapeability than plain weaves and are well suited for manufacturing parts with complex surfaces. Common satin weaves used in composite applications are four-harness satin, five-harness satin, and eight-harness satin.

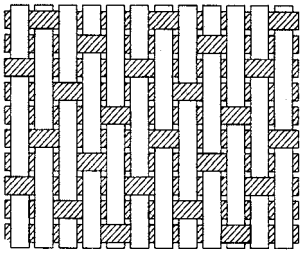


FIGURE 7. SATIN WEAVE FABRIC CONSTRUCTION (Five-harness satin shown)

Extreme care should be used when manufacturing the qualification panels using satin weave woven fabrics. Due to the unsymmetrical nature of the weave pattern, warpage may result during cure if strict lay-up practices are not followed. In the lay-up of a $[0]_n$ or $[warp]_n$ laminate, each corresponding ply should be rotated 180° about the warp axis to produce a lay-up of alternating the warp face and fill face, as depicted in figure 8.

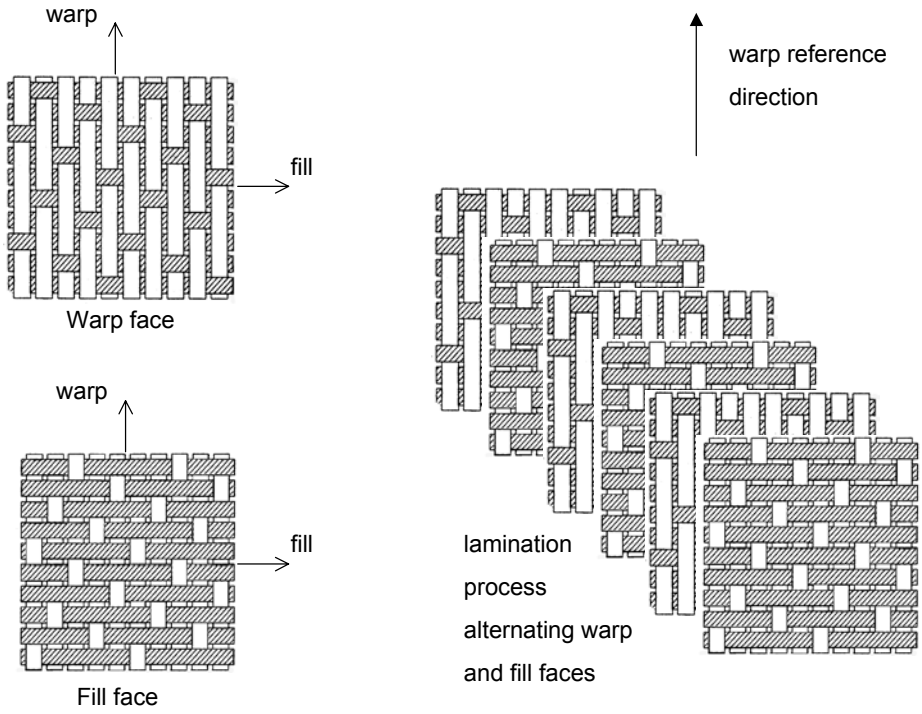


FIGURE 8. EXAMPLE SATIN WEAVE SHOWING ALTERNATING WARP AND FILL FACES USED FOR LAMINATION

3.4.5 Mechanical Property Testing and Specimen Geometry.

This section describes the specific specimen geometry used to produce each individual mechanical property. Specific dimensions and tolerances are provided for each specimen taken from the referenced test method(s) as well as requirements on the parallelism and perpendicularity. Requirements for the thickness of each specimen are provided and should be adjusted based upon the nominal cured ply thickness of the material system being qualified. Specific changes or additions to the referenced test methods are also presented.

For general guidelines with respect to specimen dimensions and tolerances, the document titled "Dimensioning and Tolerancing," American Society of Mechanical Engineers National Standard, Engineering Drawing and Related Document Practices, ASME Y14.5M-1994, provides guidelines for interpreting the specimen geometry, as shown for each test method and/or material type.

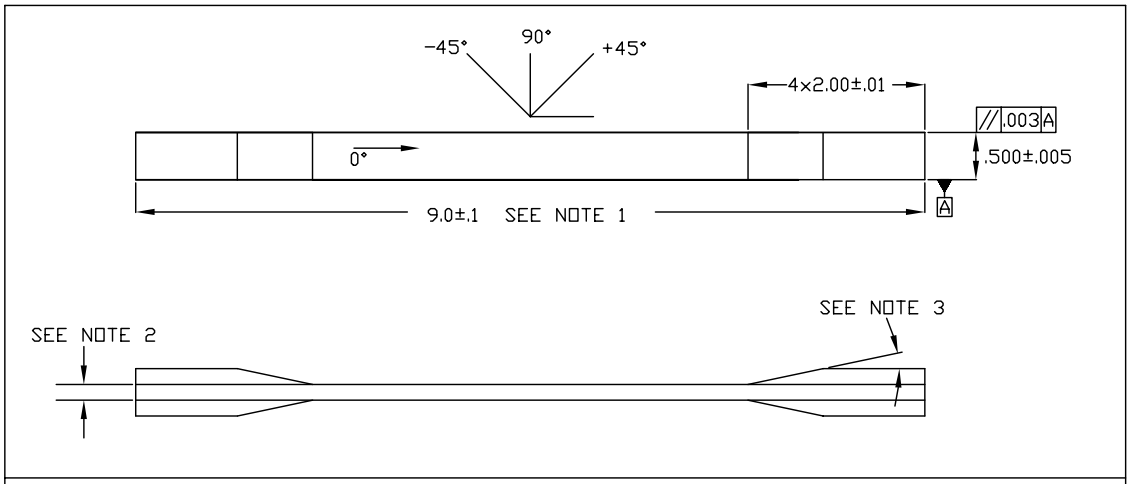
The test methods described in this section have been used to generate data for the NASA AGATE (Advanced General Aviation Transport Experiments) program. Other test methods that are accepted by the MIL-HDBK-17 committee can be substituted if starting out on a qualification process. These may be test methods such as ASTM D 3410 or ASTM D 6641 for compression and ASTM D 3518 for shear. The use of laminate and cross-ply factors to derive unidirectional strength properties, as described in MIL-HDBK-17E section 2.4.2, may also be used. See reference 2 for further information regarding the test methods.

3.4.5.1 Tensile Strength, Modulus, and Poisson's Ratio.

Specimens shall be fabricated to a, b, and c below and ASTM D 3039-00, Tensile Properties of Polymer Matrix Composite Materials.

a. Specimen Geometry

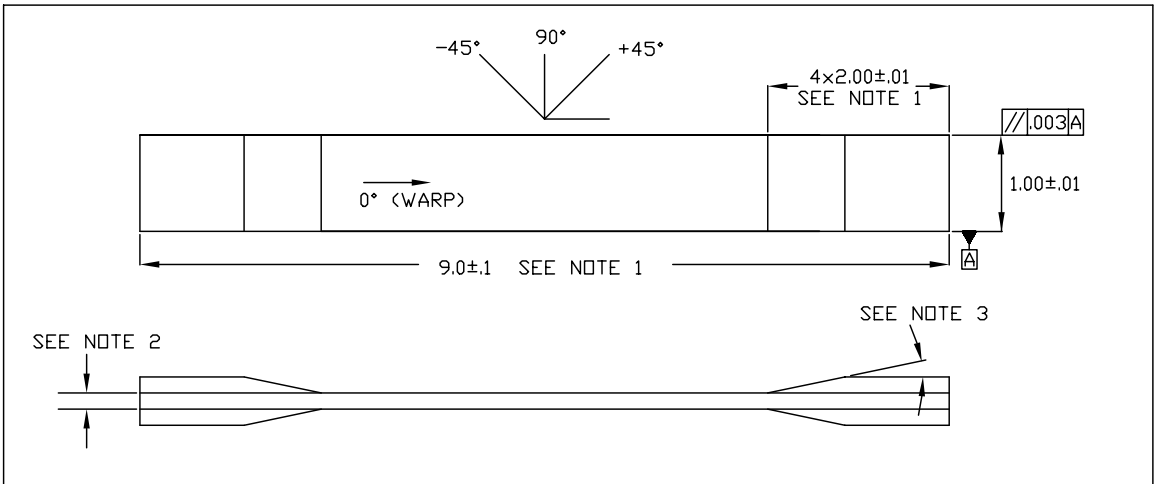
- 0° Tensile (Unidirectional Tape)—Strength, Modulus, and Poisson's Ratio (see figure 9)



NOTES:
1. MINIMUM LENGTH, LONGER SPECIMENS MAY BE USED PROVIDED THAT THE SAME TOLERANCE IS MAINTAINED
2. SPECIMEN THICKNESS BETWEEN 0.035-0.060
3. TAB BEVEL ANGLE BETWEEN 5-90°
4. DATUM A PARALLEL TO REFERENCE EDGE WITHIN ±0.25°; CANNOT BE VERIFIED ON A SPECIMEN BASIS
5. ALL DIMENSIONS IN INCHES
6. ADDITIONAL NOTES ARE LISTED IN b. AND c. OF THIS SECTION

FIGURE 9. ZERO DEGREE UNIDIRECTIONAL TAPE TENSION SPECIMEN

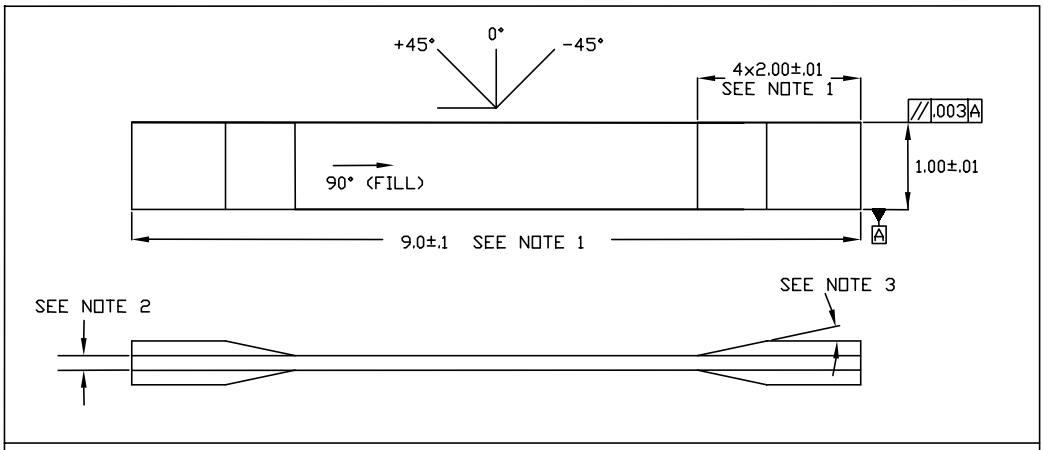
- 0° (warp) Tensile (Woven Fabric)—Strength, Modulus, and Poisson's Ratio (see figure 10)



NOTES:
1. MINIMUM LENGTH, LARGER DIMENSIONS MAY BE USED PROVIDED THAT THE SAME TOLERANCE IS MAINTAINED
2. SPECIMEN THICKNESS BETWEEN 0.090-0.120
3. TAB BEVEL ANGLE BETWEEN 5-90°
4. DATUM A PARALLEL TO REFERENCE EDGE WITHIN ±0.25°; CANNOT BE VERIFIED ON A SPECIMEN BASIS
5. ALL DIMENSIONS IN INCHES
6. ADDITIONAL NOTES ARE LISTED IN b. AND c. OF THIS SECTION

FIGURE 10. ZERO DEGREE (WARP) WOVEN FABRIC TENSION SPECIMEN

- 90° (fill) Tensile (Unidirectional Tape and Woven Fabric)—Strength, Modulus, and Poisson's Ratio (see figure 11)



NOTES:
1. MINIMUM LENGTH, LARGER DIMENSIONS MAY BE USED PROVIDED THAT THE SAME TOLERANCE IS MAINTAINED
2. SPECIMEN THICKNESS BETWEEN 0.090-0.120
3. TAB BEVEL ANGLE BETWEEN 5-90°
4. DATUM A PARALLEL TO REFERENCE EDGE WITHIN ±0.25°; CANNOT BE VERIFIED ON A SPECIMEN BASIS
5. ALL DIMENSIONS IN INCHES
6. ADDITIONAL NOTES ARE LISTED IN b. AND c. OF THIS SECTION

FIGURE 11. NINETY DEGREE (FILL) WOVEN FABRIC AND UNIDIRECTIONAL TENSION SPECIMENS

b. Laminate Lay-Up and Recommended Thickness

- 0° Tensile (Unidirectional Tape)

  $[0]_n$ where n is the number of plies
  Recommended Thickness: 0.040 inch

- 0° (warp) Tensile (Woven Fabric)

  $[0]_n$ where n is the number of plies
  Recommended Thickness: 0.100 inch

- 90° (Fill) Tensile (Unidirectional Tape and Woven Fabric)

  $[0]_n$ where n is the number of plies
  Recommended Thickness: 0.100 inch

c. Specific Additions and Changes to Referenced Test Method(s)

- Quality Control and Documentation Requirements

  At least one randomly selected specimen per subpanel should be checked for all dimensional tolerances detailed on the specimen geometry figures. If the

randomly selected specimen fails any one of the requirements, all specimens from that subpanel should be individually inspected for that dimension. If the specimens cannot be corrected to fall within the required tolerances, the impact of such deviation(s) must be investigated. Specimens with deviation(s) that will affect the test results must be discarded. Specimens with deviation(s) that will not affect the test results may be used provided that such deviations are documented on FAA Form 8130-9. A minimum of two width and thickness measurements must be recorded within the gage section of each specimen. The average width and thickness should be used for the final material property calculations.

- Strain Gage

  Perform strain gage application, per section 3.1.8, as required by section 4 of this qualification plan. Upon testing system alignment verification, back-to-back strain gages are not required to verify percent bending.

- Specimen Sampling

  Specimen sampling should be randomly selected, based upon the panel requirements delineated in appendix A or B.

- Recommended Calculation of Modulus of Elasticity and Poisson's Ratio

  Calculate the slope of a linear curve fit of the applicable data between the strain range given in table 3 of ASTM D 3039-00.

- Environmental Conditioning

  Perform specimen conditioning as outlined in section 3.2.

- Tabs

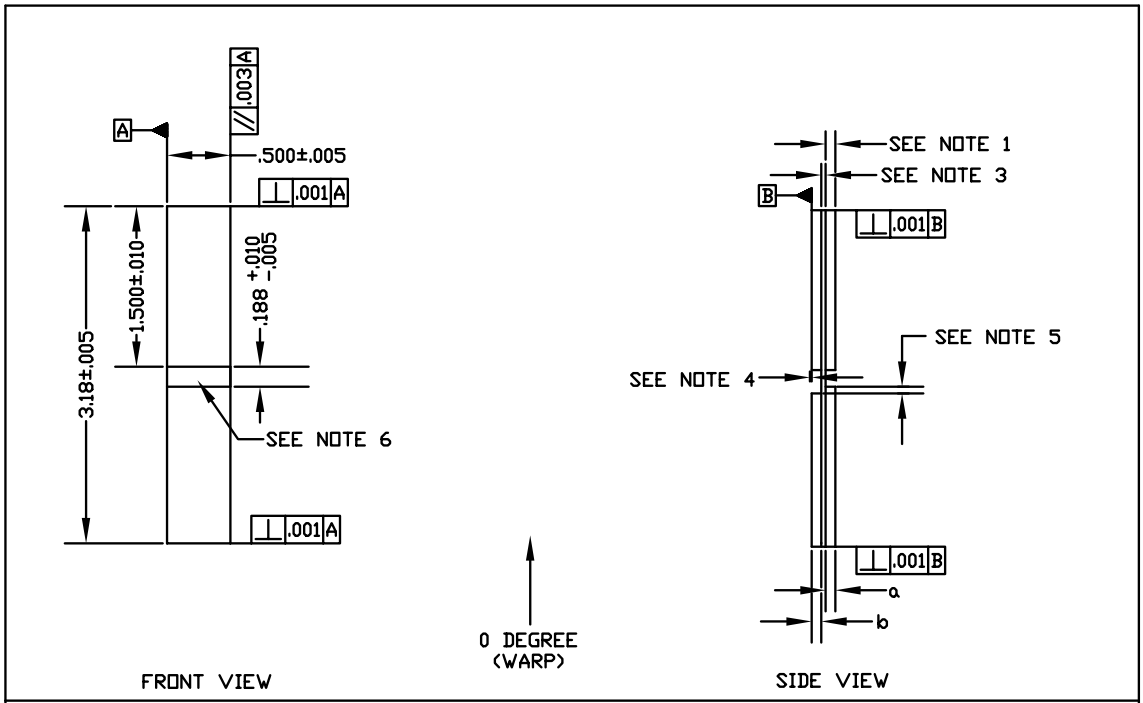
  Tab surfaces may be ground flat after tab-bonding operations if there is evidence of uneven adhesive bondline thickness that will cause bending in the specimens during gripping.

3.4.5.2 Compressive Strength and Modulus.

Specimens shall be fabricated to a, b, and c below and SACMA SRM 1-94, Compressive Properties of Oriented Fiber-Resin Composites.

a. Specimen Geometry

- 0° (Warp) Compressive (Unidirectional Tape and Woven Fabric)—Strength (see figure 12)

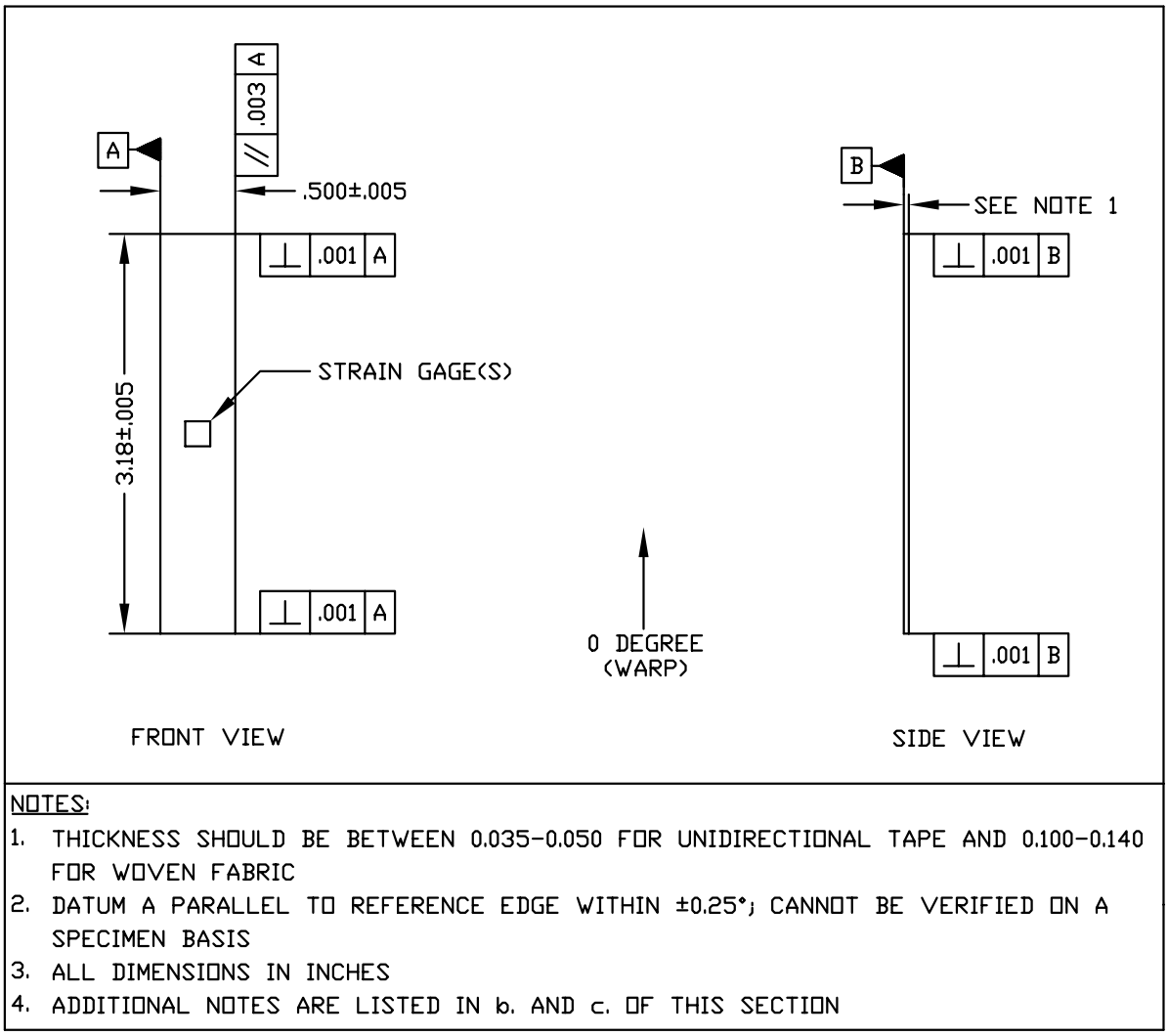


NOTES:

1. STRAIN COMPATIBLE TABBING MATERIAL
2. 'a' MUST EQUAL 'b' TO WITHIN 0.010. TAB THICKNESS EVALUATED PRIOR TO TABBING
3. THICKNESS SHOULD BE BETWEEN 0.035-0.050 FOR UNIDIRECTIONAL TAPE AND 0.100-0.140 FOR WOVEN FABRIC
4. END-TO-END TAB THICKNESS VARIATION, EVALUATED PRIOR TO TABBING, MUST BE LESS THAN 0.0025
5. SIDE-TO-SIDE OFFSET MUST BE LESS THAN 0.010
6. ADHESIVE SQUEEZE OUT IS ALLOWED AS LONG AS IT IS NOT CONTINUOUS ACROSS THE TABS AND THE GAGE SECTION CAN BE MEASURED
7. DATUM A PARALLEL TO REFERENCE EDGE WITHIN ±0.25°; CANNOT BE VERIFIED ON A SPECIMEN BASIS
8. ALL DIMENSIONS IN INCHES
9. ADDITIONAL NOTES ARE LISTED IN b. AND c. OF THIS SECTION

FIGURE 12. ZERO DEGREE (WARP) WOVEN FABRIC AND UNIDIRECTIONAL COMPRESSION STRENGTH SPECIMENS

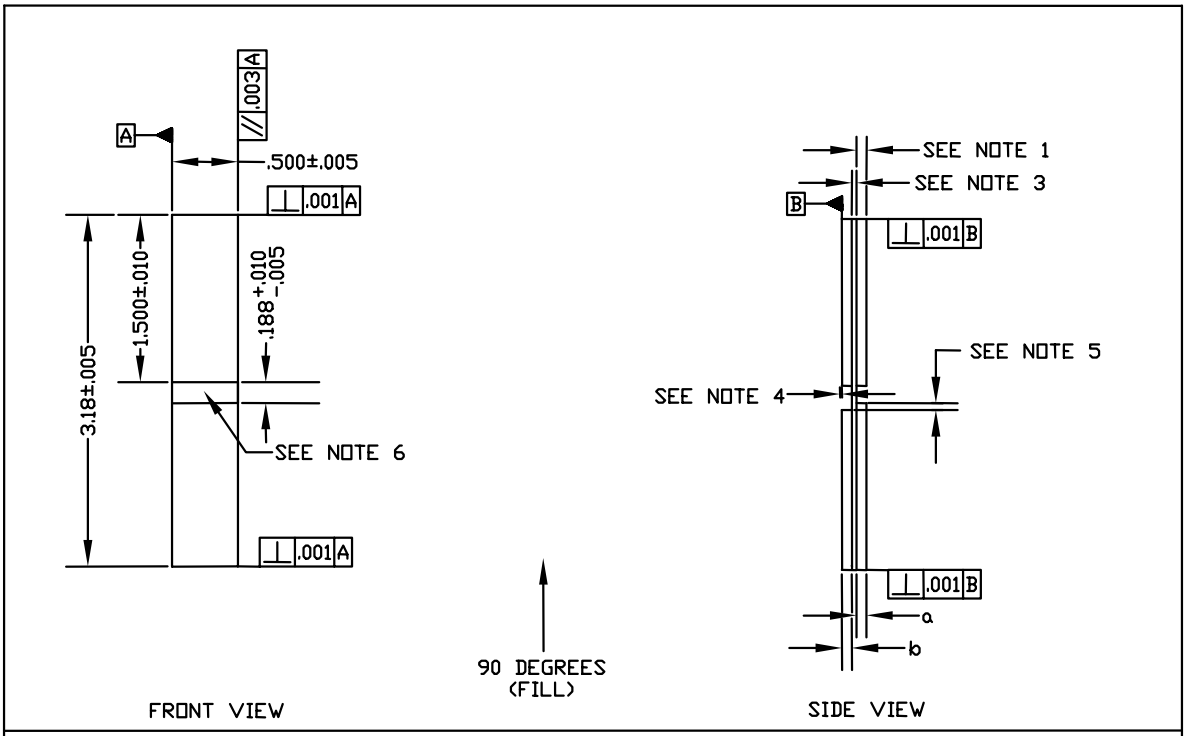
- 0° (warp) Compressive (Unidirectional Tape and Woven Fabric)—Modulus (see figure 13)



NOTES:
1. THICKNESS SHOULD BE BETWEEN 0.035–0.050 FOR UNIDIRECTIONAL TAPE AND 0.100–0.140 FOR WOVEN FABRIC
2. DATUM A PARALLEL TO REFERENCE EDGE WITHIN ±0.25°; CANNOT BE VERIFIED ON A SPECIMEN BASIS
3. ALL DIMENSIONS IN INCHES
4. ADDITIONAL NOTES ARE LISTED IN b. AND c. OF THIS SECTION

FIGURE 13. ZERO DEGREE (WARP) WOVEN FABRIC AND UNIDIRECTIONAL COMPRESSION MODULUS SPECIMENS

- 90° (fill) Compressive (Unidirectional Tape and Woven Fabric)—Strength (see figure 14)



NOTES:
1. STRAIN COMPATIBLE TABBING MATERIAL
2. 'a' MUST EQUAL 'b' TO WITHIN 0.010; TAB THICKNESS EVALUATED PRIOR TO TABBING
3. THICKNESS SHOULD BE BETWEEN 0.090-0.120 FOR UNIDIRECTIONAL TAPE AND 0.100-0.140 FOR WOVEN FABRIC
4. END-TO-END TAB THICKNESS VARIATION, EVALUATED PRIOR TO TABBING, MUST BE LESS THAN 0.0025
5. SIDE-TO-SIDE OFFSET MUST BE LESS THAN 0.010
6. ADHESIVE SQUEEZE OUT IS ALLOWED AS LONG AS IT IS NOT CONTINUOUS ACROSS THE TABS AND THE GAGE SECTION CAN BE MEASURED
7. DATUM A PARALLEL TO REFERENCE EDGE WITHIN ±0.25°; CANNOT BE VERIFIED ON A SPECIMEN BASIS
8. ALL DIMENSIONS IN INCHES
9. ADDITIONAL NOTES ARE LISTED IN b. AND c. OF THIS SECTION

FIGURE 14. NINETY DEGREE (FILL) WOVEN FABRIC AND UNIDIRECTIONAL COMPRESSION STRENGTH SPECIMENS

- 90° (fill) Compressive (Unidirectional Tape and Woven Fabric)—Modulus (see figure 15)

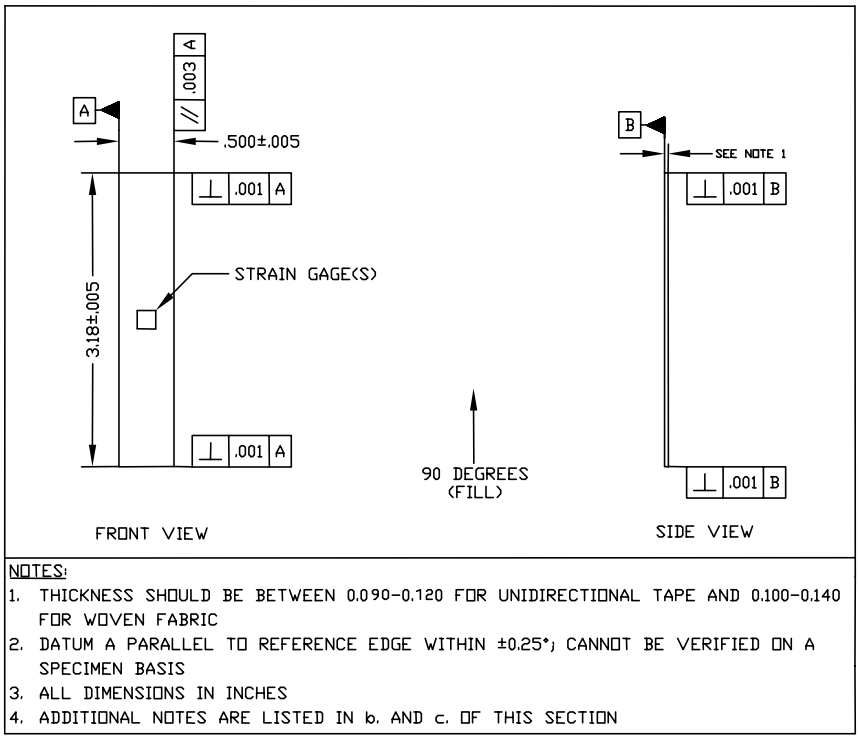


FIGURE 15. NINETY DEGREE (FILL) WOVEN FABRIC AND UNIDIRECTIONAL COMPRESSION MODULUS SPECIMENS

b. Laminate Lay-Up and Recommended Thickness

- 0° Unidirectional Tape-Compressive Strength and Modulus

  $[0]_n$ where n is the number of plies
  Recommended Thickness: 0.040 inch

- 90° Unidirectional Tape-Compressive Strength and Modulus

  $[0]_n$ where n is the number of plies
  Recommended Thickness: 0.100 inch

- 0° (warp) Woven Fabric-Compressive Strength and Modulus

  $[0]_n$ where n is the number of plies
  Recommended Thickness: 0.120 inch

- 90° (fill) Woven Fabric-Compressive Strength and Modulus

  $[0]_n$ where n is the number of plies
  Recommended Thickness: 0.120 inch

c. Specific Additions and Changes to Reference Test Method(s)

- Quality Control and Documentation Requirements

  Due to the extreme sensitivity of this test method, all specimens for 0° unidirectional tape must be checked for all dimensional tolerances detailed on the specimen geometry figures. Particular attention should be addressed to parallelism and perpendicularity. In the case of woven fabric materials or 90° unidirectional tape, at least one randomly selected specimen per subpanel must be checked for all dimensional tolerances on the specimen geometry. If the randomly selected specimen fails any one of the requirements, all specimens from that subpanel must be individually inspected for that dimension. If the specimens cannot be corrected to fall within the required tolerances, the impact of such deviation(s) must be investigated. Specimens with deviation(s) that will affect the test results must be discarded. Specimens with deviation(s) that will not affect the test results may be used, provided that such deviations are documented on FAA Form 8130-9. A minimum of two width and two thickness measurements must be recorded within the gage section of each specimen. The average width and thickness must be used for the final material property calculations.

- Strain Gage

  Perform strain gage application, per section 3.1.8, as required by section 4 of this qualification plan. Back-to-back strain gages are not mandatory for modulus tests.

- Sampling

  Specimen sampling should be randomly selected, based upon the panel requirements delineated in appendix A or B.

- Recommended Calculation of Modulus of Elasticity and Poisson's Ratio

  Calculate the slope of a linear curve fit of the applicable data between the 1000-3000 με range as needed.

- Environmental Conditioning

  Perform specimen conditioning as outlined in section 3.2.

- Tabs

  Tab surfaces may be ground flat after tab-bonding operations if there is evidence of nonparallel tab surfaces that will cause the specimens to buckle prematurely.

3.4.5.3 In-Plane Shear Strength and Modulus.

Specimens shall be fabricated to a, b, and c below and ASTM D 5379-98, Shear Properties of Composite Materials by the V-Notched Beam Method.

a. Specimen Geometry

- In-Plane Shear Strength and Modulus (Unidirectional Tape and Woven Fabric) (see figure 16)

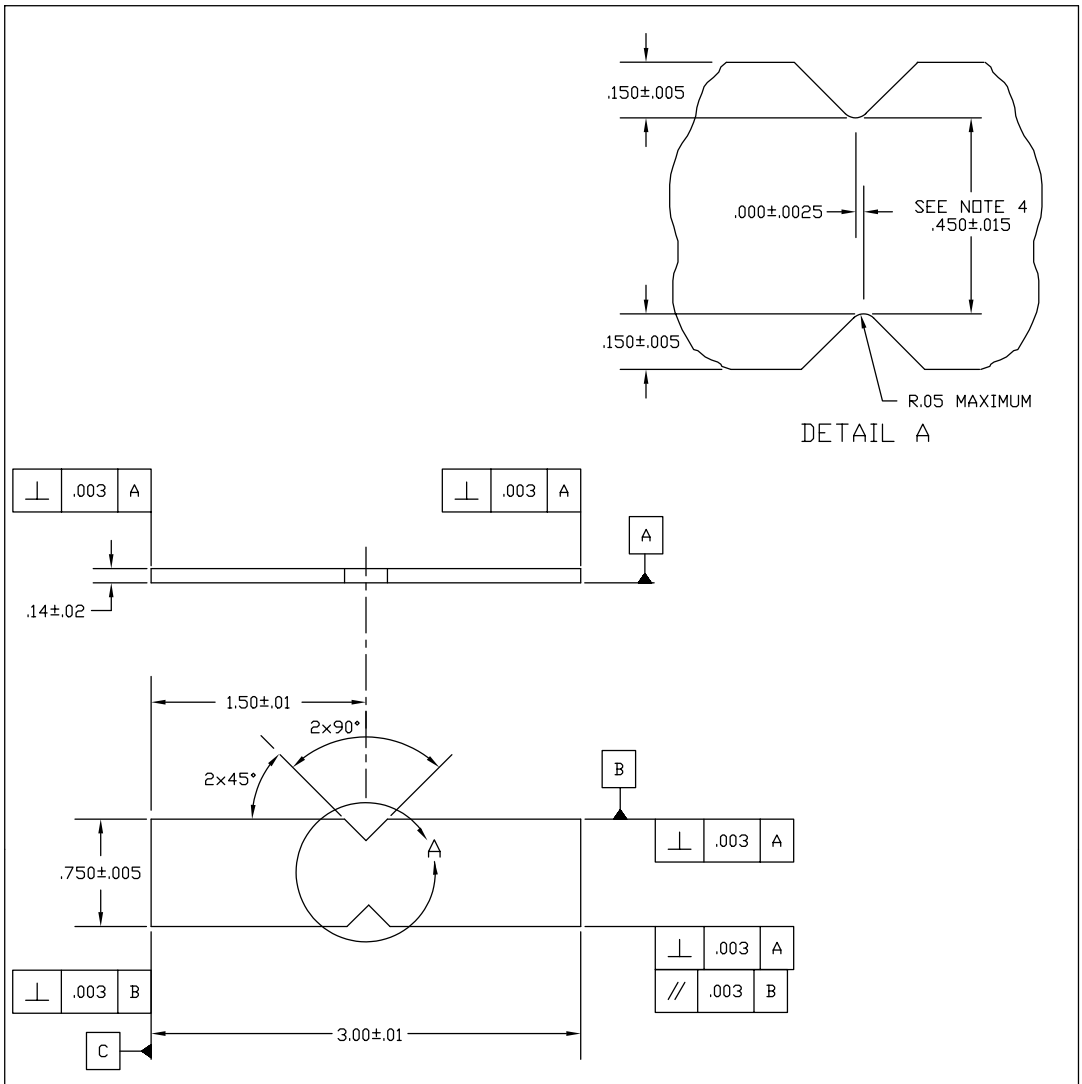


FIGURE 16. IN-PLANE SHEAR STRENGTH AND MODULUS SPECIMEN

b. Laminate Lay-Up and Recommended Thickness

- In-Plane Shear Strength and Modulus (Unidirectional Tape and Woven Fabric)

  $[0/90]_{ns}$ where n is the number of plies and s indicates a symmetric lay-up configuration

  Recommended Thickness: 0.140 inch

  Note: 0.12-0.16 inch thickness recommendation allows for testing without the use of tabs.

c. Specific Additions and Changes to Referenced Test Method(s)

- Quality Control and Documentation Requirements

  At least one randomly selected specimen per subpanel should be checked for all dimensional tolerances detailed on the specimen geometry figures. If the randomly selected specimen fails any one of the requirements, all specimens from that subpanel must be individually inspected for that dimension. If the specimens cannot be corrected to fall within the required tolerances, the impact of such deviation(s) must be investigated. Specimens with deviation(s) that will affect the test results must be discarded. Specimens with deviation(s) that will not affect the test results may be used, provided that such deviations are indicated on FAA Form 8130-9. A minimum of one width measurement across the notches (see figure 16, Detail A, Note 4) and two thickness measurements should be recorded within the gage section of each specimen. The average of these measurements should be used in the final material property calculations.

- Strain Gage

  Perform strain gage application, per section 3.1.8, as required by section 4 of this qualification plan. Back-to-back strain gages are not mandatory for modulus tests if specimen thickness is adequate to prevent twisting of the specimen during testing. Sample specimens should be verified prior to beginning the test program to be twist-free.

- Sampling

  Specimen sampling should be randomly selected, based upon the panel requirements delineated in appendix A or B.

- Recommended Calculation of Shear Strength

  Calculate the shear strength for both 5% strain and the ultimate value. The ultimate strength can be used for comparison during fluid sensitivity screening as

outlined in section 4.5.3. It is not possible to attach a strain gage during most fluid sensitivity tests.

- Recommended Calculation of Shear Modulus

  Calculate the slope of a linear curve fit of the applicable data between the strain range outlined in Section 12 of ASTM D 5379-98.

- Environmental Conditioning

  Perform specimen conditioning as outlined in section 3.2.

- Special Note

  This method is not recommended for materials that may not demonstrate homogeneity with respect to the test section.

3.4.5.4 Short-Beam Shear Strength.

Specimens shall be fabricated to a, b, and c below or ASTM D 2344-00, Apparent Interlaminar Shear Strength of Parallel Fiber Composites by Short-Beam Methods or SACMA SRM 8-94, Short-Beam Shear Strength of Oriented Fiber-Resin Composites.

Note: This test method is for quantitative quality control purposes only and should not be used for interlaminar shear strength values.

a. Specimen Geometry

- Short-Beam Shear Strength (Unidirectional Tape and Woven Fabric) (see figure 17)

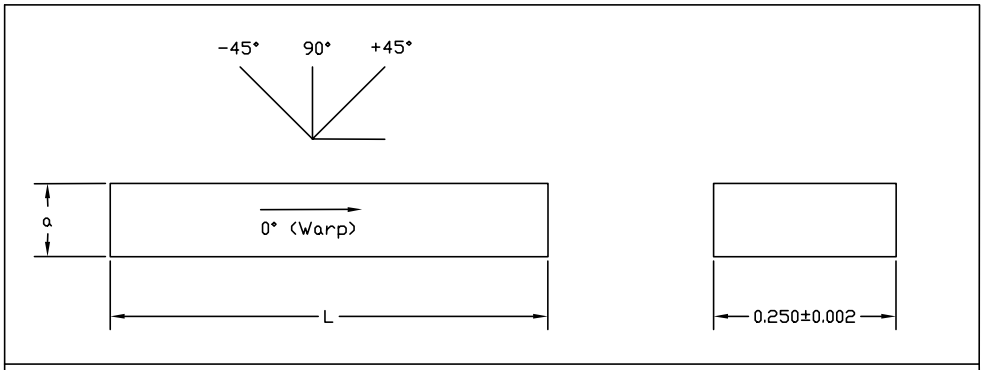


FIGURE 17. SHORT-BEAM SHEAR STRENGTH SPECIMEN

b. Laminate Lay-Up and Recommended Thickness

- Short-Beam Shear Strength (Unidirectional Tape and Woven Fabric)

  $[0]_n$ where n is the number of plies
  Recommended Thickness: 0.225 inch

c. Specific Additions and Changes

- Quality Control and Documentation Requirements

  At least one randomly selected specimen per subpanel should be checked for all dimensional tolerances detailed on the specimen geometry figures. If the randomly selected specimen fails any one of the requirements, all specimens from that subpanel must be individually inspected for that dimension. If the specimens cannot be corrected to fall within the required tolerances, the impact of such deviation(s) must be investigated. Specimens with deviation(s) that will affect the test results must be discarded. Specimens with deviation(s) that will not affect the test results may be used, provided that such deviations are indicated on FAA Form 8130-9. A minimum of two width and two thickness measurements must be recorded for each specimen. These measurements must be taken at the center of the specimen. The average of these measurements must be used in the final material property calculations.

- Sampling

  Specimens used for this test method are not required to follow the processing requirements delineated in section 3.1.3. Specimen sampling should be randomly selected, based upon the requirements delineated in appendix A or B.

- Span and Specimen Length

  For glass fibers, the recommended length-to-thickness ratio is 7 and the recommended span-to-thickness ratio is 4. For graphite fibers, the recommended length-to-thickness ratio is 6 and the recommended span-to-thickness ratio is 4. The span may be adjusted to obtain proper failure modes.

- Ply Orientation

  Specimen should be sectioned such that the 0° or warp direction is along the length of the specimen.

3.4.6 Additional Test Methods.

3.4.6.1 Fiber Volume Fraction.

3.4.6.1.1 Fiberglass Laminates.

a. Procedure—ASTM D 2584-02, Ignition Loss of Cured Reinforced Resins

b. Specific Additions or Changes

- One sample should be tested per panel used for fabricating mechanical test coupons.
- Specimens should be desiccated or oven-dried prior to taking initial weight measurement, instead of being exposed to the standard laboratory atmosphere.

3.4.6.1.2 Carbon or Graphite Laminates.

a. Procedure—ASTM D 3171-99, Fiber Content of Resin-Matrix Composites by Matrix Digestion, Procedure B

b. Specific Additions or Changes

- One sample should be tested per panel used for fabricating mechanical test coupons.
- Specimens should be desiccated or oven-dried prior to taking initial weight measurement, instead of being exposed to the standard laboratory atmosphere.
- Procedure B is recommended due to the ease of process. Although procedures A and C are recommended for epoxy matrices, both require a high capital investment in equipment. Assessment as to the degree of digestion by the proposed method should be investigated prior to beginning the test program for each matrix system.

3.4.6.2 Void Volume Fraction.

3.4.6.2.1 Specimen Density.

a. Procedure—ASTM D 792-00, Density and Specific Gravity (Relative Density) of Plastics by Displacement, Procedure A

b. Specific Additions or Changes

- One sample should be tested per panel used for fabricating mechanical test coupons.

- Optimum results will be obtained if samples tested for density are the same as those used for fiber volume fraction tests (section 3.4.6.1).

- Specimens should be dried in a desiccated oven or vacuum-oven prior to taking initial weight measurement, instead of being exposed to the standard laboratory atmosphere.

- Upon immersing the specimens in water, the weight should be recorded immediately, as the composite specimen will begin to absorb small amounts of water. If bubbles adhere to the sample, they should be removed immediately and the weight recorded soon thereafter.

3.4.6.2.2 Specimen Void Content.

a. Procedure—ASTM D 2734-94, Void Content of Reinforced Plastics, Procedure A

b. Specific Additions or Changes

- Although the test standard references only ASTM D 2584-94, the void calculation is equally applicable to method ASTM D 3171-99.

- To avoid negative void content results, section 7.1 of ASTM D 2734-94 should be strictly followed. The material supplier should supply certified resin density measurements, or procedure ASTM D 792-00 should be used on a representative sample of cured neat resin to obtain the resin density value that is used in the void calculation.

3.4.6.3 Glass Transition Temperature.

a. Procedure—SACMA SRM 18-94, Glass Transition Temperature (T_g) Determination by DMA of Oriented Fiber-Resin Composites

b. Specific Additions or Changes

- Fixture Type: Three-point bend

- Testing Frequency: 1 Hz

- Heating Rate: 5° ±0.2°C per minute

- Temperature range: Test should begin from room temperature and end at a temperature 50°C above T_g but below decomposition temperature. In the case of a lower curing material system (below 240°F), it may be necessary to begin the test below room temperature to obtain a sufficient slope at the beginning of the test.

- T_g is determined from a logarithmic plot of the storage modulus as a function of temperature. The T_g is determined to be the intersection of the two slopes from the storage modulus. Figure 18 depicts a typical plot and the T_g measurement.

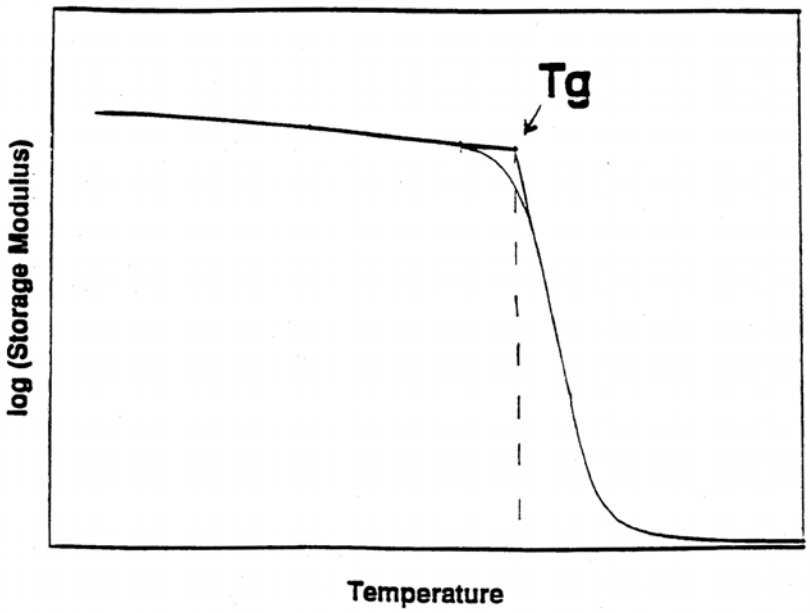


FIGURE 18. GLASS TRANSITION TEMPERATURE DETERMINATION FROM STORAGE MODULUS

4. QUALIFICATION PROGRAM.

4.1 INTRODUCTION.

This section outlines the specific number of tests required at each condition to substantiate a statistically based design allowable for each material property. Unless noted, the following test procedures will be performed for each individual material system being qualified.

4.2 GENERAL.

For a composite material system design allowable, several batches of material must be characterized to establish the statistically based material property for each of the material systems. The definition of a batch of material for this qualification plan refers to a quantity of homogenous resin (base resin and curing agent) prepared in one operation with traceability to individual component batches as defined by the resin manufacturer.

To account for processing and panel-to-panel variability, the material system being qualified must also be representative of multiple-processing cycles as delineated in section 3.1.3. For this qualification plan, each batch of prepreg material must be represented by a minimum of two independent processing or curing cycles.

4.3 TECHNICAL REQUIREMENTS.

To substantiate the environmental effects with respect to the material properties, several environmental conditions will be defined to represent extreme cases of exposure. The conditions defined as extreme cases in this qualification plan are listed as follows:

- Cold Temperature Dry (CTD) -65°F with an as-fabricated moisture content
- Room Temperature Dry (RTD) ambient laboratory conditions with an as-fabricated moisture content
- Elevated Temperature Dry (ETD) 180°F with an as-fabricated moisture content
- Elevated Temperature Wet (ETW) 180°F with an equilibrium moisture weight gain in a 85% relative humidity environment, per section 3.2

4.4 MATERIAL QUALIFICATION PROGRAM FOR UNCURED PREPREG.

Table 1 describes the physical tests recommended for each batch of material received from the material vendor. These tests should be traceable to each referenced test method. These test methods are for the purpose of quality control in addition to specific values used in the normalization of material data (described in section 5.2). Some of the tests must be repeated in an incoming receiving inspection. Usually this retesting provides a verification of shipping to the airframe manufacturer and to establish that an error did not occur during shipment. In general, it should be noted that most of these properties significantly influence the producibility of the material system and commonly do not influence the resulting mechanical properties.

TABLE 1. RECOMMENDED PHYSICAL AND CHEMICAL PROPERTY TESTS TO BE PERFORMED BY THE MATERIAL VENDOR

No.	Test Property	Test Method(s)		No. of Replicates per Batch
		ASTM	SACMA	
1	Resin Content	D 3529, C 613, D 5300, D 3171	SRM 23, SRM 24	6
2	Volatile Content	D 3530	- - -	6
3	Gel Time	D 3532	SRM 19	6
4	Resin Flow	D 3531	SRM 22	6
5	Fiber Areal Weight	D 3776	SRM 23, SRM 24	6
6	IR (Infrared Spectroscopy)	E 1252, E 168	- - -	3
7	HPLC (High Performance Liquid Chromatography)*	- - -	SRM 20	3
8	DSC (Differential Scanning Calorimetry)	E 1356	SRM 25	3

*Sections 5.5.1 and 5.5.2 of MIL-HDBK-17-1E describe detailed procedures that will be used when extracting resin from prepreg and performing HPLC tests.

Listed in table 1 are suggestions taken from MIL-HDBK-17-1E for the acceptable test methods to produce each property. Both ASTM and SACMA test methods are shown. The material vendor should describe the exact test method used for each property, and such methods must comply with the test methods described in table 1.

These chemical and physical tests also represent the properties of the prepreg system with the fibers and resin combined. The quality control procedures of the material vendor should be reviewed to ensure that quality control programs are in place for both the raw fiber and neat resin. The material vendor should submit these quality procedures to each manufacturer and be on file as part of the original qualification as well as part of quality assurance documentation for the airframe manufacturer.

4.5 MATERIAL QUALIFICATION PROGRAM FOR CURED LAMINA MAIN PROPERTIES.

The required number of material batches and replicates per batch are presented in the following sections. For the purpose of presentation, the following format was adopted to represent the required number of batches and replicates per batch:

x

where the first # represents the required number of batches and the second # represents the required number of replicates per batch. For example, 3 x 6 refers to 3 batches of material and 6 specimens per batch for a total requirement of 18 test specimens.

The MIL-HDBK-17 Working Group is in the process of revising the definition of prepreg batch at the time of this publication. As an interim, the definition of prepreg batch in section 9.0 may be used. Note that duplication of fiber or resin lot in any two prepreg batches within a material qualification program is not allowed. According to the definition, the prepreg produced after an interim run or a significant downtime should be considered as a separate prepreg batch but should not be used in a material qualification program together with the previous prepreg batch because this would result in a duplication of the resin or fiber lot. In addition, minor changes in resin constituent lot(s), to produce a separate resin lot, is undesirable. The objective is to ensure that the material qualification database accurately represents the population and the associated material variability.

Table 2 shows the cured lamina physical properties required to support the maximum operational temperature limit of the material system as well as specific data to be used in the statistical design-allowable generation. Typically, the maximum operational limit for the material should have a margin that is at least 50°F below the wet glass transition temperature.

TABLE 2. CURED LAMINA PHYSICAL PROPERTY TESTS

Physical Property	Test Procedure	No. of Replicates per Batch
Fiber Volume	ASTM D 3171[1] or D 2584[2]	See note 3
Resin Content	ASTM D 3171[1] or D 2584[2]	See note 3
Void Content	ASTM D 2734[4]	See note 3
Cured Neat Resin Density	ASTM D 792	See note 5
Glass Transition Temperature (dry[6])	SACMA SRM 18	3
Glass Transition Temperature (wet[7])	SACMA SRM 18	3

Notes:

1. Test method used for carbon or graphite materials.
2. Test method used for fiberglass materials.
3. At least one test shall be performed on each panel manufactured for qualification (see appendices A and B).
4. Test method may also be applied to carbon or graphite materials.
5. Data or neat resin sample should be provided by material supplier for each batch of material.
6. Dry specimens are as-fabricated specimens that have been maintained at ambient conditions in an environmentally controlled laboratory.
7. Wet specimens are humidity-aged until an equilibrium moisture weight gain is achieved, per section 3.2.

Fiber, resin, and void fraction specimens are taken from each subpanel used for qualification to verify quality and to establish ranges for acceptable production.

The properties obtained from the tests in this section may be used to develop mature material specifications for material procurement as well as used to develop acceptable limits for material equivalency and acceptance. In many cases, the properties generated are adequate for material equivalency and acceptance purposes. However, since some materials such as unidirectional carbon/epoxy are rather sensitive to specimen preparation and testing skills, additional tests are recommended for such materials. Reference 3 provides guidance for performing additional tests for the purpose of material equivalency and acceptance.

4.5.1 Robust Sampling Requirements for A- and B-Basis Allowables.

Table 3 describes the number of tests required for each environmental condition along with the relevant test method for robust sampling. The format shown in each matrix is described in section 4.5. The temperature for each environmental condition is described in section 4.3.

TABLE 3. ROBUST SAMPLING REQUIREMENTS FOR CURED LAMINA MAIN PROPERTIES

Figure No.	Test	Method Reference	No. of Specimens Per Test Condition			
			CTD[1]	RTD[2]	ETW[3]	ETD[4]
9* or 10*	0 (warp) Tensile Modulus, Strength and Poisson's Ratio	ASTM D 3039	5 x 11	5 x 11	5 x 11	5 x 11
11*	90° (fill) Tensile Modulus and Strength	ASTM D 3039	5 x 11	5 x 11	5 x 11	5 x 11
12	0° (warp) Compressive Strength	SACMA SRM 1	5 x 11	5 x 11	5 x 11	5 x 11
13*	0° (warp) Compressive Modulus	SACMA SRM 1	5 x 11	5 x 11	5 x 11	5 x 11
14	90° (fill) Compressive Strength	SACMA SRM 1	5 x 11	5 x 11	5 x 11	5 x 11
15*	90° (fill) Compressive Modulus	SACMA SRM 1	5 x 11	5 x 11	5 x 11	5 x 11
16*	In-Plane Shear Modulus and Strength	ASTM D 5379	5 x 11	5 x 11	5 x 11	5 x 11
17	Short-Beam Shear	ASTM D 2344	--	5 x 11	--	--

*Strain gages or extensometers used during testing.

Notes:

1. Five batches of material are required (test temperature = -65° ±5°F, moisture content = as-fabricated[5]).
2. Five batches of material are required (test temperature = 70° ±10°F, moisture content = as-fabricated[5]).
3. Five batches of material are required (test temperature = 180° ±5°F, moisture content = per section 3.2).
4. Five batches of material are required (test temperature = 180° ±5°F, moisture content = as-fabricated[5]).
5. Dry specimens are as-fabricated specimens that have been maintained at ambient conditions in an environmentally controlled laboratory.

4.5.2 Reduced Sampling Requirements for B-Basis Allowables.

Table 4 describes the number of tests required for each environmental condition along with the relevant test method for reduced sampling. The format shown in each matrix is described in section 4.5. The temperature for each environmental condition is described in section 4.3.

TABLE 4. REDUCED SAMPLING REQUIREMENTS FOR CURED LAMINA MAIN PROPERTIES

Figure No.	Test	Method Reference	No. of Specimens Per Test Condition			
			CTD[1]	RTD[2]	ETW[3]	ETD[4]
9 or 10*	0^o (warp) Tensile Modulus, Strength and Poisson's Ratio	ASTM D 3039	3 x 6	3 x 6	3 x 6	3 x 6
11*	90^o (fill) Tensile Modulus and Strength	ASTM D 3039	3 x 6	3 x 6	3 x 6	3 x 6
12	0^o (warp) Compressive Strength	SACMA SRM 1	3 x 6	3 x 6	3 x 6	3 x 6
13*	0^o (warp) Compressive Modulus	SACMA SRM 1	3 x 6	3 x 6	3 x 6	3 x 6
14	90^o (fill) Compressive Strength	SACMA SRM 1	3 x 6	3 x 6	3 x 6	3 x 6
15*	90^o (fill) Compressive Modulus	SACMA SRM 1	3 x 6	3 x 6	3 x 6	3 x 6
16*	In-Plane Shear Modulus and Strength	ASTM D 5379	3 x 6	3 x 6	3 x 6	3 x 6
17	Short-Beam Shear	ASTM D 2344	--	3 x 6	--	--

*Strain gages or extensometers used during testing.

Notes:

1. Three batches of material are required (test temperature = -65° ±5°F, moisture content = as-fabricated[5]).
2. Three batches of material are required (test temperature = 70° ±10°F, moisture content = as-fabricated[5]).
3. Three batches of material are required (test temperature = 180° ±5°F, moisture content = per section 3.2).
4. Three batches of material are required (test temperature = 180° ±5°F, moisture content = as-fabricated[5]).
5. Dry specimens are as-fabricated specimens that have been maintained at ambient conditions in an environmentally controlled laboratory.

4.5.3 Fluid Sensitivity Screening.

In addition to moisture, composite materials may come in contact with various kinds of fluids during service. These fluids usually fall into two exposure classifications: (1) a fluid that is in contact with the material for an extended period of time or (2) a fluid that is wiped on and off (or evaporates) with relatively short exposure times.

To assess the degree of sensitivity of fluids other than water or moisture, table 5 shows various fluid types that will be used in this qualification plan. Additional fluids, such as de-icing fluids, may also be required, depending on the particular application.

TABLE 5. FLUID TYPES USED FOR SENSITIVITY STUDIES

Fluid Type	Specification	Exposure Classification
Jet Fuel (JP-4)	MIL-T-5624	Extended Period
Hydraulic Fluid (Tri-N-butyl phosphate ester)	Laboratory Grade	Extended Period
Solvent (Methyl Ethyl Ketone)	Laboratory Grade	Wipe On and Off

To assess the influence of various fluids types, a test method sensitive to matrix degradation will be used as an indicator of fluid sensitivity and compared to the unexposed results at both RTD and ETD conditions. Engineering judgement and statistical tests should be used to assess the degree of material degradation. If significant degradation occurs, the material systems must be re-evaluated for possible fluid degradation (other than water or moisture). Table 6 shows the fluid sensitivity-testing matrix with respect to the fluids defined in table 5. Visual inspection, inspection under a stereoscope, and thickness measurements are also often useful for determining matrix degradation.

TABLE 6. MATERIAL QUALIFICATION PROGRAM FOR FLUID RESISTANCE

Fluid Type	Test Method	Test Temperature (°F)	Exposure[1]	Number of Replicates[2]
Jet Fuel (JP-4)	ASTM D 5379[3]	180	See note 4	5
Hydraulic Fluid	ASTM D 5379[3]	180	See note 4	5
Solvent	ASTM D 5379[3]	Ambient	See note 5	5

Notes:

1. Soaking in fluid at ambient temperature (immersion)
2. Only a single batch of material is required
3. Ultimate shear strength only since strain gages typically will not bond to fluid soaked specimens
4. Exposure duration = 500 hours ±50 hours
5. Exposure duration = 60 to 90 minutes

5. DESIGN-ALLOWABLE GENERATION.

5.1 INTRODUCTION.

Upon completion of the mechanical test program and associated data reduction, the next step in the qualification procedure is to produce statistical design allowables for each mechanical property. Due to the inherent material property variability in composite materials, this variability should be acknowledged when assigning design values to each mechanical property. Although the statistical procedures presented in the following sections account for most common types of variability, it should be noted that these procedures might not account for all sources of variability.

A- and B-basis design allowables are determined for each strength property using the statistical procedures outlined in the following sections. In the case of modulus and Poisson's ratio design values, the average value of all corresponding tests for each environmental condition should be used.

If strain design allowables are required, simple one-dimensional linear stress-strain relationships may be used to obtain corresponding strain design values. However, it should be noted that this process should approximate tensile and compressive strain behavior relatively well but may produce extremely conservative strain values in shear, due to the nonlinear behavior. These conservative shear allowables are appropriate if a linear analysis of the laminate is performed. If a nonlinear analysis is performed, then the nonlinear shear stress-strain curve may be used, with a maximum strain value of 5% used as the shear strain allowable (reference MIL-HDBK-17-1E, section 5.7.6).

5.2 NORMALIZATION.

5.2.1 Normalization Procedure.

This normalization method is performed for direct comparison of mechanical test results, adjusting raw test values to a specified fiber volume content. The process of data normalization attempts to reduce variability in fiber-dominated properties and is justified on the basis that most of the load is carried by the fibers.

The following excerpts and methodology are taken from MIL-HDBK-17-1E, section 2.4.3.

5.2.1.1 Assumptions.

- The method is based on the assumption that the relationship between fiber volume fraction and ultimate laminate strength is linear over the entire range of fiber/resin ratios. (It neglects the effects of resin starvation at high fiber contents.)
- Fiber volume is not commonly measured for each test sample, so this method accounts for the fiber volume variation between individual test specimens by using a relationship between fiber volume fraction and laminate cured ply thickness. This relationship is virtually linear in the 0.45 to 0.65 fiber volume fraction range.

5.2.1.2 Methodology.

- Define an equivalent thickness of fiber, which would result if the fiber material could be shaped into a solid sheet of uniform thickness with no air space between filaments

$$t_f = \frac{FAW}{\rho_f} \tag{1}$$

where

t_f = equivalent thickness of a solid layer of fiber
FAW = reinforcement fiber areal weight
ρ_f = fiber density

- The fraction of fiber in a laminate is the thickness of this fiber layer divided by the total laminate thickness

$$FV = \frac{t_f}{CPT} \tag{2}$$

where

FV = fiber volume fraction
CPT = laminate cured ply thickness

- It follows that

$$FV = \frac{FAW}{\rho_f \times CPT} \tag{3}$$

and

$$FV_{normalizing} = \frac{FAW_{nominal}}{\rho_f \times CPT_{normalizing}} \tag{4}$$

and

$$FV_{specimen} = \frac{FAW_{specimen}}{\rho_f \times CPT_{specimen}} \tag{5}$$

where

$FV_{normalizing}$ = fiber volume fraction specified or chosen for normalizing

$FV_{specimen}$ = fiber volume fraction of the specimen

$FAW_{nominal}$ = nominal fiber areal weight from a material specification or other source

$FAW_{specimen}$ = specimen actual fiber areal weight

$CPT_{normalizing}$ = cured ply thickness corresponding to normalizing fiber volume fraction

$CPT_{specimen}$ = actual specimen ply thickness (specimen thickness divided by number of plies)

- Combining the previous two equations renders

$$\frac{FV_{normalizing}}{FV_{specimen}} = \frac{FAW_{nominal}}{FAW_{specimen}} \times \frac{CPT_{specimen}}{CPT_{normalizing}} \tag{6}$$

and since

$$Normalized\ Value = Test\ Value \times \frac{FV_{normalizing}}{FV_{specimen}} \tag{7}$$

$$Normalized\ Value = Test\ Value \times \frac{FAW_{nominal}}{FAW_{specimen}} \times \frac{CPT_{specimen}}{CPT_{normalizing}} \tag{8}$$

Assuming a negligible difference between the *FAW*, equation 8 may be rewritten as

$$Normalized\ Value = Test\ Value \times \frac{CPT_{specimen}}{CPT_{normalizing}} \tag{9}$$

5.2.2 Application of Normalization.

The methodology for practical application of normalization has been adopted from MIL-HDBK-17-1E, section 2.4.3.3. Fiber-dominated properties shall be normalized according to the procedure outlined in the previous section, with specific examples cited below.

Normalize:

- 0° (warp) tensile strength and modulus (fabric weave and unidirectional tape)
- 90° (fill) tensile strength and modulus (fabric weave only)
- 0° (warp) compressive strength and modulus (fabric weave and unidirectional tape)
- 90° (fill) compressive strength and modulus (fabric weave only)

Do not normalize:

- 90° tensile strength and modulus (unidirectional only)
- 90° compressive strength and modulus (unidirectional only)
- Interlaminar shear
- In-plane shear strength and modulus
- Short-beam strength
- Poisson's ratio

After normalizing, data scatter should reduce or remain the same. However, if data scatter increases significantly after normalizing, the reason should be investigated.

5.3 STATISTICAL ANALYSIS.

When compared to metallic materials, the base material properties for fiber-reinforced composite materials exhibit a high degree of variability. This variability is due to many factors including, but not limited to, raw material and prepreg manufacture, material handling, part fabrication techniques, ply-stacking sequence, environmental conditions, and testing techniques. In some cases, the variation in the defects or flaws associated with these factors is the apparent cause. The variability, which is directly related to the test procedures, has been minimized over the

years through research and standardization. Nevertheless, the cost of composite testing is relatively high. This, combined with additional testing due to the orthotropic nature of composite materials, has led to smaller data sets for a particular property than those produced for metallic materials. This necessitates the usage of advanced statistical techniques for determining reasonable design allowables for composites.

5.3.1 Methodology.

The statistical analyses and design-allowable generation for both A- and B-basis values may be performed using the methodology presented by Shyprykevich [4]. In this data reduction method, the data from all environments, batches, and panels are used jointly to obtain statistical information about the corresponding test condition and failure mode. This approach uses essentially small data sets to generate test condition statistics such as population variability factors and corresponding basis values for pooling of test results for a specific failure mode across all test environments. This section describes an overview of this methodology as applied to a design allowable generated using the testing procedures presented in the qualification plan. For additional information regarding this methodology or statistical analyses in general, the reader is referred to either Shyprykevich [4] or MIL-HDBK-17-1E, chapter 8.

The data reduction methodology presented in this section requires several underlying assumptions to generate a valid design allowable. By pooling the data sets in the analysis method, the variability across environments should be comparable, and the failure modes for each environment should not significantly change. The methodology presented here uses a normal distribution to analyze the data. If the assumption of normality is not acceptable, the Weibull distribution can be used as outlined by Shyprykevich [4]. It generally produces the most conservative basis values. If the variability or failure modes significantly change with environmental condition or if the assumption of normality is violated, other statistical methods in MIL-HDBK-17 should be used.

The methodology to produce a design allowable (based upon testing completed via section 4.5) is presented through a stepwise process, which assumes that all testing data for each condition and testing environment has been reduced and is in terms of failure stress. An assumption of normality is used in the method to reduce and model the behavior. The stepwise process then proceeds to determine a basis design-allowable value (A or B) as follows:

a. Normalize all relevant fiber-dominated data via the procedures presented in MIL-HDBK-17-1E, section 2.4.3 (which is also given in section 5.2). This normalization procedure will account for variations in the fiber volume fraction between individual specimens, panels, and batches of material.

b. For each environmental condition, check whether the different batches (subpopulations) of data are compatible, using the *k*-sample Anderson-Darling Test described in section 5.3.1.1.

c. For a single test condition (such as 0° compression strength), collect the data for each environmental condition being tested. The number of observations in each environmental

condition is n_j, where the subscript j represents the environments beings pooled. Calculate the sample mean $\bar{x}_j$ and sample standard deviation s_j for each environment via

$$\bar{x}_j = \frac{1}{n_j}\sum_{i=1}^{n_j} x_i \tag{10}$$

$$s_j^2 = \frac{1}{n_j - 1}\sum_{i=1}^{n_j} (x_i - \bar{x}_j)^2 \tag{11}$$

d. Each environmental grouping must be checked for any outliers, per section 5.3.1.2. If any outliers exist within any environmental grouping, the disposition of any outlier should be determined via the procedures given in section 5.3.1.2.1.

e. Check whether the assumption of normality is true for each environmental condition, per section 5.3.1.3. When checking population normality, engineering judgment should be applied to verify that the assumption of normality is not significantly violated. If the assumption of normality is significantly violated, other statistical models should be investigated to fit the data. As stated above, the Weibull distribution provides the most conservative basis values.

f. Check for equality of variances or coefficient of variations, as the data is normalized, between different environmental groupings, per section 5.3.1.4. If the variance of any environmental grouping is significantly different, as determined by the procedure described in section 5.3.1.4, other statistical methods in MIL-HDBK-17 should be used.

g. Normalize the data in each environment by dividing the individual strength by the mean strength for the corresponding environment. Normalizing will result in all data having a mean of 1.0. Pool all of the normalized data together from each environment into one data set.

In general, a coefficient of variation between 4% to 10% is typical of composite materials. Experiences with large data sets have shown that this range is representative of most composite material systems. Lower coefficients of variation may be caused by the specimen fabrication and testing by a single laboratory, while higher coefficients may point to a lack of material and processing control. In cases where the coefficients of variation of the pooled data set are higher or lower than this range, the reason for the higher or lower coefficient of variation should be investigated before determining design-allowable values from the pooled data set. The use of sample coefficient of variation of less than 4% to calculate allowables will result in values that are potentially unconservative. If the coefficient of variation of data for a given environment is less than 4%, the data can be transformed using the procedure described in section 5.3.1.5, such that the transformed data will have a coefficient of variation of 4%. The transformed data can then be normalized by proceeding with steps h through l.

h. For the pooled, normalized data set, calculate the number of samples N, the sample mean $\bar{x}_j$, and sample standard deviation s via equations 10 and 11. For the pooled data set, a

visual comparison of the best normal fit should be conducted, per section 5.3.1.3. For the distributional check of normality, engineering judgement should be applied to verify that the assumption of normality is not significantly violated. If the assumption of normality is significantly violated, the other statistical models should be investigated to fit the data. In general, the Weibull distribution provides the most conservative basis value.

i. Calculate the one-sided B- and A-basis tolerance factors for the normal distribution for each environment *j* that is based upon the number of samples in the pooled data set N and the number of samples in each environment n_j. The B-basis tolerance factor (number of standard deviations) $(k_B)_j$ may be approximated by [5]

$$(k_B)_j = z_B\sqrt{\frac{f}{Q}} + \sqrt{\frac{1}{c_B n_j} + \left(\frac{b_B}{2c_B}\right)^2} - \frac{b_B}{2c_B} \tag{12}$$

where n_j is the number of observations of the selected environment (a subset of N, the number of total pooled observations) and z_B is the standard normal random variable. In the case of a B-basis calculation, z_B is taken as 1.28115 (90% probability). The subscript *j* is used to indicate the tolerance factor for that specific environment. The coefficients b_B and c_B are given by the following relationships

$$b_B(f) = 1.1372\frac{1}{\sqrt{f}} - 0.49162\frac{1}{f} + 0.18612\frac{1}{f\sqrt{f}} \tag{13}$$

$$c_B(f) = 0.36961 + 0.0040342\frac{1}{\sqrt{f}} - 0.71750\frac{1}{f} + 0.19693\frac{1}{f\sqrt{f}} \tag{14}$$

where f = N-2 is the degrees of freedom for the variance. In the case $f \geq 3$, Q may be approximated by

$$Q = f - 2.327\sqrt{f} + 1.138 + 0.6057\frac{1}{\sqrt{f}} - 0.3287\frac{1}{f} \tag{15}$$

For f = 2, the exact value of Q may be used as Q = 0.05129. The above approximations are accurate within 1.2% of the tabulated values for B-basis calculations.

The A-basis tolerance factor, k_A may be approximated by

$$(k_A)_j = z_A\sqrt{\frac{f}{Q}} + \sqrt{\frac{1}{c_A n_j} + \left(\frac{b_A}{2c_A}\right)^2} - \frac{b_A}{2c_A} \tag{16}$$

where n_j is the number of observations of the selected environment (a subset of N, the number of total pooled observations) and z_A is the standard normal random variable. In the case of an A-basis calculation, z_A is taken as 2.32635 (99% probability). The subscript *j* is used to indicate the tolerance factor for that specific environment. The coefficients b_A and c_A are given by the following relationships

$$b_A(f) = 2.0643\frac{1}{\sqrt{f}} - 0.95145\frac{1}{f} + 0.51251\frac{1}{f\sqrt{f}} \tag{17}$$

$$c_A(f) = 0.36961 + 0.0026958\frac{1}{\sqrt{f}} - 0.65201\frac{1}{f} + 0.011320\frac{1}{f\sqrt{f}} \tag{18}$$

where f = N-2 is the degrees of freedom for the variance. In the case $f \geq 3$, Q may be approximated by

$$Q = f - 2.327\sqrt{f} + 1.138 + 0.6057\frac{1}{\sqrt{f}} - 0.3287\frac{1}{f} \tag{19}$$

For $f = 2$, the exact value of Q may be used as $Q = 0.05129$. The above approximations are accurate within 0.9% of the tabulated values for A-basis calculations.

Use steps j and k if the variances are determined to be statistically equal.

j. Calculate the normal distribution B- and A-basis allowable using the pooled mean, standard deviation and tolerance factors for each environment j via the equation

$$B_j = \bar{x} - (k_B)_j s \tag{20}$$

This number should essentially be a knockdown factor less than 1. The A-basis value for each environment may be obtained similarly by

$$A_j = \bar{x} - (k_A)_j s \tag{21}$$

k. Multiply the pooled basis values obtained in step j by the mean strength calculated for each environment obtained in step c. These values then become the basis values (A and B) for each individual environmental condition.

Use step l if the variances are determined to be significantly different.

l. Calculate the normal distribution B- and A-basis allowables using the mean strength, standard deviation, and tolerance factors separately for each environment. First check that the coefficient of variation for each environment, CoV_j, is greater than 4%. If the CoV_j is less than 4%, then recalculate the standard deviation for that environment using $s_j = 0.04\overline{x_j}$. Calculate the basis values using the following equations

$$B_j = \bar{x}_j - (k_B)_j s_j \tag{22}$$

$$A_j = \bar{x}_j - (k_A)_j s_j \tag{23}$$

A flow chart depicting this stepwise procedure is shown in figure 19. An example of this procedure is given in section 5.3.2.

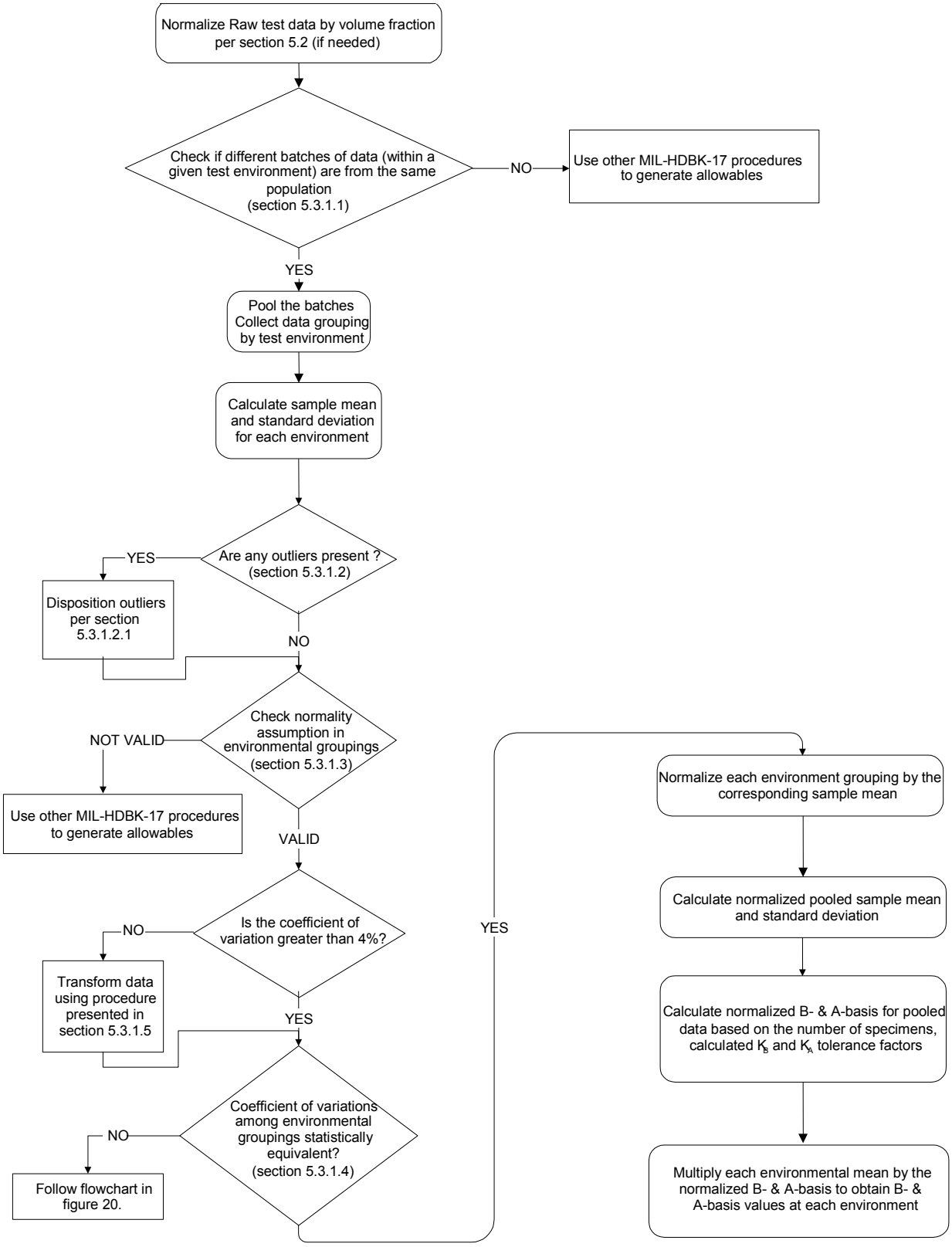


FIGURE 19. STEPWISE DATA REDUCTION PROCEDURE FOR DESIGN-ALLOWABLE GENERATION

5.3.1.1 Compatibility of Batches: *k*-sample Anderson Darling Test.

The *k*-sample Anderson-Darling test, as described in MIL-HDBK-17, section 8.3.2.2, is a nonparametric statistical procedure that tests the hypothesis that the populations from which two or more groups (batches) of data were drawn are identical. The test requires that each group be an independent random sample from a population.

Let x_{ij} be the j^{th} observation (data) ($j = 1,\ldots,n_i$) of the i^{th} group (batch) ($i=1,..,k$), where k is the total number of batches and n_i is the total number of observations in the i^{th} batch. The total number of observations is $n = n_1 + n_2 + \ldots + n_k$. The distinct values in the combined data set, ordered from smallest to largest, is denoted $z_{(1)}, z_{(2)}, \ldots, z_{(L)}$, where L will be less than n if there are tied observations.

The *k*-sample Anderson Darling statistic is given by

$$ADK = \frac{n-1}{n^2(k-1)} \sum_{i=1}^{k} \left[\frac{1}{n_i} \sum_{j=1}^{L} h_j \frac{(nF_{ij} - n_i H_j)^2}{H_j(n - H_j) - nh_j/4} \right] \tag{24}$$

where

h_j = the number of values in the combined samples equal to $z_{(j)}$

H_j = the number of values in the combined samples less that $z_{(j)}$ plus one half the number of values in the combined samples equal to $z_{(j)}$

F_{ij} = the number of values in the i^{th} group (batch) which are less that $z_{(j)}$ plus one half the number of values in this group which are equal to $z_{(j)}$

Under the hypothesis of no difference in the populations, the mean and variance of *ADK* are approximately 1 and

$$\sigma_n^2 = Var(ADK) = \frac{an^3 + bn^2 + cn + d}{(n-1)(n-2)(n-3)(k-1)^2} \tag{25}$$

with

$$\begin{aligned} a &= (4g-6)(k-1) + (10-6g)S \\ b &= (2g-4)k^2 + 8Tk + (2g - 14T - 4)S - 8T + 4g - 6 \\ c &= (6T + 2g - 2)k^2 + (4T - 4g + 6)k + (2T - 6)S + 4T \\ d &= (2T + 6)k^2 - 4Tk \end{aligned} \tag{26}$$

where

$$S = \sum_{i=1}^{k} \frac{1}{n_i} \tag{27}$$

$$T = \sum_{i=1}^{n-1} \frac{1}{i} \tag{28}$$

$$g = \sum_{i=1}^{n-2} \sum_{j=i+1}^{n-1} \frac{1}{(n-1)j} \tag{29}$$

If the critical value

$$ADC = 1 + \sigma_n \left[1.645 + \frac{0.678}{\sqrt{k-1}} - \frac{0.362}{k-1} \right] \tag{30}$$

is less than the test statistic *ADK*, then one can conclude (with a 5 percent risk of being in error) that the groups were drawn from different populations. Otherwise, the hypothesis that the groups were selected from identical populations is not rejected.

The critical value *ADC*, can be obtained at different α levels using the following equation [6].

$$ADC(\alpha) = 1 + \sigma_n \left[b_0 + \frac{b_1}{\sqrt{k-1}} + \frac{b_2}{k-1} \right]$$

where the constants b_0, b_1, and b_2 for different α can be selected from the following.

α	b_0	b_1	b_2
0.252	0.675	-0.245	-0.105
0.10	1.281	0.250	-0.305
0.05	1.645	0.678	-0.362
0.025	1.960	1.149	-0.391
0.01	2.326	1.822	-0.396

5.3.1.2 Checking for Outliers.

5.3.1.2.1 Test for Outliers.

Once the strength data is generated for each testing condition, the data should be screened for outliers, since these values can have a substantial influence on the statistical analysis. This screening may be done visually using graphical plots of the data as well as the quantitative procedure outlined below, which is taken from MIL-HDBK-17, section 8.3.3. The data used for the screening should be checked for outliers in both raw-grouped data (by environment) as well as the normalized pooled data set.

The Maximum Normed Residual (MNR) method, as suggested by MIL-HDBK-17, is used for detecting outliers. The MNR test declares a value to be an outlier if it has an absolute deviation

from the sample mean that, when compared to the sample standard deviation, is too large to be due to chance. This method can only detect one outlier at a time from a selected group or subgroup; hence, once an outlier is detected, the outlier must be dispositioned (see section 5.3.1.2.2) and the analysis rerun to check for additional outliers.

Let $x_1, x_2, \ldots x_n$ denote the data values in the sample of size n, and let $\bar{x}$ and s be the sample mean and standard deviation defined previously for the normal distribution. The MNR statistic is the maximum absolute deviation, from the sample mean, divided by the sample deviation

$$MNR = \max_i \frac{\left| x_i - \bar{x} \right|}{s}, \quad i = 1,2,\ldots,n \tag{31}$$

The value obtained from this equation is compared to the critical value for the sample size n taken from table 7. If the calculated MNR is smaller than the critical value, then no outliers are detected in the sample. If the MNR value is greater than the critical value, the data value associated with the largest value of $\left|x_i - \bar{x}\right|$ is declared to be an outlier. If an outlier is detected, the disposition of the outlier should be investigated via the procedure described in section 5.3.1.2.2.

TABLE 7. CRITICAL VALUES

n	CV	n	CV	n	CV	n	CV	n	CV
-	-	41	3.047	81	3.311	121	3.448	161	3.539
-	-	42	3.057	82	3.315	122	3.451	162	3.541
3	1.154	43	3.067	83	3.319	123	3.453	163	3.543
4	1.481	44	3.076	84	3.323	124	3.456	164	3.545
5	1.715	45	3.085	85	3.328	125	3.459	165	3.547
6	1.887	46	3.094	86	3.332	126	3.461	166	3.549
7	2.020	47	3.103	87	3.336	127	3.464	167	3.551
8	2.127	48	3.112	88	3.340	128	3.466	168	3.552
9	2.215	49	3.120	89	3.344	129	3.469	169	3.554
10	2.290	50	3.128	90	3.348	130	3.471	170	3.556
11	2.355	51	3.136	91	3.352	131	3.474	171	3.558
12	2.412	52	3.144	92	3.355	132	3.476	172	3.560
13	2.462	53	3.151	93	3.359	133	3.479	173	3.561
14	2.507	54	3.159	94	3.363	134	3.481	174	3.563
15	2.548	55	3.166	95	3.366	135	3.483	175	3.565
16	2.586	56	3.173	96	3.370	136	3.486	176	3.567
17	2.620	57	3.180	97	3.374	137	3.488	177	3.568
18	2.652	58	3.187	98	3.377	138	3.491	178	3.570
19	2.681	59	3.193	99	3.381	139	3.493	179	3.572
20	2.708	60	3.200	100	3.384	140	3.495	180	3.574
21	2.734	61	3.206	101	3.387	141	3.497	181	3.575
22	2.758	62	3.212	102	3.391	142	3.500	182	3.577
23	2.780	63	3.218	103	3.394	143	3.502	183	3.579
24	2.802	64	3.224	104	3.397	144	3.504	184	3.580
25	2.822	65	3.230	105	3.401	145	3.506	185	3.582
26	2.841	66	3.236	106	3.404	146	3.508	186	3.584
27	2.859	67	3.241	107	3.407	147	3.511	187	3.585
28	2.876	68	3.247	108	3.410	148	3.513	188	3.587
29	2.893	69	3.252	109	3.413	149	3.515	189	3.588
30	2.908	70	3.258	110	3.416	150	3.517	190	3.590
31	2.924	71	3.263	111	3.419	151	3.519	191	3.592
32	2.938	72	3.268	112	3.422	152	3.521	192	3.593
33	2.952	73	3.273	113	3.425	153	3.523	193	3.595
34	2.965	74	3.278	114	3.428	154	3.525	194	3.566
35	2.978	75	3.283	115	3.431	155	3.527	195	3.598
36	2.991	76	3.288	116	3.434	156	3.529	196	3.599
37	3.003	77	3.292	117	3.437	157	3.531	197	3.601
38	3.014	78	3.297	118	3.440	158	3.533	198	3.603
39	3.025	79	3.302	119	3.442	159	3.535	199	3.604
40	3.036	80	3.306	120	3.445	160	3.537	200	3.606

5.3.1.2.2 Dispositioning of Outliers.

The rationale for dispositioning of outliers detected in the data set is taken from MIL-HDBK-17E, section 2.4.4 and is primarily based upon engineering judgement so that outliers that should be retained are not casually discarded and those that should be deleted are not retained. The rationale presented attempts to separate variability apparent in the data that does not exist from material, processing parameter, or environmental variability. These types of variability should be reflected in the data set and should be represented in the finalized basis value. Variability, which exists from other sources such as inferior specimen fabrication, processing parameters, which fall outside the control limits, test fixture or machine deficiencies, or a number of other factors both detectable and undetectable, may produce outliers in the data set and cause an unnecessary statistical penalty in the basis value. The purpose of this section is to provide some guidance to retain or delete the detected outliers.

When an outlier is detected, the first action should be to identify the cause through physical evidence. The following list is taken from MIL-HDBK-17E to give some examples of conditions that could be used as the basis for discarding outlier data.

a. The material was out of specification.

b. One or more panel or specimen fabrication parameters were outside the specified tolerances.

c. Test specimen dimensions or orientation were outside the specified tolerance range.

d. A defect was detected in the test specimen.

e. An error was made in the specimen preconditioning (or conditioning parameters were out of specified tolerance ranges).

f. The test machine and/or test fixture was improperly set up in some specific and identifiable manner.

g. The test specimen was improperly installed in the test fixture in some specific and identifiable manner.

h. Test parameters (speed, temperature, etc.) were outside the specified range.

i. The test specimen slipped in the grips during the test.

j. The test specimen failed in a mode other than the mode under test (loss of tabs, unintended bending, failure outside the gage section, etc.).

k. A test was purposely run to verify conditions suspected to have produced outlier data.

l. Data were improperly normalized.

m. A different failure mode that is still in the gage section (most specimens failed in interlaminar shear but one failed due to fiber matrix interface).

If the search for physical causes has been completed without success, engineering judgement should be used in assessing the outlier data. This section provides some guidelines in case no physical determination exists but is not meant to provide rulings when data should be retained or deleted. In most cases, if the outlier's inclusion in the data set does not significantly affect calculated basis values, the outlier should simply be retained without further consideration.

In the case of a detected outlier, given the stepwise process presented in section 5.3.1, two possibilities exist with respect to the corresponding data set (either environmentally grouped or pooled data): the outlier may be high or low. If an outlier (high or low) is detected with respect to the environmental grouping of the data as described in section 5.3.1, engineering judgement should be used to disposition the outlier.

Clearly, the easiest case to examine is when a high outlier is detected. For a high outlier, engineering judgement should be used to consider whether the outlier is within the range of material capability. If the outlier is clearly outside the range of the material capability, the outlier should be deleted from the data set (particularly in the case of pooled data). If the high outlier is within the range of material capability, the outlier should be retained.

In the case of a low outlier without physical evidence, in general, the data should be retained. If the low outlier is seen to penalize the basis value severely, the FAA ACO should be consulted to discuss deletion of the outlier and possible causes for the outlier. In this case, additional testing may be required in order to substantiate this outlier deletion.

The original equipment manufacturer (OEM) must take the responsibility to take real root cause corrective action to prevent the detected occurrence from affecting future production runs (e.g., if, as a result of the investigation of outliers, it is determined that the fiber sizing was out of date, the OEM must ensure that the problem will not reoccur in production). This may require changes in the quality control requirements or in the material specifications.

5.3.1.3 Normality Check.

The normality of a given set of data may be verified visually by comparing the data distribution with the best-fit normal curve and using engineering judgement to check the fit of the distribution. The normality of the grouped data (data from different batches for the same test environment) is checked as follows.

The data from different batches are grouped together and sorted in an ascending order. The probability of survival at each value of the data is

$$\textit{Probability of survival at } x_i = 1 - \frac{i}{n+1} \tag{32}$$

where

n = total number of data points
i = rank of the x_i data value in the sorted list
x_i = data value of rank i in the sorted list

The mean and standard deviation for the grouped data are then computed using the rudimentary statistical techniques presented in 5.3.1 c. The mean and the standard deviation are the parameters that define the normal distribution. Using this value of the mean and standard deviation, the probability of survival is computed at each data value using a standard normal distribution. The data values are then plotted against the respective probability of survival obtained using equation 32 and the normal distribution. The data are compared visually and the normality of the data is evaluated using engineering judgement.

The grouped data are then normalized with respect to the mean of the individual groups. The normalized groups are then pooled together and sorted and arranged in an ascending order. The probability of survival at each pooled normalized data value is computed using equation 32. The mean and the standard deviation of the pooled normalized data are then used to compute the probability of survival using the standard normal distribution. The normalized data values are then plotted against their respective probability of survival obtained using equation 32 and the normal distribution. The data is compared visually and the normality of the data is evaluated using engineering judgement.

Another check for normality may be performed using the Anderson-Darling test (see MIL-HDBK-17-1E, section 8.3.4.2). This test generates an observed significance level (OSL), which measures the probability of observing an Anderson-Darling statistic at least as extreme as the value calculated if in fact the data are from a normal distribution. If the OSL is ≤ 0.05, one may conclude (at a 5 percent risk of being in error) that the population is not normally distributed. Otherwise, the hypothesis that the population is normally distributed is not rejected.

5.3.1.4 Equality of Coefficient of Variations.

The equality of the coefficient of variations between different grouped data must also be checked using Levene's test (MIL-HDBK-17-1E, section 8.3.5.2.1). This test determines whether the sample coefficient of variations for k groups differ significantly, which is an important assumption that must be validated to substantiate the pooling across environments. The following steps are involved in performing this test.

a. The normalized data is transformed according to

$$w_{ij} = | x_{ij} - \tilde{x}_i | \tag{33}$$

where

w_{ij} = the transformed value of the jth normalized data point in the ith group
x_{ij} = the normalized original jth data point in the ith group
$\tilde{x}_i$ = the median of the ith group

b. Perform an F-test (MIL-HDBK-17-1E, section 8.3.5.2.2) and compute the F statistic. The F statistic is given by

$$F = \frac{\sum_{i=1}^{k} n_i \left(\overline{w}_i - \overline{w}\right)^2 / (k-1)}{\sum_{i=1}^{k}\sum_{j=1}^{n_i} \left(w_{ij} - \overline{w}_i\right) / (n-k)} \tag{34}$$

where

$\overline{w}_i$ = the average of the n_i values in the ith group
$\overline{w}$ = the average of all the n observations (i.e., of the pooled data)
k = the number of groups
n_i = the number of observations in the ith group
n = the total number of observations

c. The F statistic obtained above is compared with the (1-α) quantile of the F-distribution having k-1 numerator and n-k denominator degrees of freedom. A typical value of $\alpha = 0.05$ is used. This statistic from the F-distribution is termed as $F_{critical}$. The value for $F_{critical}$ may be obtained using an approximate formula

$$F_{critical} = \exp\left[2\,\delta\left\{1 + \frac{z^2-1}{3} - \frac{4\sigma^2}{3}\right\} + 2\,\sigma\, z\sqrt{1 + \frac{\sigma^2\left(z^2-3\right)}{6}}\right] \tag{35}$$

where

$$\delta = 0.5\left\{\frac{1}{\gamma_2 - 1} - \frac{1}{\gamma_1 - 1}\right\} \tag{36}$$

$$\sigma^2 = 0.5\left\{\frac{1}{\gamma_2 - 1} + \frac{1}{\gamma_1 - 1}\right\} \tag{37}$$

z = 1.645
γ_1 = numerator degrees of freedom (k-1)
γ_2 = denominator degrees of freedom (n-k)

d. If the computed F-statistic is less than $F_{critical}$, the coefficient of variations of the groups are not significantly different.

e. It should be noted that other α values less than 0.05 may also be used to assess the equality of coefficient of variations at different environments (see step c.). These different values of α can be useful in establishing engineering judgement as to the degree

of variance inequality and suggest possible problems with obtaining a representative pooled data set. If the coefficient of variations are not equal at the 0.05 level, engineering judgement should be used to determine the degree of inequality. Figure 20 provides guidance in the situation of unequal coefficient of variations and describes procedures to obtain a conservative design allowable. Note that these procedures must be combined with engineering judgement and that the failure modes must remain the same across environments. In general, if the coefficient of variations are significantly different at the 0.01 level, the reason should be investigated and some corrective action may be required.

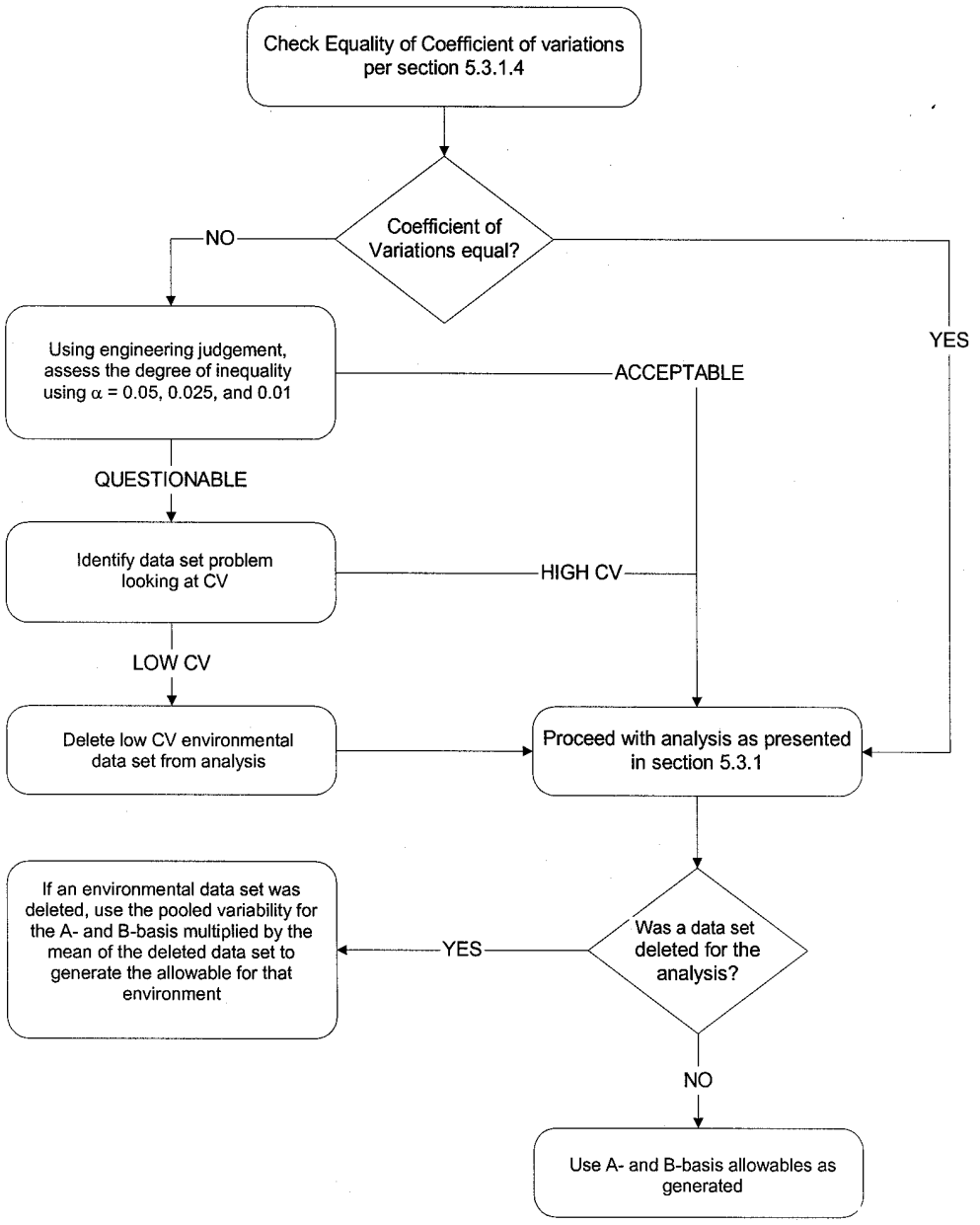


FIGURE 20. PROCEDURES TO OBTAIN DESIGN ALLOWABLES IN THE CASE OF INEQUALITY OF COEFFICIENT OF VARIATIONS

5.3.1.5 Procedure for Transforming Coefficient of Variations of Test Samples.

A simple procedure for modifying the variance of a test sample to any desired value is proposed. Consider a test sample x_i of n specimens with an average value of $\bar{x}$. Let the variance of this sample be CV which is given by

$$CV = \sqrt{\frac{\sum_{i=1}^{n}(x_i - \bar{x})^2}{n-1}} \tag{38}$$

Let the desired variance of the sample be CV^*. Consider a transformation of the form

$$x_i^* = x_i + \alpha(x_i)\Delta \tag{39}$$

where x_i^* is the transformed data, Δ is a constant and, $\alpha(x_i)$ is a weighting function. Let the weighting function be

$$\alpha(x_i) = (x_i - \bar{x}) \tag{40}$$

The new variance for the transformed data is then given by

$$CV^* = \sqrt{\frac{\sum_{i=1}^{n}(x_i^* - \bar{x}^*)^2}{n-1}} \tag{41}$$

where $\bar{x}^*$ is the average value of the transformed sample. Substituting equations 39 and 40 into equation 41 one can obtain

$$CV^* = \sqrt{\frac{\sum_{i=1}^{n}\left[\{x_i + (x_i - \bar{x})\Delta\} - \bar{x}^*\right]^2}{n-1}} \tag{42}$$

If one further let $\bar{x}^* = \bar{x}$, equation 42 reduces to

$$CV^* = \sqrt{\frac{(1+\Delta)^2\sum_{i=1}^{n}(x_i - \bar{x})^2}{n-1}} \tag{43}$$

which gives

$$\Delta = \frac{CV^*}{CV} - 1 \tag{44}$$

Thus, a sample with a known variance *CV* can be transformed using equation 39 to obtain the desired variance *CV**. The constant for transformation, Δ, can be calculated using equation 44. The transformation for a typical data set with a *CV* of 1.8% is illustrated using a probability of survival plot shown in figure 21. It can be observed that the original normal curve has been rotated and stretched due to the transformation.

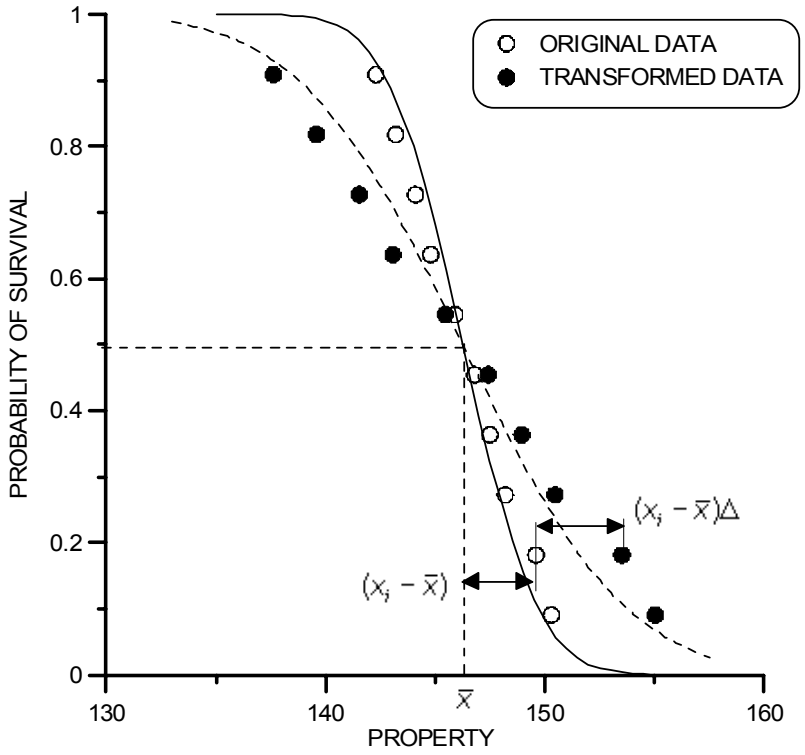


FIGURE 21. ORIGINAL AND TRANSFORMED DATA POINTS

5.3.2 Example of B-Basis Calculation.

This section illustrates the calculation of basis values according to the stepwise procedure presented in section 5.3.1 using example mechanical property data (in this specific example, for compression) that was generated according to the procedures outlined in this document. The example data represent testing at all environments, per reduced sampling in table 4, and already have been normalized to fiber volume fraction by the procedures delineated in section 5.2. The resulting mechanical property data (in ksi) are shown in table 8. The sample mean, standard deviation, coefficient of variation, and number of observations are shown at the bottom of each column of data that is grouped by testing environment.

The next step in the data reduction procedure is to check whether the different batches of data at each of the test environments belong to identical populations using the *k*-sample Anderson-Darling test. For the above data set, the three batches of data for the ETW test environment do not pass the *k*-sample Anderson-Darling test. The value of the test statistic (*ADK*) is 2.258, while the critical value (*ADC*) at $\alpha = 0.05$ is 1.917, indicating that the three batches of data do not belong to identical populations (with 5% risk of being in error). However, with $\alpha = 0.01$, the

critical value will be 2.613, indicating compatibility of the three batches of data (with 1% risk of being in error). In practice, if the batches of data are deemed unfit to be grouped due to significant batch-to-batch variability, the method described for structured data sets in section 8.2.3 of MIL-HDBK-17-1E must be employed for generating the basis values. In this example, different batches of data under the ETW test environment will, however, be grouped for further analysis.

TABLE 8. EXAMPLE DATA SET FOR EACH TESTING ENVIRONMENT PER TABLE 4

CTD			RTD			ETD			ETW		
Batch	Panel	Data	Batch	Panel	Data	Batch	Panel	Data	Batch	Panel	Data
1	1	103.260	1	1	94.395	1	1	72.712	1	1	55.809
1	1	104.281	1	1	101.854	1	1	81.884	1	1	55.853
1	1	102.650	1	1	102.363	1	1	68.822	1	1	58.091
1	2	111.336	1	2	101.442	1	2	78.771	1	2	63.587
1	2	102.967	1	2	96.687	1	2	84.838	1	2	60.137
1	2	108.615	1	2	104.112	1	2	79.906	1	2	56.951
2	3	113.210	2	3	102.360	2	3	58.500	2	3	62.986
2	3	111.150	2	3	96.684	2	3	83.108	2	3	67.795
2	3	102.320	2	3	97.435	2	3	80.162	2	3	64.954
2	4	106.580	2	4	95.267	2	4	80.815	2	4	61.094
2	4	102.360	2	4	104.483	2	4	84.690	2	4	65.736
2	4	101.650	2	4	98.908	2	4	91.886	2	4	61.769
3	5	112.150	3	5	93.750	3	5	76.109	3	5	62.099
3	5	114.120	3	5	89.360	3	5	77.838	3	5	60.080
3	5	104.560	3	5	93.860	3	5	93.304	3	5	59.553
3	6	108.290	3	6	95.519	3	6	73.745	3	6	66.199
3	6	107.630	3	6	97.085	3	6	84.229	3	6	56.975
3	6	100.960	3	6	103.260	3	6	71.684	3	6	60.037
AVG	:	106.56	AVG	:	98.27	AVG	:	78.50	AVG	:	61.09
STD	:	4.37	STD	:	4.29	STD	:	7.51	STD	:	3.62
CV%	:	4.10	CV%	:	4.36	CV%	:	9.57	CV%	:	5.92
n	:	18	n	:	18	n	:	18	n	:	18

The next step in the data reduction procedure is to check the individually grouped environmental data for any outliers that may exist. This procedure calculates the *MNR* statistic using equation 29 for each environmental condition individually (which is based upon the mean and standard deviation) and compares these values with the critical values obtained from table 7 (which is based upon the number of observations). Table 9 shows the resulting *MNR* statistic for each observation along with the critical value taken from table 7. An outlier is detected if the calculated *MNR* statistic is greater than the critical value given at the bottom of each column. As seen from table 9, an outlier does exist in the ETD test data for the stress of 58.500 ksi. The calculated test statistic in this case is 2.663, which is greater than the critical value of 2.652 based upon 18 observations. For the purpose of this example, the low outlier will be retained in the data set at this point.

TABLE 9. CALCULATED *MNR* STATISTIC FOR THE ENVIRONMENTALLY GROUPED DATA

CTD		RTD		ETD		ETW	
Raw Data	*MNR*	Raw Data	*MNR*	Raw Data	*MNR*	Raw Data	*MNR*
103.260	0.756	94.395	0.903	72.712	0.771	55.809	1.461
104.281	0.522	101.854	0.837	81.884	0.451	55.853	1.448
102.650	0.895	102.363	0.955	68.822	1.289	58.091	0.830
111.336	1.093	101.442	0.740	78.771	0.036	63.587	0.689
102.967	0.823	96.687	0.369	84.838	0.844	60.137	0.265
108.615	0.470	104.112	1.363	79.906	0.187	56.951	1.145
113.210	1.523	102.360	0.955	58.500	2.663	62.986	0.523
111.150	1.051	96.684	0.369	83.108	0.614	67.795	1.851
102.320	0.971	97.435	0.194	80.162	0.221	64.954	1.066
106.580	0.004	95.267	0.700	80.815	0.308	61.094	0.000
102.360	0.962	104.483	1.450	84.690	0.824	65.736	1.282
101.650	1.124	98.908	0.149	91.886	1.782	61.769	0.186
112.150	1.280	93.750	1.054	76.109	0.318	62.099	0.277
114.120	1.731	89.360	2.078	77.838	0.088	60.080	0.280
104.560	0.458	93.860	1.028	83.304	0.640	59.553	0.426
108.290	0.396	95.519	0.641	73.745	0.633	66.199	1.410
107.630	0.245	97.085	0.276	84.229	0.763	56.975	1.138
100.960	1.282	103.260	1.164	71.684	0.908	60.037	0.292
Critical Value 2.652		Critical Value 2.652		Critical Value 2.652		Critical Value 2.652	

After the data is checked for outliers, a visual check should be performed on the environmentally grouped data to validate the assumption of normality, following the procedures outlined in section 5.3.1.2. Figure 22 shows the data from table 8 plotted against the standard normal curves for each environment tested. As shown in the figure, the normal model appears to closely represent the data across all represented environments and does not appear to cause any significant engineering concerns. This plot may also be graphically represented on a probability scale, which reduces the distribution to a straight line. Probability plotting is a graphical method for determining whether sample data conforms to a hypothesized normal distribution based on a subjective visual examination of the data. If the normal distribution adequately describes the data, the plotted points will fall approximately on a straight line.

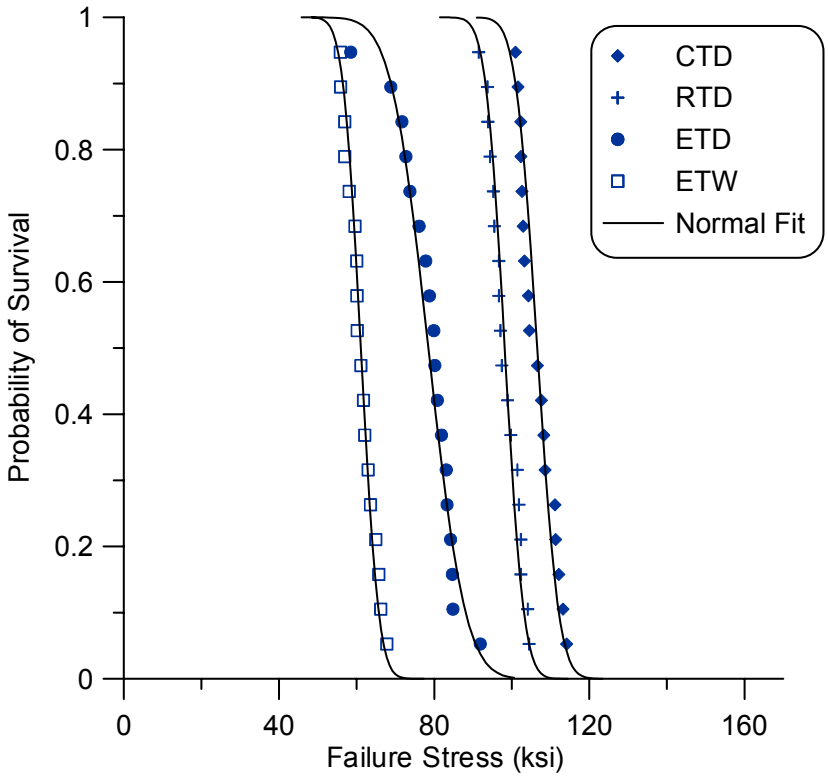


FIGURE 22. NORMALIZED FIT OF EXPERIMENTAL DATA FOR EACH ENVIRONMENT

After ascertaining the normality of the environmentally grouped data, the data groups should be checked for equality of coefficient of variations across environments, using the procedures of section 5.3.1.4. The Levene's test described in section 5.3.1.4, gives an F statistic value of 2.38 while the critical value $F_{critical} = 2.899$ at a significance level of 5%. Since the calculated value is less than the critical value, $F_{critical}$, the test indicates that the coefficient of variations are statistically equal for this set of data. If the coefficient of variations had been determined to be significantly different, the procedure described in figure 20 may be followed.

The next step in the data reduction process is the pooling of data across environments. The data from each environment is normalized using the sample mean from each environmental condition. Table 10 shows the resulting normalized data, pooling all environments together. As seen from this method, all strength values then take on a normalized value in the neighborhood of one. Also shown in table 10 are the resulting mean, standard deviation, coefficient of variation, and number of observations.

TABLE 10. RESULTING POOLED DATA AFTER NORMALIZATION PROCEDURE

CTD			RTD			ETD			ETW		
Batch	Panel	Data	Batch	Panel	Data	Batch	Panel	Data	Batch	Panel	Data
1	1	0.969	1	1	0.961	1	1	0.926	1	1	0.913
1	1	0.979	1	1	1.036	1	1	1.043	1	1	0.914
1	1	0.963	1	1	1.042	1	1	0.877	1	1	0.951
1	2	1.045	1	2	1.032	1	2	1.003	1	2	1.041
1	2	0.966	1	2	0.984	1	2	1.081	1	2	0.984
1	2	1.019	1	2	1.059	1	2	1.018	1	2	0.932
2	3	1.062	2	3	1.042	2	3	0.745	2	3	1.031
2	3	1.043	2	3	0.984	2	3	1.059	2	3	1.110
2	3	0.960	2	3	0.992	2	3	1.021	2	3	1.063
2	4	1.000	2	4	0.969	2	4	1.029	2	4	1.000
2	4	0.961	2	4	1.063	2	4	1.079	2	4	1.076
2	4	0.954	2	4	1.007	2	4	1.171	2	4	1.011
3	5	1.052	3	5	0.954	3	5	0.970	3	5	1.016
3	5	1.071	3	5	0.909	3	5	0.992	3	5	0.983
3	5	0.981	3	5	0.955	3	5	1.061	3	5	0.975
3	6	1.016	3	6	0.972	3	6	0.939	3	6	1.084
3	6	1.010	3	6	0.988	3	6	1.073	3	6	0.933
3	6	0.947	3	6	1.051	3	6	0.913	3	6	0.983

Pooled Average:	1.000
Pooled Standard Deviation:	0.062
Coefficient of Variation:	6.237
Number of Observations:	72

Using the pooled data, figure 23 shows the visual check of the normal distribution with respect to the pooled data. As shown in figure 23, the normal model appears to closely represent the data across all pooled data and does not appear to cause any significant engineering concerns.

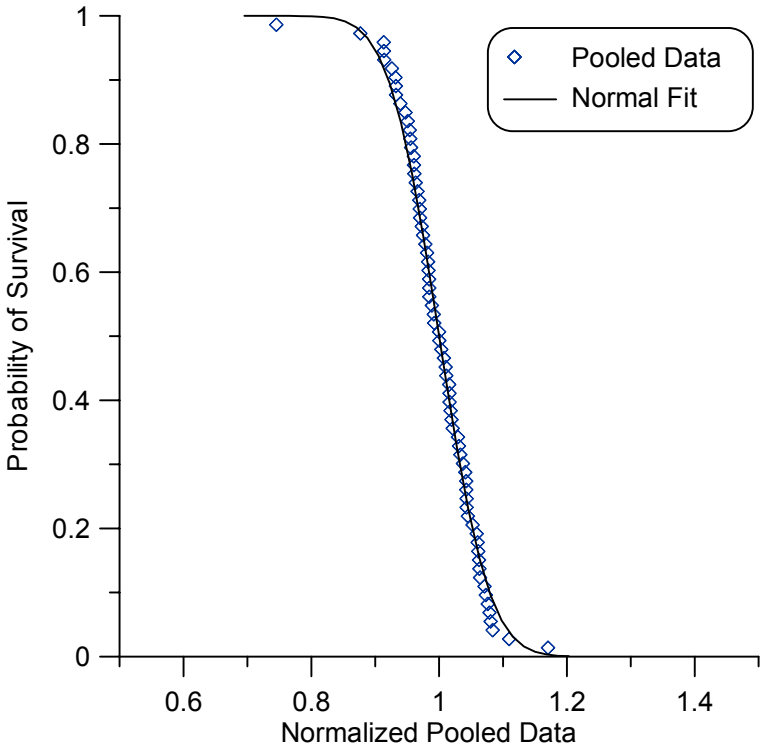


FIGURE 23. NORMALIZED FIT OF POOLED DATA

After the pooled data has been collected, the pooled sample mean and standard deviation may be computed (see table 10). Using these values, the B- and A-basis values may be calculated for the pooled data. Using equations 12 through 19, the one-sided tolerance limits may be calculated for each environmental condition. The values of these tolerance limits for each environment are

Statistic	CTD	RTD	ETD	ETW
k_B	1.7426	1.7426	1.7426	1.7426
k_A	2.8908	2.8908	2.8908	2.8908

which, combined with the pooled normal sample mean and standard deviation, yield B and A knockdown values for each via equations 20 and 21

Statistic	CTD	RTD	ETD	ETW
B_{normal}	0.8913	0.8913	0.8913	0.8913
A_{normal}	0.8197	0.8197	0.8197	0.8197

Once these values are obtained, the A- and B-basis for each environmental condition may be obtained using the mean of each environment and the pooled A- and B-basis values. Simple multiplication yields the A- and B-basis values for each environment as

Statistic	CTD	RTD	ETD	ETW
A-basis value	87.35	80.55	64.35	50.08
B-basis value	94.98	87.59	69.97	54.46

It should be noted that even though A-basis numbers were calculated for this example, reduced sampling is not recommended for A-basis calculations. For a more robust A-basis allowable, the number of specimens can be increased to those given in table 3.

5.4 MATERIAL PERFORMANCE ENVELOPE AND INTERPOLATION.

Using the B-basis numbers generated in the previous example, a material performance envelope may be generated for the example material system by plotting these values as a function of temperature. Figure 24 shows the material performance envelope using the B-basis values generated in the previous example.

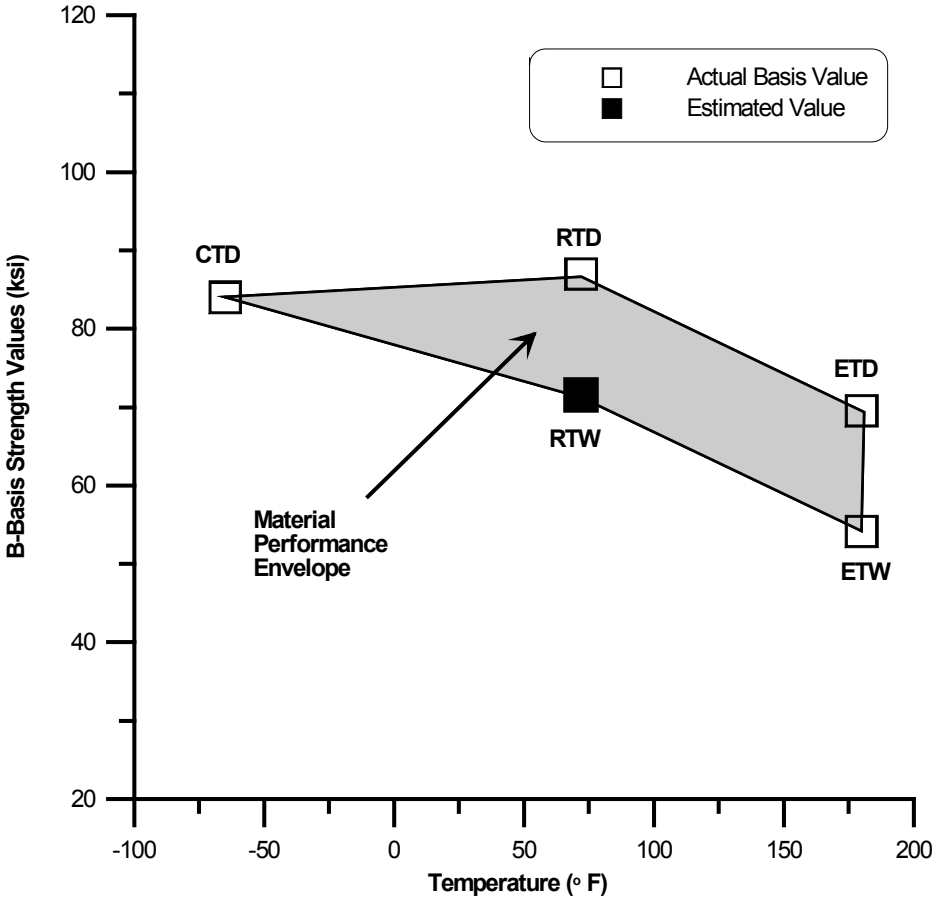


FIGURE 24. MATERIAL PERFORMANCE ENVELOPE

Since each specific aircraft application of the qualified material may have different material operational limits (MOL) than those tested in the material qualification (which is usually the upper limit of the material), some applications may require a reduced MOL. In this case, simple linear interpolation may be used to obtain the corresponding basis values at the new application MOL.

This interpolation may be accomplished using the following simple relationships assuming $T_{RTD} < T_{MOL} < T_{ETD}$.

For the corresponding *MOL* dry basis value, the interpolated basis value using the qualification data is

$$B_{MOL} = B_{RTD} - \frac{(B_{RTD} - B_{ETD})(T_{RTD} - T_{MOL})}{(T_{RTD} - T_{ETD})} \tag{45}$$

where

B_{MOL} = new application basis value interpolated to T_{MOL}
B_{RTD} = basis RTD strength value
B_{ETD} = basis ETD strength value
T_{RTD} = RTD test temperature
T_{ETD} = ETD test temperature
T_{MOL} = new application MOL temperature

For the corresponding *MOL* wet basis value, an estimated RTW value must be calculated. This may be accomplished by the simple relation

$$B_{RTW} = B_{RTD} - (B_{ETD} - B_{ETW}) \tag{46}$$

The interpolated wet basis value using the qualification data may then be obtained by

$$B_{MOL} = B_{RTW} - \frac{(B_{RTW} - B_{ETW})(T_{RTW} - T_{MOL})}{(T_{RTW} - T_{ETW})} \tag{47}$$

where

B_{MOL} = new application basis value interpolated to T_{MOL}
B_{RTW} = estimated basis RTW strength value
B_{ETW} = basis ETW strength value
T_{RTW} = RTW (i.e., RTD) test temperature
T_{ETW} = ETW test temperature
T_{MOL} = new application MOL temperature

These equations may also be used for interpolated mean strengths as well as A-basis values with the appropriate substitutions. It should be noted that because unforeseen material property drop-offs with respect to temperature and environment can occur, extrapolation to a higher MOL should not be attempted without additional testing and verification. In addition, the interpolation equations shown above are practical for materials obeying typical mechanical behavior. In most cases, some minimal amount of testing may also be required to verify the interpolated values.

Using the basis values obtained in the previous example, presented in section 5.3.2, this section provides an example of linear interpolations to a specific application environment less than the tested upper material limit used in qualification. Assuming a specific application environment of 150°F, figure 25 depicts the linear interpolation of the B-basis design allowable to this environment. Using equations 46 and 47 along with the nominal testing temperatures (see table 4), the interpolated basis values at 150°F become

$$\text{ETD} \quad : \quad B_{MOL} = 75.765 \text{ ksi}$$

$$\text{ETW} \quad : \quad B_{MOL} = 58.875 \text{ ksi}$$

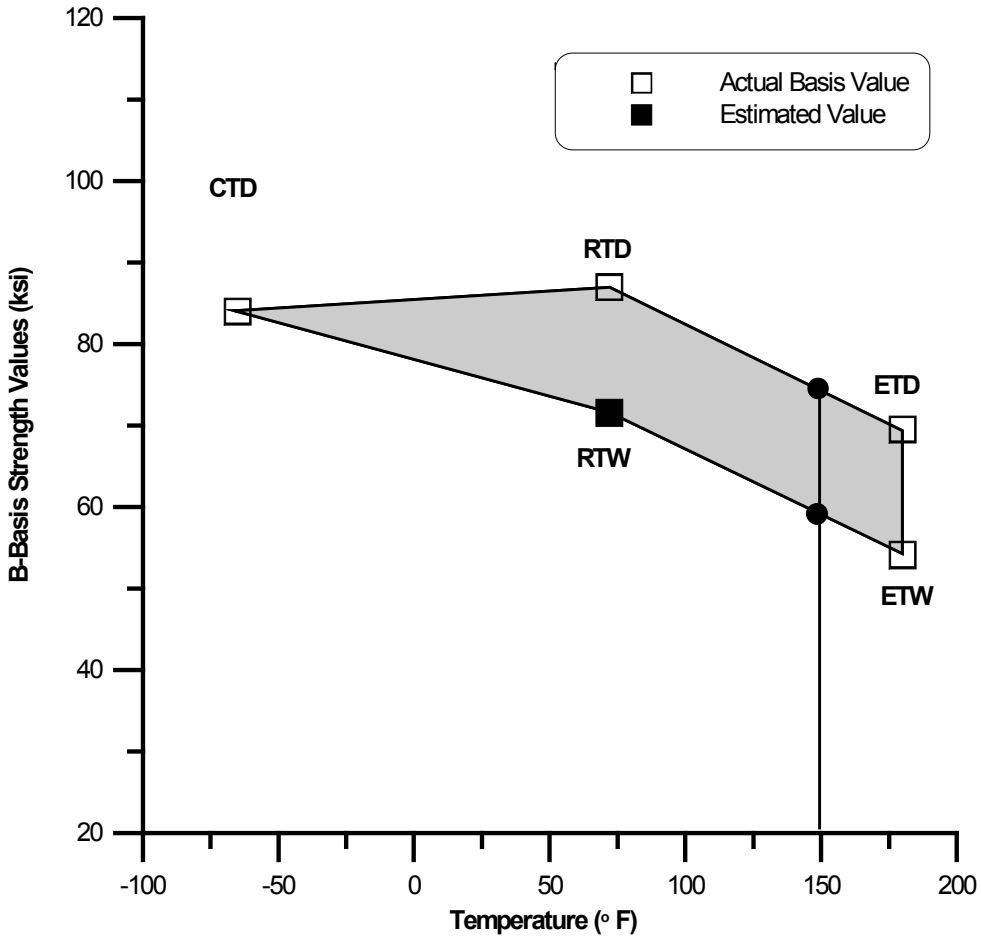


FIGURE 25. EXAMPLE OF 150°F INTERPOLATION FOR B-BASIS VALUES

6. MATERIAL EQUIVALENCY AND ACCEPTANCE TESTING.

This section describes the methodology to demonstrate material equivalency and establish acceptance testing criteria. Material equivalency programs are specified to ensure that a follow-on material or follow-on process will produce material properties equivalent to those of the original qualification. Acceptance testing is a quality control procedure designed to detect large property variations or undesirably high or low properties in an incoming prepreg lot.

In general, the properties that are normalized (see section 5.2.2) in the original qualification should be compared with normalized properties of the follow-on material for statistical testing purposes, particularly in the case of unidirectional tape. The data normalization method of the two sets of data should be identical. If data scatter increases significantly either in the original or follow-on material properties after the normalization process, the reason should be investigated.

The properties that are not normalized (see section 5.2.2) from the original qualification should be compared with unnormalized properties of the follow-on material. No clear model is currently available to accurately normalize matrix-dominated properties, although the effects of fiber volume fraction on these properties have been observed. This form of error may hamper the effectiveness and validity of the statistical tests. Rejection by statistical tests on these properties may be justified by significant differences in cured-ply thickness, fiber volume fraction, or void content; however, the reason for such differences should be investigated. In general, engineering judgement must be exercised to determine the significance of these properties that fail the criteria and may override the statistical tests.

A major part of the criterion adopted in this document is based on a statistical test commonly known as test of hypotheses. For strength properties, both the means and the minimum individual values are considered. This is a joint or combined α for a one-sided test, hence, a low mean or low minimum individual value or both will constitute a rejection. For modulus properties, only the means are considered. Table 11 provides the suitable criteria and test statistic for each property of interest.

When one embarks on the path of showing equivalency, engineering judgment should not be left behind. If some mechanical property at one temperature does not show statistical equivalence, the importance of that property and the size of the discrepancy should be investigated before declaring that the materials are not the same or equivalent. For example, tensile strength and modulus and ETW compression strength and modulus are examples of properties which are usually design critical and more importance should be placed on the statistical test results.

The criteria described in this section are applicable only when between-batch variability is assumed insignificant. MIL-HDBK-17-1E, section 8.4.2 provides guidance where between-batch variability is significant.

TABLE 11. SUITABLE PASS/FAIL CRITERIA AND TEST STATISTIC FOR EACH PROPERTY OF INTEREST

Table	Test Property	Pass/Fail Criteria and Test Statistic
12 and 15	Resin Content	Section 6.3.2 or see note 1
12 and 15	Volatile Content	Section 6.3.3 or see notes 1 and 5
12 and 15	Gel Time	Section 6.3.2 or see note 1
12 and 15	Resin Flow	Section 6.3.2 or see note 1
12 and 15	Fiber Areal Weight	Section 6.3.2 or see note 1
12 and 15	IR	See note 2
12 and 15	HPLC	See note 2
12 and 15	DSC	Section 6.3.2 or see note 4
13 and 16	Cured Ply Thickness	Section 6.3.2 or see note 1
13	Fiber Volume	Section 6.3.2 or see note 1
13	Resin Volume	Section 6.3.2 or see note 1
13	Void Content	Section 6.3.3 or see note 1
13	Cured Neat Resin Density	Section 6.3.2 or see note 1
13 and 16	Glass Transition Temperature (dry)	Section 6.3.2 or see sections 6.3.4 and 6.3.5
13	Glass Transition Temperature (wet)	Section 6.3.2 or see section 6.3.4
14 and 17	0^o (warp) Tensile Strength	Section 6.3.1
14 and 17	0^o (warp) Tensile Modulus	Section 6.3.2
14 and 17	90^o (fill) Tensile Strength	Section 6.3.1
14 and 17	90^o (fill) Tensile Modulus	Section 6.3.2 and see note 3 for unidirectional material form
14 and 17	0^o (warp) Compressive Strength	Section 6.3.1
14 and 17	0^o (warp) Compressive Modulus	Section 6.3.2
14 and 17	90^o (fill) Compressive Strength	Section 6.3.1 and see note 3 for unidirectional material form
14 and 17	90^o (fill) Compressive Modulus	Section 6.3.2 and see note 3 for unidirectional material form
14	In-Plane Shear Strength	Section 6.3.1 and see note 3
14	In-Plane Shear Modulus	Section 6.3.2 and see note 3
14 and 17	Short-Beam Shear	Section 6.3.1 and see note 3

Notes:

1. Values to be agreed upon between airframe manufacturer and material supplier. They should not be significantly different than that obtained from statistical tests.
2. Visual comparison of fingerprint is sufficient but quantitative pass/fail thresholds are highly recommended. All peaks in the original charts must be present in the follow-on charts. Extraneous peak(s) may suggest erroneous chemical composition or contamination. Unless the extraneous peak(s) is intentional, the material should be rejected.
3. These properties are not normalized but may be sensitive to fiber volume fraction. If these properties fail the criteria, the reason(s) should be investigated. Engineering judgement should be exercised to determine the significance of the failure.
4. Quantitative thresholds to be agreed upon between airframe manufacturer and material supplier.
5. Use section 6.3.3 for resin systems that cure by addition reaction (i.e., epoxy) and use section 6.3.2 for resin systems that cure by condensation reaction (i.e., phenolic).

6.1 MATERIAL EQUIVALENCE.

The procedures for material equivalency described in this report are only applicable to the following specific types of changes:

a. Identical material fabricated by the same airframe manufacturer using identical fabrication process at a different location

b. Identical material fabricated by a different airframe manufacturer using a follow-on process that is equivalent to the original process

c. Identical material fabricated by the same airframe manufacturer using a follow-on process that is slightly different from the original process

d. Minor changes in the prepreg constituent(s) or constituent manufacturing process

e. Combinations of the above

The above-mentioned changes are subject to the following limitations:

a. All critical prepreg constituent(s) or constituent manufacturing process must remain unchanged.

b. All critical steps in the process specifications used to fabricate the original and follow-on material systems must be equivalent. The process specification for the follow-on material system may not include any information that might degrade the performance of the follow-on material system below that of the originally qualified system.

c. The fabrication of the follow-on material system must meet the applicable CFR requirements including, but are not limited to:

- § 23.603 (a) and (b)
- § 23.605 (a) and (b)

In all cases of material equivalence, an original database should exist that contains material properties of the original material system.

The types of changes to the follow-on material system that are considered as major changes, which are not covered by this document include, but are not limited to:

a. Change of fiber (for example, changing from AS4 to T300 fibers)

b. Change of resin (for example, changing from 3501-6 to E7K8 resin)

c. Change of fabric weave style (for example, changing from eight-harness satin weave to plain weave)

d. Change of tow dimension of fabric (for example, changing from 6K tow to 3K tow)

e. Significant change in resin content of prepreg

f. Change of sizing or coupling agent type

The specific types of changes to the follow-on material system or process that may be considered as minor changes include, but are not limited to:

a. Increasing the cure pressure or vacuum level for the follow-on process. This includes changing from oven curing (vacuum only) to autoclave curing. Decreasing the cure pressure or vacuum level for the follow-on process, however, is generally not allowed.

b. Cure parameters such as dwell time and heat-up rate

c. Prepreg tackiness

Further evaluation or testing may be required depending on the extent of the changes. Reference 3 provides additional detailed guidance as to the specific levels of change applicable for the demonstration of material equivalency. For example, increasing the prepreg tackiness may result in a higher volatile content. Higher volatile content has been known to cause higher void content and lower glass transition temperature in cured laminate. MIL-HDBK-17-1E, sections 2.3.4, 2.3.7, 2.5.3.4, and 8.4.3, provides further guidance on this subject. Although outlined in MIL-HDBK-17-1E, in particular cases, engineering judgement must assess the degree of similarity between different materials or manufacturing process changes and the significance of these changes.

In the case where a material supplier decides to modify the material system, even for the purpose of improving the material properties, airframe manufacturers, which have been approved to use the material system, may be required to perform the material equivalency exercise to demonstrate that the change(s) is compatible with individual manufacturers' processing parameters.

A successful material equivalency demonstration does not imply that the follow-on material or follow-on process will also yield equal properties at laminate, element, and subcomponent levels, because the manufacturing complexity of a particular application may result in different properties. To ascertain if there will be any divergence of properties for more complex shapes and configurations, some simple laminate-notched tension and compression tests should be performed before investing in tooling, etc. If successful, further tests, such as elements and components, are typically needed to fulfill the remaining parts of the structural substantiation requirement.

The material equivalency procedures outlined herein are not intended for use in determining the effect of cocuring the prepreg onto honeycomb or foam. This level of testing should be conducted at the laminate level.

Fluid sensitivity screenings should be included in the material equivalency test matrix if the material will be exposed to fluids other than those screened in the original material qualification. (Section 4.5.3 may be used as a guide.)

The statistical method described in this report was chosen for its simplicity in application. Other methods can be found in MIL-HDBK-17-1E that can perform similar equivalency evaluations. Material equivalence testing should be conducted to incorporate the processing or panel-to-panel variability. Specimen sampling and selection should be based upon at least two independent processing or cure cycles, as shown in figure 26.

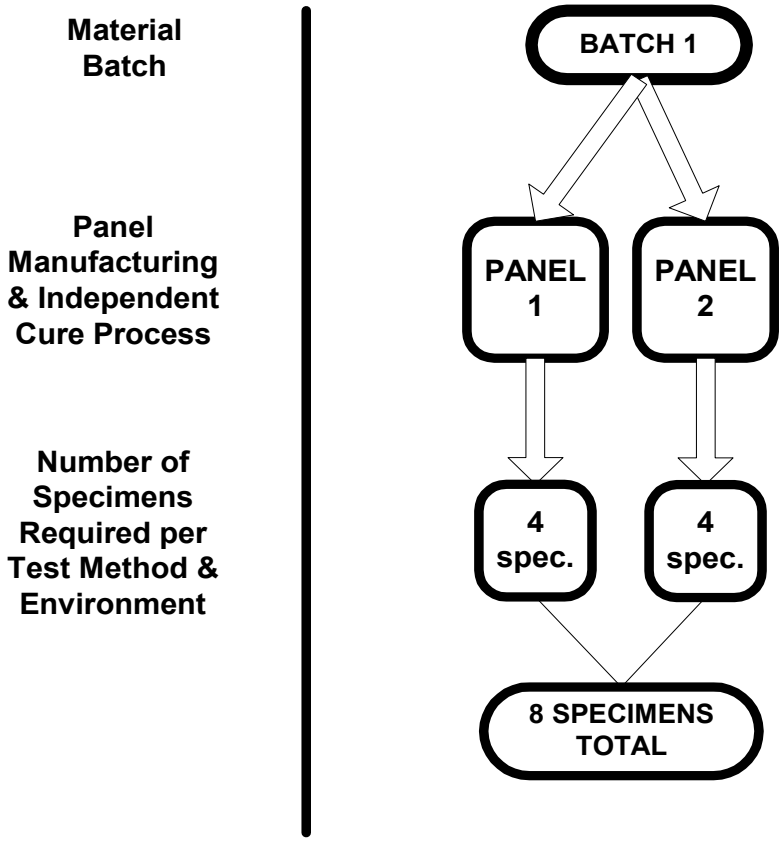


FIGURE 26. AN EXAMPLE OF SPECIMEN SELECTION METHODOLOGY AND PROCESSING TRACEABILITY PER TEST METHOD AND ENVIRONMENTAL CONDITION USED TO ESTABLISH MATERIAL EQUIVALENCE

Tables 12, 13, and 14 list the minimum requirements to substantiate material equivalency. The test matrix in table 12 is intended to verify that the material equivalence material is identical to the original material, or if the change is intentional, it will determine the extent of the change. Table 14 describes the minimum number of tests required for each environmental condition along with the relevant test methods to establish material equivalence with respect to the original A- or B-basis design allowable. The temperature for each environmental condition is described in section 4.3.

TABLE 12. MATERIAL EQUIVALENCE TESTING REQUIREMENTS FOR PHYSICAL, CHEMICAL, AND THERMAL PROPERTIES

Test Property	Test Method(s)		No. of Replicates
	ASTM	SACMA	
Resin Content	D 3529, C 613, D 5300	SRM 23, SRM 24	6
Volatile Content	D 3530	- - -	6
Gel Time	D 3532	SRM 19	6
Resin Flow	D 3531	SRM 22	6
Fiber Areal Weight	D 3776	SRM 23, SRM 24	6
IR	E 1252, E 168	- - -	3
HPLC*	- - -	SRM 20	3
DSC	E 1356	SRM 25	3

*Sections 5.5.1 and 5.5.2 of MIL-HDBK-17-1E describe detailed procedures that may be used to extract resin from prepreg and perform HPLC tests.

TABLE 13. MATERIAL EQUIVALENCE TESTING REQUIREMENTS FOR CURED LAMINA PHYSICAL PROPERTY TESTS

Physical Property	Test Procedure	No. of Replicates per Cure Cycle
Cured Ply Thickness	SACMA RM 10R	see note 8
Fiber Volume	ASTM D 3171[1] or D 2584[2]	see note 3
Resin Volume	ASTM D 3171[1] or D 2584[2]	see note 3
Void Content	ASTM D 2734[4]	see note 3
Cured Neat Resin Density	ASTM D 792	see note 5
Glass Transition Temperature (dry[6])	SACMA RM 18	2
Glass Transition Temperature (wet[7])	SACMA RM 18	2

Notes:

1. Test method used for carbon or graphite materials.
2. Test method used for fiberglass materials.
3. At least one test shall be performed on each panel manufactured for material equivalence (see appendices A and B).
4. Test method may also be applied to carbon or graphite materials.
5. Data or neat resin sample should be provided by material supplier for each batch of material.
6. Dry specimens are as-fabricated specimens that have been maintained at ambient conditions in an environmentally controlled laboratory.
7. Wet specimens are humidity-aged until an equilibrium moisture weight gain is achieved, per section 3.2.
8. Must be performed on every test panel.

TABLE 14. MATERIAL EQUIVALENCE TESTING REQUIREMENTS FOR CURED LAMINA MAIN PROPERTIES

Figure No.	Test	Method Reference	No. of Specimens per Test Condition	
			RTD[1]	ETW[2]
9 or 10*	0° (warp) Tensile Modulus and Strength	ASTM D 3039	8	8
11*	90° (fill) Tensile Modulus and Strength[4]	ASTM D 3039	8	8
12	0° (warp) Compressive Strength	SACMA SRM 1	8	8
13*	0° (warp) Compressive Modulus	SACMA SRM 1	8	8
14	90° (fill) Compressive Strength[4]	SACMA SRM 1	8	8
15*	90° (fill) Compressive Modulus[4]	SACMA SRM 1	8	8
16*	In-Plane Shear Modulus and Strength	ASTM D 5379	8	8
17	Short-Beam Shear	ASTM D 2344	8	--

*Strain gages or appropriate extensometers may be used.

Notes:

1. Only one batch of prepreg material is required (test temperature = 70° ±10°F, moisture content = as fabricated[3]).
2. Only one batch of prepreg material is required (test temperature = 180° ±5°F, moisture content = per section 3.2).
3. Dry specimens are as-fabricated specimens that have been maintained at ambient conditions in an environmentally controlled laboratory.
4. Necessary for unidirectional (tape) material form when design relies on the properties.

6.2 ACCEPTANCE TESTING.

Acceptance testing is also known as material receiving inspection, incoming material inspection, or raw material quality control testing. It is designed to detect large variations or undesirably high or low properties in the incoming prepreg lot. The procedures and acceptance criteria described herein are intended as guidelines for developing material and process specifications for quality control purposes. Material and process specifications should be revised based on lessons learned to reflect the quality assurance needs of specific material systems and production environments. This section provides test methods that are commonly used by airframe manufacturers and may not include every quality control test method necessary for adequate quality assurance. MIL-HDBK-17 and DOT/FAA/AR-02/109, Guidelines and Recommended Criteria for the Development of a Material Specification for Carbon Fiber/Epoxy Unidirectional Prepreg, contain more information on this subject. The procedures for receiving inspection do not allow for any changes in the material system or manufacturing process. The material system and manufacturing process must be identical to that used in the original qualification, or if material equivalency has been substantiated, it must be identical to that used in the material equivalence exercise.

Acceptance test requirements may vary from airframe manufacturer to airframe manufacturer. All the tests described in tables 15-19 should be performed by a material vendor, airframe manufacturer, or both. As use and confidence increase, the receiving inspection testing may be modified based on proven performance in cooperation with the material manufacturers and

appropriate FAA representatives. In this case, specific procedures must be in place to ensure that exposure to environments, which are detrimental to the prepreg during shipping, will be detected. Statistical process controls are typically in place to support these delegations. Additionally, annual verifications of material properties by the OEM or an independent facility must be conducted to verify process control of material in addition to periodic sampling. Delegations are typically conducted in stages that may involve several increasing levels of reliance on the supplier's testing. It should be noted that this testing provides assurance that the OEM panel fabrication and shipping conditions have not affected the material properties, as well as verification that the material manufacturer's processes are in control.

TABLE 15. ACCEPTANCE TEST MATRIX FOR PHYSICAL, CHEMICAL, AND THERMAL PROPERTIES (Recommendations Only)

Test Property	Test Method(s)		No. of Replicates
	ASTM	SACMA	
Resin Content	D 3529, C 613, D 5300, D 3171	SRM 23, SRM 24	3
Volatile Content	D 3530	- - -	3
Gel Time	D 3532	SRM 19	3
Resin Flow	D 3531	SRM 22	3
Fiber Areal Weight	D 3776	SRM 23, SRM 24	3
IR	E 1252, E 168	- - -	3
HPLC*	- - -	SRM 20	3
DSC	E 1356	SRM 25	3

*Sections 5.5.1 and 5.5.2 of MIL-HDBK-17-1E describe detailed procedures that may be used to extract resin from prepreg and perform HPLC tests.

TABLE 16. ACCEPTANCE TEST MATRIX FOR CURED LAMINA PHYSICAL PROPERTIES (Recommendations Only)

Physical Property	Test Procedure	No. of Replicates
Cured Ply Thickness	SACMA SRM 10R	See notes 2 and 3
Glass Transition Temperature (dry[1])	SACMA SRM 18	1

Notes:

1. Dry specimens are as-fabricated specimens that have been maintained at ambient conditions in an environmentally controlled laboratory.
2. Must be performed on every test panel.
3. Type of measuring surface should be identical to the one used in original material qualification, or the amount of difference introduced by the measuring surface should be taken into account.

TABLE 17. ACCEPTANCE TESTING FOR CURED LAMINA PROPERTIES
(Recommendations Only)

Figure No.	Test	Method Reference	No. of Specimens	
			RTD[1, 2]	ETD[1, 2]
9 or 10*	0^o (warp) Tensile Modulus and Strength	ASTM D 3039	3-5	-
11*	90^o (fill) Tensile Modulus and Strength[3]	ASTM D 3039	3-5	-
12	0^o (warp) Compressive Strength	SACMA SRM 1	-	3-5
13*	0^o (warp) Compressive Modulus	SACMA SRM 1	3-5	-
14	90^o (fill) Compressive Strength[3]	SACMA SRM 1	-	3-5
15*	90^o (fill) Compressive Modulus[3]	SACMA SRM 1	3-5	-
17	Short-Beam Shear	ASTM D 2344	3-5	-

*Strain gages or appropriate extensometers may be used.
Notes:

1. Only one lot of material is required (test temperature = 70° ±10°F, moisture content = as fabricated[2]).
2. Dry specimens are as-fabricated specimens that have been maintained at ambient conditions in an environmentally controlled laboratory.
3. Necessary for unidirectional (tape) material form when design relies on these properties.

For acceptance testing, it is not necessary to incorporate processing cycle or panel-to-panel variability, as shown in figure 26. All the test panels for the test matrix in table 17 may be processed in a single cure cycle.

Material and process specifications often define acceptable levels for visual defects; however, they are rather ineffective when incorporated into acceptance testing since it is impractical to unroll every roll of prepreg for the purpose of quality assurance. This inspection process is often left to individuals in charge of prepreg cutting and lay-up. These individuals must be trained and be familiar with prepreg visual inspection techniques. Table 18 lists some common types of defects and their corresponding acceptable levels.

TABLE 18. PREPREG VISUAL DEFECTS AND THEIR ACCEPTABLE LEVELS
(Recommendations Only)

Defects	Definitions	Acceptable Levels
Fiber Alignment	Deviation of the warp and fill fibers from a straight line using selvage as reference. This form of defect is usually performed on fabric form only, since it is difficult to determine fiber alignment of unidirectional form.	Less than 0.25 inch per linear foot
Fiber Breaks	Broken, damaged, or discontinuous fibers.	Less than 0.1 inch wide per square foot area for unidirectional form. Less than 1 yarn per square foot area for fabric form.
Inclusions	Foreign objects or particles.	No inclusion is allowed.
Fuzz Ball	Loose filament clumps or balls that are incorporated into the prepreg. Fuzz balls occur when individual filaments are abraded or broken during the prepreg manufacturing process.	Less than 1 square inch in any square foot area. Thickness of any fuzz ball should be less than 50% of the prepreg thickness.
Lack of Adherence to Backing Film	Separation between the prepreg and backing/separator film. This may be an indication of lack of tackiness that may cause problems in the cutting and lay-up processes.	To be determined by material and process engineering and production personnel.
Wrinkles	Ply wrinkles on backing film.	None allowed

Test frequency should be a function of the number of rolls of prepreg received. Table 19 shows some typical test frequencies as a function of the number of prepreg rolls. As use and confidence increase, the test frequency can be decreased. However, the remaining tests must be sufficient to assure the material will meet or exceed the engineering requirements.

TABLE 19. TEST FREQUENCY FOR ACCEPTANCE TESTING

Number of Rolls Received	Test Frequency
1-10	1 from a randomly selected roll
11-30	2 from the first and last rolls
31-60	3 from the first, last, and randomly selected rolls
61-90	4 from the first, last, and randomly selected rolls
90 and more	1 additional test for every additional 40 rolls from the first, last, and randomly selected rolls

6.3 STATISTICAL TESTS FOR MATERIAL EQUIVALENCY AND ACCEPTANCE TESTING.

This section provides test statistics related to material equivalency and acceptance testing. The test statistics are selected based on the material properties of interest. For certain properties, such as volatile content of prepreg, a high mean value is undesirable. The suitable test statistic for these types of properties will reject a high mean value. Other properties, such as modulus, require the mean value to be within an acceptable range; neither a high nor a low mean is desirable. The test statistics for these properties are designed to reject either a high or a low mean value. The test statistics for strength properties, on the other hand, will reject either a low

mean or a low minimum individual value. Table 11 shows the properties along with notes and sections that contain pass/fail criteria for the suitable test statistics.

6.3.1 Failure for Decrease in Mean or Minimum Individual Value.

Details of this statistical test can be found in reference 7. The mean, $\bar{x}$, and standard deviation, s, are approximated by the results obtained from the individual test condition (environment) of the original qualification. The pass/fail thresholds for mean properties, W_{mean}, are determined by equation 48. The mean values from experimental tests must meet or exceed the W_{mean}.

$$W_{mean} = \bar{x} - k_n^{\text{Table 20}} \cdot s \tag{48}$$

TABLE 20. CONSTANTS $k_n^{\text{Table 20}}$ FOR TEST ON MEAN AND MINIMUM INDIVIDUAL (VALUES FOR MEAN)

		α								
		0.25	0.1	0.05	0.025	0.01	0.005	0.0025	0.001	0.0005
Number of Samples (n)	2	0.6266	1.0539	1.3076	1.5266	1.7804	1.9528	2.1123	2.3076	2.4457
	3	0.5421	0.8836	1.0868	1.2626	1.4666	1.6054	1.7341	1.8919	2.0035
	4	0.4818	0.7744	0.9486	1.0995	1.2747	1.3941	1.5049	1.6408	1.7371
	5	0.4382	0.6978	0.8525	0.9866	1.1425	1.2488	1.3475	1.4687	1.5546
	6	0.4048	0.6403	0.7808	0.9026	1.0443	1.1411	1.2309	1.3413	1.4196
	7	0.3782	0.5951	0.7246	0.8369	0.9678	1.0571	1.1401	1.2422	1.3145
	8	0.3563	0.5583	0.6790	0.7838	0.9059	0.9893	1.0668	1.1622	1.2298
	9	0.3379	0.5276	0.6411	0.7396	0.8545	0.9330	1.0061	1.0959	1.1596
	10	0.3221	0.5016	0.6089	0.7022	0.8110	0.8854	0.9546	1.0397	1.1002
	11	0.3084	0.4790	0.5811	0.6699	0.7735	0.8444	0.9103	0.9914	1.0490
	12	0.2964	0.4593	0.5569	0.6417	0.7408	0.8086	0.8717	0.9493	1.0044
	13	0.2856	0.4418	0.5354	0.6168	0.7119	0.7770	0.8376	0.9121	0.9651
	14	0.2760	0.4262	0.5162	0.5946	0.6861	0.7488	0.8072	0.8790	0.9300
	15	0.2673	0.4121	0.4990	0.5746	0.6630	0.7235	0.7798	0.8492	0.8985
	16	0.2594	0.3994	0.4834	0.5565	0.6420	0.7006	0.7551	0.8223	0.8700
	17	0.2522	0.3878	0.4692	0.5400	0.6230	0.6797	0.7326	0.7977	0.8440
	18	0.2455	0.3771	0.4561	0.5250	0.6055	0.6606	0.7120	0.7753	0.8202
	19	0.2394	0.3673	0.4441	0.5111	0.5894	0.6431	0.6930	0.7546	0.7984
	20	0.2337	0.3582	0.4330	0.4982	0.5745	0.6268	0.6755	0.7355	0.7782
	21	0.2284	0.3498	0.4227	0.4863	0.5607	0.6117	0.6593	0.7178	0.7594
	22	0.2235	0.3419	0.4131	0.4752	0.5479	0.5977	0.6441	0.7013	0.7420
	23	0.2188	0.3345	0.4041	0.4648	0.5359	0.5846	0.6300	0.6859	0.7257
	24	0.2145	0.3276	0.3957	0.4551	0.5246	0.5723	0.6167	0.6715	0.7104
	25	0.2104	0.3211	0.3878	0.4459	0.5141	0.5608	0.6043	0.6579	0.6960
	26	0.2065	0.3150	0.3803	0.4373	0.5041	0.5499	0.5926	0.6451	0.6825
	27	0.2028	0.3092	0.3733	0.4292	0.4947	0.5396	0.5815	0.6331	0.6698
	28	0.1994	0.3038	0.3666	0.4215	0.4858	0.5299	0.5710	0.6217	0.6577
	29	0.1961	0.2986	0.3603	0.4142	0.4774	0.5207	0.5611	0.6109	0.6463
	30	0.1929	0.2936	0.3543	0.4073	0.4694	0.5120	0.5517	0.6006	0.6354

The pass/fail threshold for minimum individual properties, $W_{minimum\ individual}$, are determined by equation 49. The minimum individual values from experimental tests must meet or exceed the $W_{minimum\ individual}$.

$$W_{minimum\ individual} = \bar{x} - k_n^{\text{Table 21}} \cdot s \tag{49}$$

TABLE 21. CONSTANTS $k_n^{\text{Table 21}}$ FOR TEST ON MEAN AND MINIMUM INDIVIDUAL (VALUES FOR MINIMUM INDIVIDUAL)

		α								
		0.25	0.1	0.05	0.025	0.01	0.005	0.0025	0.001	0.0005
Number of Samples (n)	2	1.2887	1.8167	2.1385	2.4208	2.7526	2.9805	3.1930	3.4549	3.6412
	3	1.5407	2.0249	2.3239	2.5888	2.9027	3.1198	3.3232	3.5751	3.7550
	4	1.6972	2.1561	2.4420	2.6965	2.9997	3.2103	3.4082	3.6541	3.8301
	5	1.8106	2.2520	2.5286	2.7758	3.0715	3.2775	3.4716	3.7132	3.8864
	6	1.8990	2.3272	2.5967	2.8384	3.1283	3.3309	3.5220	3.7603	3.9314
	7	1.9711	2.3887	2.6527	2.8900	3.1753	3.3751	3.5638	3.7995	3.9690
	8	2.0317	2.4407	2.7000	2.9337	3.2153	3.4127	3.5995	3.8331	4.0011
	9	2.0838	2.4856	2.7411	2.9717	3.2500	3.4455	3.6307	3.8623	4.0292
	10	2.1295	2.5250	2.7772	3.0052	3.2807	3.4745	3.6582	3.8883	4.0541
	11	2.1701	2.5602	2.8094	3.0351	3.3082	3.5005	3.6830	3.9116	4.0765
	12	2.2065	2.5918	2.8384	3.0621	3.3331	3.5241	3.7054	3.9328	4.0969
	13	2.2395	2.6206	2.8649	3.0867	3.3558	3.5456	3.7259	3.9521	4.1155
	14	2.2697	2.6469	2.8891	3.1093	3.3766	3.5653	3.7447	3.9699	4.1326
	15	2.2975	2.6712	2.9115	3.1301	3.3959	3.5836	3.7622	3.9865	4.1485
	16	2.3232	2.6937	2.9323	3.1495	3.4138	3.6007	3.7784	4.0019	4.1633
	17	2.3471	2.7146	2.9516	3.1676	3.4306	3.6166	3.7936	4.0163	4.1772
	18	2.3694	2.7342	2.9698	3.1846	3.4463	3.6315	3.8079	4.0298	4.1902
	19	2.3904	2.7527	2.9868	3.2005	3.4611	3.6456	3.8214	4.0425	4.2025
	20	2.4101	2.7700	3.0029	3.2156	3.4751	3.6589	3.8341	4.0546	4.2142
	21	2.4287	2.7864	3.0181	3.2298	3.4883	3.6715	3.8461	4.0660	4.2252
	22	2.4463	2.8020	3.0325	3.2434	3.5009	3.6835	3.8576	4.0769	4.2357
	23	2.4631	2.8168	3.0463	3.2562	3.5128	3.6949	3.8685	4.0873	4.2457
	24	2.4790	2.8309	3.0593	3.2685	3.5243	3.7058	3.8790	4.0972	4.2553
	25	2.4941	2.8443	3.0718	3.2802	3.5352	3.7162	3.8889	4.1066	4.2644
	26	2.5086	2.8572	3.0838	3.2915	3.5456	3.7262	3.8985	4.1157	4.2732
	27	2.5225	2.8695	3.0953	3.3023	3.5557	3.7357	3.9077	4.1245	4.2816
	28	2.5358	2.8813	3.1063	3.3126	3.5653	3.7449	3.9165	4.1328	4.2897
	29	2.5486	2.8927	3.1168	3.3225	3.5746	3.7538	3.9250	4.1409	4.2975
	30	2.5609	2.9036	3.1270	3.3321	3.5835	3.7623	3.9332	4.1487	4.3050

6.3.2 Failure for Change in Mean.

This statistical test assumes that the standard deviations of the original and follow-on data are equal but unknown. The pooled standard deviation, S_p, is used as an estimator of common population standard deviation.

$$S_p = \sqrt{\frac{(n_1 - 1) \cdot S_1{}^2 + (n_2 - 1) \cdot S_2{}^2}{n_1 + n_2 - 2}} \tag{50}$$

$$t_0 = \frac{\bar{x}_1 - \bar{x}_2}{S_p \cdot \sqrt{\frac{1}{n_1} + \frac{1}{n_2}}} \tag{51}$$

The test statistic is t_0 and n is the number of specimens. Subscripts 1 and 2 denote follow-on and original, respectively. Since this is a two-sided t-test, $t_{a,n} = t_{\alpha/2, n_1+n_2-2}$. Note that $a = \alpha/2$ for the two-sided test. $t_{a,n}$ is obtained from table 22. The passing range is between $-t_{\alpha/2, n_1+n_2-2}$ and $t_{\alpha/2, n_1+n_2-2}$. In other words, t_0 must be smaller than $t_{\alpha/2, n_1+n_2-2}$ but larger than $-t_{\alpha/2, n_1+n_2-2}$ to pass the criteria.

TABLE 22. CONSTANTS $t_{a,n}$

	a									
n	0.4	0.25	0.1	0.05	0.025	0.01	0.005	0.0025	0.001	0.0005
1	0.325	1	3.078	6.314	12.706	31.821	63.657	127.32	318.31	636.62
2	0.289	0.816	1.886	2.920	4.303	6.965	9.925	14.089	23.326	31.598
3	0.277	0.765	1.638	2.353	3.182	4.541	5.841	7.453	10.213	12.924
4	0.271	0.741	1.533	2.132	2.776	3.747	4.604	5.598	7.173	8.610
5	0.267	0.727	1.476	2.015	2.571	3.365	4.032	4.773	5.893	6.869
6	0.265	0.718	1.440	1.943	2.447	3.143	3.707	4.317	5.208	5.959
7	0.263	0.711	1.415	1.895	2.365	2.998	3.499	4.029	4.785	5.408
8	0.262	0.706	1.397	1.860	2.306	2.896	3.355	3.833	4.501	5.041
9	0.261	0.703	1.383	1.833	2.262	2.821	3.250	3.690	4.297	4.781
10	0.260	0.700	1.372	1.812	2.228	2.764	3.169	3.581	4.144	4.587
11	0.260	0.697	1.363	1.796	2.201	2.718	3.106	3.497	4.025	4.437
12	0.259	0.695	1.356	1.782	2.179	2.681	3.055	3.428	3.930	4.318
13	0.259	0.694	1.350	1.771	2.160	2.650	3.012	3.372	3.852	4.221
14	0.258	0.692	1.345	1.761	2.145	2.624	2.977	3.326	3.787	4.140
15	0.258	0.691	1.341	1.753	2.131	2.602	2.947	3.286	3.733	4.073
16	0.258	0.690	1.337	1.746	2.120	2.583	2.921	3.252	3.686	4.015
17	0.257	0.689	1.333	1.740	2.110	2.567	2.898	3.222	3.646	3.965
18	0.257	0.688	1.330	1.734	2.101	2.552	2.878	3.197	3.610	3.922
19	0.257	0.688	1.328	1.729	2.093	2.539	2.861	3.174	3.579	3.883
20	0.257	0.687	1.325	1.725	2.086	2.528	2.845	3.153	3.552	3.850
21	0.257	0.686	1.323	1.721	2.080	2.518	2.831	3.135	3.527	3.819
22	0.256	0.686	1.321	1.717	2.074	2.508	2.819	3.119	3.505	3.792
23	0.256	0.685	1.319	1.714	2.069	2.500	2.807	3.104	3.485	3.767
24	0.256	0.685	1.318	1.711	2.064	2.492	2.797	3.091	3.467	3.745
25	0.256	0.684	1.316	1.708	2.060	2.485	2.787	3.078	3.450	3.725
26	0.256	0.684	1.315	1.706	2.056	2.479	2.779	3.067	3.435	3.707
27	0.256	0.684	1.314	1.703	2.052	2.473	2.771	3.057	3.421	3.690
28	0.256	0.683	1.313	1.701	2.048	2.467	2.763	3.047	3.408	3.674
29	0.256	0.683	1.311	1.699	2.045	2.462	2.756	3.038	3.396	3.659
∞	0.253	0.674	1.282	1.645	1.960	2.326	2.576	2.807	3.090	3.291

For stiffness properties, modulus and Poisson's ratio, variations of ±5%-7% from the base material mean can be an acceptable practice if difficulties are encountered with the t-test.

6.3.3 Failure for a High Mean.

The test statistic, t_0, is obtained from equation 51. This test is designed to detect undesirably high mean values such as the volatile content of epoxy-based prepreg. The mean of the follow-on property is said to be higher than the mean of the original property if equation 52 is satisfied, an indication of bad material or process. This is a one-sided t-test so $t_{a,n} = t_{\alpha,n_1+n_2-2}$. Note that $a = \alpha$ for the one-sided test. $t_{a,n}$ is obtained from table 22.

$$t_0 > t_{\alpha,n_1+n_2-2} \tag{52}$$

6.3.4 Criteria Specific to Material Equivalence.

As of now, there are no fixed criteria for establishment of the MOL. One commonly used method uses wet glass transition temperature, reduced by some temperature margin ΔT, to establish the MOL. If this method is used, the MOL must exceed the maximum operating temperature. In addition, the average glass transition temperature (dry and wet) results in table 12 should not be significantly lower or higher than the results obtained from original material qualification. Section 6.3.2 can be used to determine the acceptable range. If the test method, equipment, or fixture are not identical to the ones used in the original qualification, the t-test may be invalid. It is recommended that a test method, equipment, or test fixture study be performed to investigate the amount of error due to the new test parameter.

For determining material equivalency, it is recommended to set the probability of rejecting a good property (α) to 0.05 or 5% for all test methods that use the test statistics in sections 6.3.1, 6.3.2, and 6.3.3. One retest is allowed for each property, reducing the actual probability to 0.0025 or 0.25%. As shown in table 14, a minimum of eight specimens is required for strength properties comparison (typically four specimens from each processing cycle). A minimum of four specimens is required for modulus comparisons (typically two specimens from each processing cycle). If one or more properties fail the criteria, one may choose to test only those properties that failed the criteria. However, it is recommended that the entire material equivalence test matrix be repeated if more than half of the properties in table 14 fail the criteria, so that a new qualification database may be generated. See section 6.4.5 for discussions on generating a new original qualification from material equivalence.

6.3.5 Criteria Specific to Acceptance Testing.

The determination of glass transition via onset of storage modulus requires two tangent lines to be drawn. Since this is somewhat operator dependent, the peak of tangent delta or the peak of loss modulus may be a more desirable interpretation method for this quality control purpose. Section 6.3.2 can be used to determine the acceptable range. If the test method, equipment, or fixture are not identical to the ones used in the original qualification, the t-test may be invalid. It is recommended that a test method, equipment, or test fixture study be performed to investigate the amount of error due to the new test parameter.

For determining material acceptance, it is recommended to set the probability of rejecting a good property to 0.01 or 1% for all the test methods that use the test statistics in sections 6.3.1, 6.3.2, and 6.3.3. Since one retest is allowed for acceptance testing, the actual probability of rejecting a good property is reduced to 0.0001 or 0.01%. Only those properties that fail the criteria need to be repeated. Note that the minimum number of specimens required for strength results in table 17 is three. It is highly recommended that five or more specimens be used to reduce the probability of accepting a bad lot of prepreg material without increasing the probability of rejecting a good lot of material. See section 6.4.2 for discussion on Type 1 and Type 2 errors.

It is recommended that the acceptance limits (pass/fail thresholds) be established for each material system. If there is more than one material system in a material and process specification (alternate material systems), each material system should have its own acceptance limits. This approach allows undesirable variations in each material property to be detected. In many traditional approaches, all the material systems within a material specification share the same acceptance limits. The acceptance limits are usually based on the properties of the lowest performing material within the material and process specification. This approach may not detect undesirable property variations in the higher-performing material within the same specification, which may be an indication of out-of-control process.

6.3.6 Statistical Testing Examples.

The following examples use experimental results from a 270°F-cured 3K plain weave carbon/epoxy tested at the 180°F wet (ETW) condition.

6.3.6.1 An Example of Statistical Test for 0° Compressive Strength.

This example uses the procedure delineated in section 6.3.1. The recommended probability of Type 1 error, α, is 0.05 or 5%. The normalized raw data for this example is shown in table 23.

TABLE 23. COMPRESSIVE STRENGTH RESULTS OF CARBON/EPOXY

Specimen ID	Processing Cycle	Prepreg Lot	Strength (ksi)
K1123F	1	1	49.656
K1124F	1	1	51.887
K1125F	1	1	47.508
K1126F	1	1	48.610
K1323F	2	1	52.595
K1324F	2	1	47.439
K1325F	2	1	54.702
K1326F	2	1	56.231
K1327F	2	1	57.199
		Mean	51.759
		Standard Deviation	3.7088

The mean and standard deviation of the original strength results are 58.762 ksi and 4.5612 ksi, respectively. Since 0° compressive strength is a fiber-dominated property, both sets of data have been normalized to the same fiber volume fraction (see section 5.2). The pass/fail threshold calculation for mean strength from equation 48 is as follows:

- $W_{mean} = \bar{x} - k_n^{\text{Table 20}} \cdot s$
- $W_{mean} = 58.762 - k_9^{\text{Table 20}} \cdot 4.5612$
- $W_{mean} = 58.762 - 0.6411 \cdot 4.5612$
- $W_{mean} = 55.838\,\text{ksi}$

Since the follow-on mean (51.759 ksi) is lower than the W_{mean} (55.838 ksi), the follow-on material fails the test. It is concluded that the mean compressive strength of the follow-on material is lower than 58.762 ksi based on $\alpha = 0.05$ level.

The pass/fail threshold calculation for minimum individual strength from equation 49 is as follows:

- $W_{min\,imum\ \ individual} = \bar{x} - k_n^{\text{Table 21}} \cdot s$
- $W_{min\,imum\ \ individual} = 58.762 - k_9^{\text{Table 21}} \cdot 4.5612$
- $W_{min\,imum\ \ individual} = 58.762 - 2.7411 \cdot 4.5612$
- $W_{min\,imum\ \ individual} = 46.259\,\text{ksi}$

All the individual strength values exceed the $W_{minimum\ individual}$, but since the mean failed the requirement, the follow-on material is said to have failed the test. The test for this property will need to be repeated.

6.3.6.2 An Example of Statistical Test for 0° ETW Compressive Modulus.

This example uses the procedure delineated in section 6.3.2. The normalized data for this example is shown in table 24.

TABLE 24. ZERO DEGREE ETW COMPRESSIVE MODULUS RESULTS OF CARBON/EPOXY

Specimen ID	Processing Cycle	Prepreg Lot	Modulus (ksi)
L1121F	1	1	7.761
L1122F	1	1	7.660
L1123F	1	1	7.399
L1124F	1	1	7.610
L1131F	2	1	7.783
L1132F	2	1	7.606
L1133F	2	1	7.419
L1134F	2	1	7.810
		Mean	7.631
		Standard Deviation	0.1571

The mean and standard deviation of the original modulus results are 7.506 Msi and 0.3066 Msi, respectively. Since 0° compressive modulus is a fiber-dominated property, both sets of data have been normalized to the same fiber volume fraction (see section 5.2). The original qualification used a total of 18 modulus specimens. As in the previous example, the recommended α is 0.05 or 5%, and $\alpha/2$ is 0.025. The pass/fail threshold calculation for mean modulus from equations 50 and 51 is as follows:

- $$S_p = \sqrt{\frac{(n_1 - 1) \cdot S_1^{\,2} + (n_2 - 1) \cdot S_2^{\,2}}{n_1 + n_2 - 2}}$$
- $$S_p = \sqrt{\frac{(8 - 1) \cdot 0.1571^2 + (18 - 1) \cdot 0.3066^2}{8 + 18 - 2}}$$
- $$S_p = 0.2716$$
- $$t_0 = \frac{\bar{x}_1 - \bar{x}_2}{S_p \cdot \sqrt{\frac{1}{n_1} + \frac{1}{n_2}}}$$
- $$t_0 = \frac{7.631 - 7.506}{0.2716 \cdot \sqrt{\frac{1}{8} + \frac{1}{18}}}$$
- $$t_0 = 1.083$$

From table 22, for a two-sided test, $t_{a,n} = t_{\alpha/2,n_1+n_2-2} = t_{0.05/2,8+18-2} = t_{0.025,24} = 2.064$. Since 1.083 is within the range of -2.064 and 2.064, the ETW compressive modulus passes the criteria.

6.3.6.3 An Example of Statistical Test for Volatile Content.

This example uses the procedure delineated in section 6.3.3. The original qualification used 18 volatile content test specimens from three batches of prepreg. The mean and standard deviation are 0.263% and 0.1061%, respectively. The follow-on test results have a mean of 0.258% and a standard deviation of 0.0108%.

- $$S_p = \sqrt{\frac{(n_1 - 1) \cdot S_1^{\,2} + (n_2 - 1) \cdot S_2^{\,2}}{n_1 + n_2 - 2}}$$
- $$S_p = \sqrt{\frac{(6 - 1) \cdot 0.0108^2 + (18 - 1) \cdot 0.1061^2}{6 + 18 - 2}}$$

- $S_p = 0.09341\%$
- $t_0 = \dfrac{\bar{x}_1 - \bar{x}_2}{S_p \cdot \sqrt{\dfrac{1}{n_1} + \dfrac{1}{n_2}}}$
- $t_0 = \dfrac{0.258 - 0.263}{0.09341 \cdot \sqrt{\dfrac{1}{6} + \dfrac{1}{18}}}$
- $t_0 = -0.1135$

From table 22, $t_{a,n} = t_{\alpha,n_1+n_2-2} = t_{0.05,6+18-2} = t_{0.05,22} = 1.717$. Since t_0 is less than 1.717, there is no evidence to claim that the follow-on material has higher volatile content than the original material. This batch of material passes the volatile content test requirement.

6.4 FURTHER DISCUSSION.

6.4.1 Effects of Coefficient of Variation.

The statistical tests described in sections 6.3.2 and 6.3.3 may not provide adequate conservatism in the case where the CV is too large and the number of specimens is minimal. The acceptable range may be too large for the test in section 6.3.2, or the pass/fail threshold may be too low for the test in section 6.3.3. When the CV is erroneously small, the acceptable range or threshold may be too conservative. In general, a CV in the 4% to 10% range is typical of composite materials and would yield adequate conservatism. Engineering judgement may supercede the thresholds obtained from these statistical tests in the case of an erratic CV or when the acceptable range or threshold do not make engineering sense. In general, the statistical test described in section 6.3.1 is more immune to a large CV since A- and B-basis allowables will also be lower when the CV is large.

6.4.2 Type 1 and Type 2 Errors.

This section provides some background information about the statistical tests described in section 6.3. The statistical tests are commonly known as hypothesis tests. For simplicity, the following discussions will assume that the samples come from a normal distribution with mean (μ) and standard deviation (σ). The discussion will employ an example of a one-sided test where a low mean strength is not acceptable. Note that this is not exactly identical to the statistical test for strength since it does not include a test on minimum individual value.

	Claim that $\mu_{follow\text{-}on} > \mu_{original}$ is true	Claim that $\mu_{follow\text{-}on} > \mu_{original}$ is not true
$\mu_{follow\text{-}on} > \mu_{original}$ is actually true	No Error	Type 1 Error
$\mu_{follow\text{-}on} > \mu_{original}$ is actually not true	Type 2 Error	No Error

Type 1 error occurs when the statistical test claims that the $\mu_{follow\text{-}on} > \mu_{original}$ is not true when $\mu_{follow\text{-}on} > \mu_{original}$ is actually true. In other words, a material property is erroneously failed. The probability of committing a Type 1 error is commonly designated as α. Type 2 error occurs when the statistical test fails to claim that $\mu_{follow\text{-}on} > \mu_{original}$ is not true when $\mu_{follow\text{-}on} > \mu_{original}$ is actually true. The probability of committing a Type 2 error is commonly known as β.

The figures in the following section are intended to provide engineers with some background knowledge of hypothesis tests. They are for illustration purposes only. Due to their simplicity, these figures contain some subtle technical errors; however, the observations that are made from these figures are valid statistical facts.

6.4.2.1 Effects of Number of Specimens on Pass/Fail Threshold.

Figures 27 and 28 show one-sided tests where a low mean strength is unacceptable. The standard deviations of both figures are equal. The probability of rejecting a good follow-on property, α, for both cases is 0.01 or 1%. Note that the pass/fail thresholds are unequal for both cases. In figure 27, the number of specimens tested, n, is 2. The threshold is 60.04 ksi. The number of specimens in figure 28, n, is 10. The threshold is 62.57 ksi. The shift in the threshold is purely due to the number of specimens tested. When only two specimens are tested, the probability of the average value to appear different from the original qualification data is higher. When the number of specimens tested is ten, the probability of the average to appear different from the original qualification data is lower. Since the Type 1 error probability is defined in the statistical test, the threshold must be lower for fewer specimens and higher for more specimens. This also means that if the threshold is maintained at the same level (60.04 ksi) when the number of specimens is increased from two to ten, the probability of Type 1 error will decrease. In order to remain at the same α level, the threshold must be increased when the number of specimens is increased. Note that this is true only where a low mean is unacceptable.

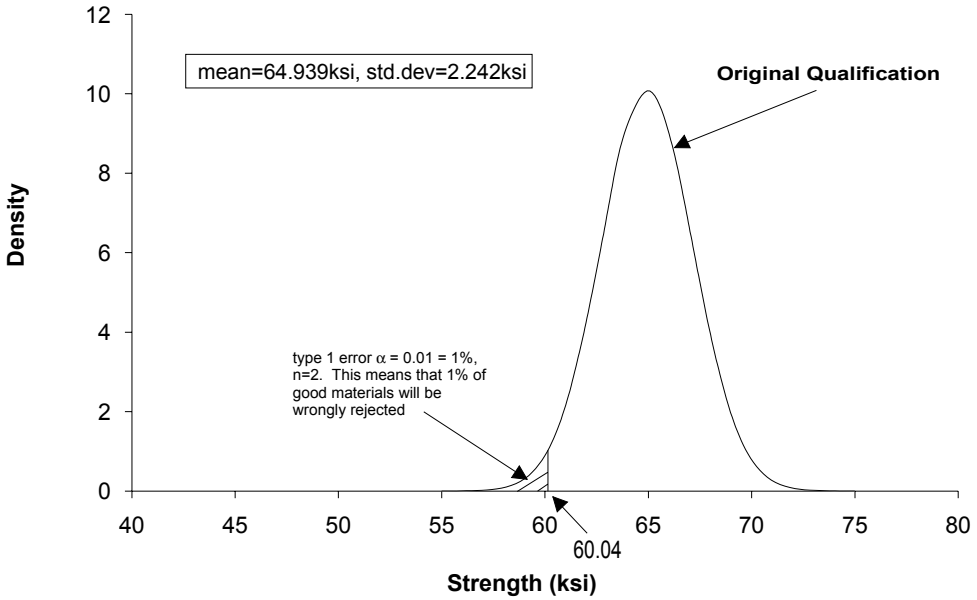


FIGURE 27. A NORMAL DISTRIBUTION, TWO SPECIMENS

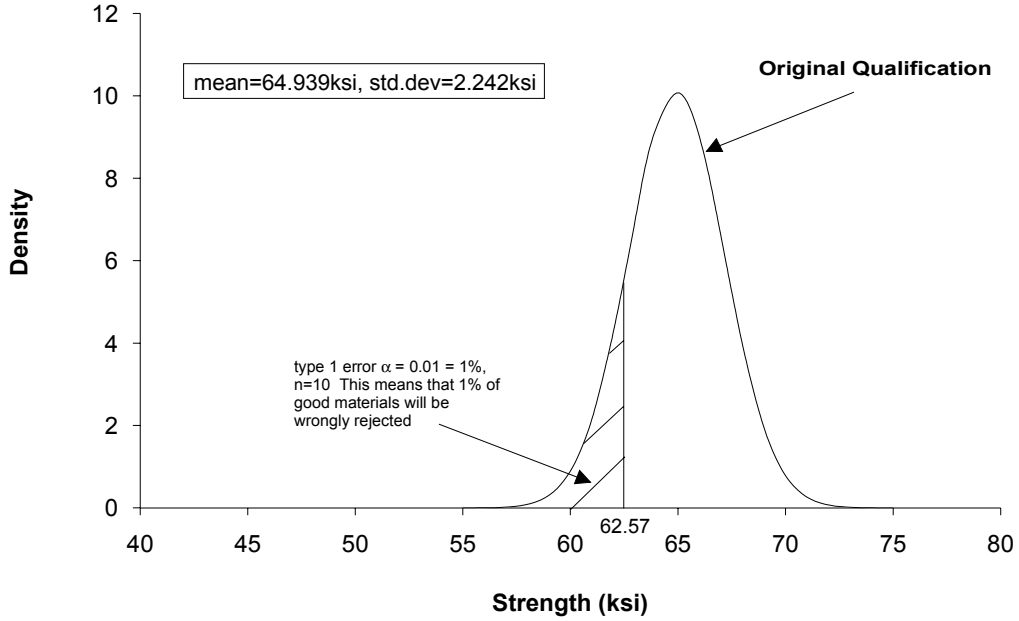


FIGURE 28. A NORMAL DISTRIBUTION, TEN SPECIMENS

6.4.2.2 Specifics About the Test on Minimum Individual.

This section attempts to explain the purpose of the test on minimum individual (section 6.3.1). The actual purpose of this test is not known; however, it is evident that engineers from various companies and organizations have decided that minimum individual is an important indicator of a bad material. To explain in statistical terms, a test on minimum individual may be viewed as analogous to a test on standard deviation. Figure 29 shows two normal distributions with equal means but unequal standard deviations. It is assumed that the minimum individual value will fail the statistical test if the standard deviation of the follow-on property is greater than the standard deviation of the original property. If the true purpose of this test is to detect a large standard deviation, then the test on standard deviation is certainly a more adequate test. However, this test usually requires substantially more specimens (about 20 or more) to achieve the desired accuracy, which may be impractical for most material equivalence or acceptance testing applications.

6.4.2.3 Some Misleading and Useful Information About Type 2 Error.

Type 2 error probability is the probability of claiming that the follow-on material has a higher mean strength than the original material when the reverse is true. One may be inclined to think that a Type 2 error is the type of error that should be controlled since the interest is to detect bad material. In fact, the definition of a Type 2 error is misleading. Consider figures 30 and 31. In both figures, the number of specimens is n=10, $\alpha = 0.01 = 1\%$, and the standard deviations are equal. The only difference is that the mean strength of the follow-on material is closer to the mean strength of the original material in figure 30. Note that the Type 2 error (cross-hatched area) in figure 30 is greater than the Type 2 error in figure 31. This implies that Type 2 error probability is higher when the mean strength of the follow-on material is closer to the mean strength of the original material.

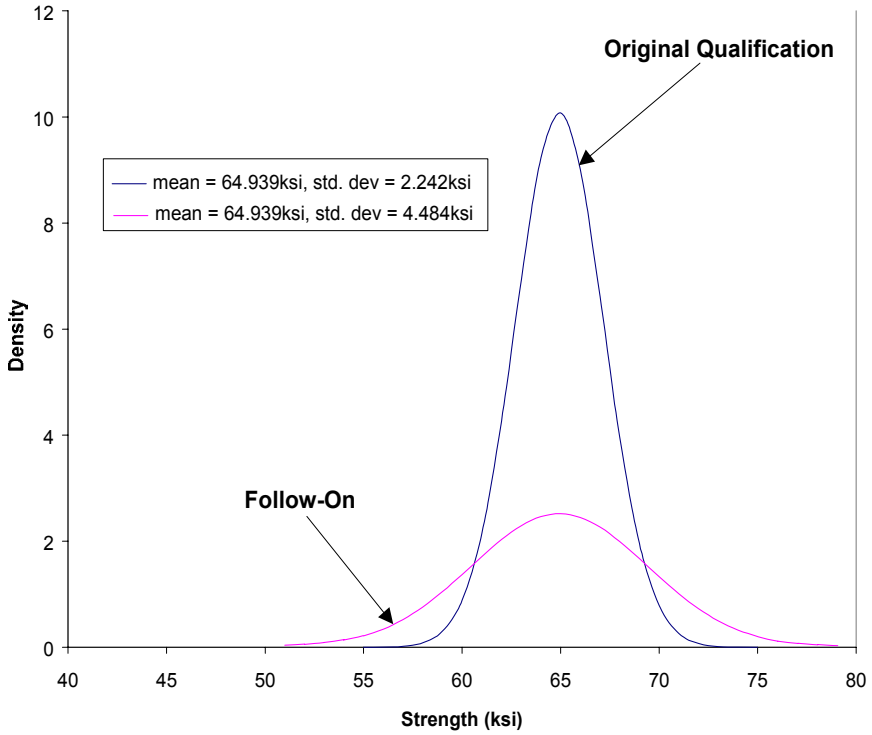


FIGURE 29. TWO NORMAL DISTRIBUTIONS, WITH EQUAL MEANS BUT UNEQUAL STANDARD DEVIATIONS

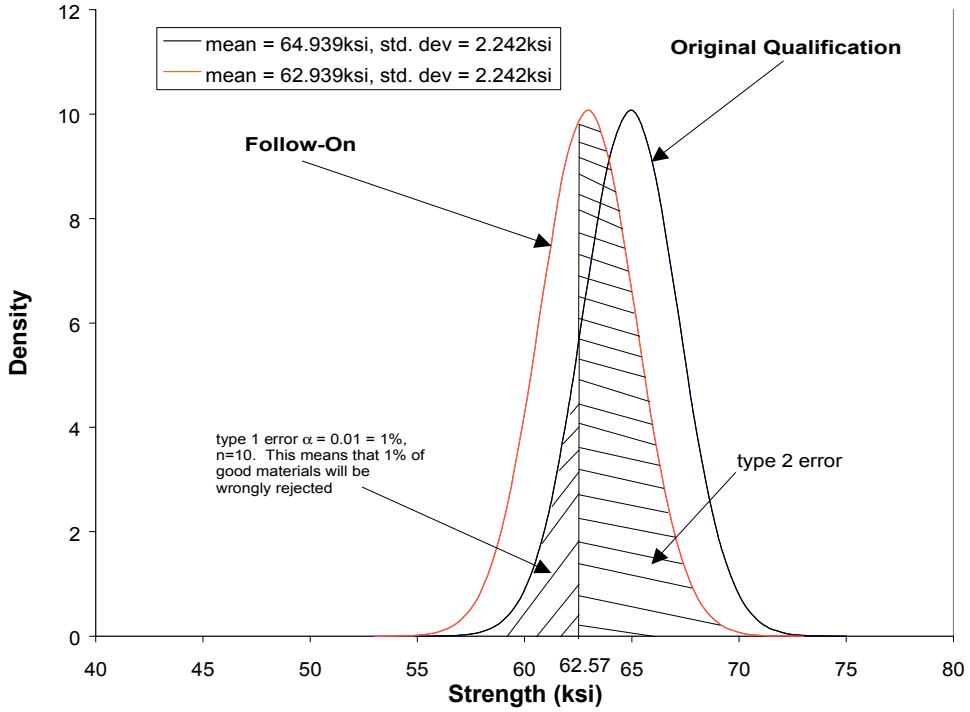


FIGURE 30. TWO NORMAL DISTRIBUTIONS OF EQUAL STANDARD DEVIATIONS, CLOSE BUT UNEQUAL MEANS, TEN SPECIMENS

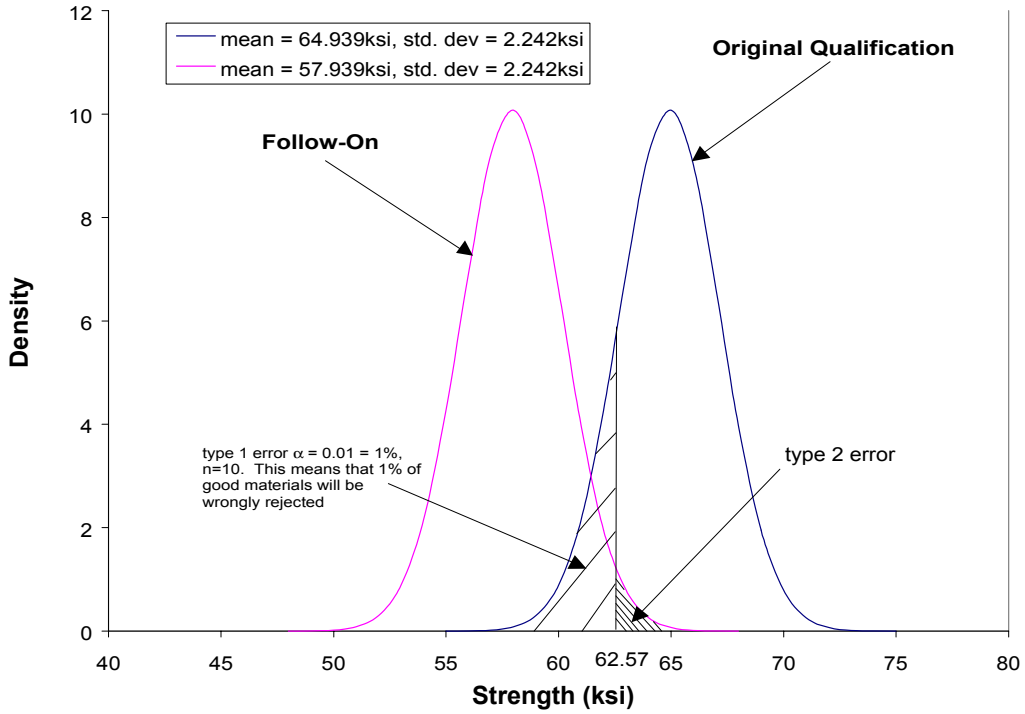


FIGURE 31. TWO NORMAL DISTRIBUTIONS OF EQUAL STANDARD DEVIATIONS, UNEQUAL MEANS, TEN SPECIMENS

Despite the misleading definition, a Type 2 error does provide some useful information. Comparing figures 31 and 32, the original qualification plot in figure 31 is similar to that in figure 28, and the original qualification plot in figure 32 is similar to that in figure 27. Note that the Type 2 error (cross-hatched area) in figure 31 is less than the Type 2 error in figure 32. These two figures show that by increasing the number of specimens, the Type 2 error probability may be reduced. Note that the probability of committing a Type 1 error is the same for both cases. The minimum number of specimens required for material equivalence and acceptance testing is defined to reduce the probability of accepting a bad property. It is highly recommended that more specimens than the required minimum be tested to increase the probability of detecting a bad property without increasing the probability of rejecting a good property.

Note that the selection of α is for each material property; the actual probability of committing a Type 1 error for a set of material equivalence tests or a set of acceptance tests is higher than α since several properties are considered in a test matrix.

In reality, it is impossible to commit a Type 1 error when the follow-on actually has a lower mean strength than the original (see section 6.4.2). The actual distribution of the follow-on is not usually known due to the limited number of specimens typically tested in material equivalence and acceptance testing. Also, Type 1 error probability for a one-sided test is maximum and equal to the selected value (α=0.01=1%) when the mean of the follow-on is actually equal to the mean of the original. Type 1 error probability will be smaller than the selected value when the mean of the follow-on is actually higher than the mean of the original.

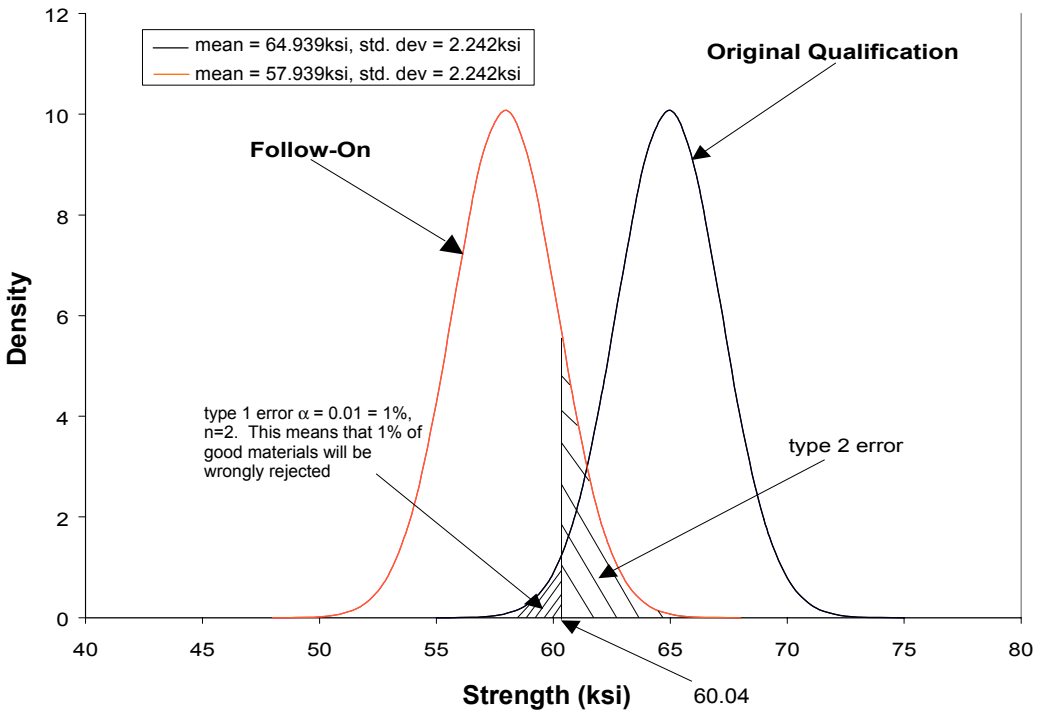


FIGURE 32. TWO NORMAL DISTRIBUTIONS OF EQUAL STANDARD DEVIATIONS, UNEQUAL MEANS, TWO SPECIMENS

6.4.3 Some Unaccounted Forms of Error.

It is highly recommended that the specific specimen preparation and testing procedures used in the original material qualification be documented and followed during material equivalence and acceptance testing. The procedures described in this section do not take into account the between-laboratory error. Every attempt should be made to document the specific procedures used in the original qualification to minimize the between-laboratory error. The actual probability of rejecting good property may be higher or lower than specified (α=0.05 for material equivalence and α=0.01 for acceptance testing), if unaccounted errors such as those introduced by between-laboratory exist.

For example, consider the situation where material qualification testing has been performed by laboratory A. Material acceptance testing is delegated to laboratory B without a prior between-laboratory study with laboratory A. This situation may result in unconservative consequences (per section 6.3.1) if laboratory B is more skillful than laboratory A in specimen preparation and testing. Laboratory B would not detect an undesirable decrease in material strength. On the other hand, if laboratory B is less skillful than laboratory A, laboratory B may erroneously reject a good prepreg lot. It should be noted that acceptance testing is designed to detect undesirable material property variations. Unaccounted forms of error such as between-laboratory error, between-test-method error, or operator error may hamper the effectiveness of material acceptance to detect undesirable material property variations. See section 6.2.1 for more information.

6.4.4 Assumptions.

The statistical tests described herein assume that the original qualification data comes from a normal distribution. Statistical tests on means are generally quite insensitive to the type of distribution, so deviation from normality for tests on means is usually acceptable. In other words, the test on means is robust in identifying a departure from a normal distribution. Recall that statistical tests for modulus values fall in this category. On the other hand, the statistical testing for strength properties requires both a test on mean and a test on minimum individual. The part which involves the test on means is also robust to departure from normal distribution based on the same argument. However, the part which involves minimum individual may be quite sensitive to departure from normal distribution. Violation of the normality assumption is likely to cause more materials to be rejected, which is a conservative situation. If an alternative probability model that more appropriately represents the data is available, the acceptance criteria described in this section may be substituted.

6.4.5 Generating a New Material Qualification Database.

The material equivalence procedures outlined above may lead to the generation of a new material qualification database. If several properties fail the material equivalence criteria, one may decide to repeat the entire material equivalence test matrix rather than repeating only the tests that failed the criteria. If the second round of material equivalence testing also yields unsatisfactory failures, the third round may incorporate other test conditions such as CTD and ETD to complete the reduced sampling test matrix in table 4. Successful completion of the remaining requirements in sections 4 and 5 will generate a new original material properties database.

6.4.6 Qualification of an Alternate Material.

Qualification of an alternate material refers to the situation where one material system from a single supplier has been qualified, and it is necessary or desirable to qualify an alternate material system or supplier. Although given in section 2.3.4 of MIL-HDBK-17-1E, the procedure for this subject is still under development by the MIL-HDBK-17 Working Group at the time of this publication. Readers are encouraged to refer to future revisions of MIL-HDBK-17 for developments related to this subject. Assuming an original qualification database exists for the alternate material, the material equivalence procedures of this document (sections 6.1 and 6.3) may be used as shown by the flowchart in figure 33.

The limitations delineated in section 6.1 do not allow the material equivalency methodology of this report to be applied directly to qualification of an alternate material system. However, the material equivalency procedures delineated in this report may be used to demonstrate equivalency to an alternate material system if an original database of the candidate for alternate material exists. If this approach is to be used, prior comparisons between the two original material databases must reveal that the two material systems are equal, or the alternate material is desirably superior to the existing material. An FAA representative(s) is typically involved in such decision-making processes which goes beyond material properties measured with coupons. Section 2.3.4 of MIL-HDBK-17-1E may be used as a guideline for this comparison. The material equivalence procedures in this report (sections 6.1 and 6.3) may be adapted to compare the degree of similarities between the two original databases. This determination of equivalency

only deals with lamina-level properties. Additional tests at higher levels (laminate, element, and subcomponent) are usually required to demonstrate acceptable equivalency between two material systems for design details representative of the intended application. These higher-level tests are required to validate equivalency for laminate and structural properties that quantify the effects of holes, bolted and bonded joints, impact damage, large notches, and critical design features.

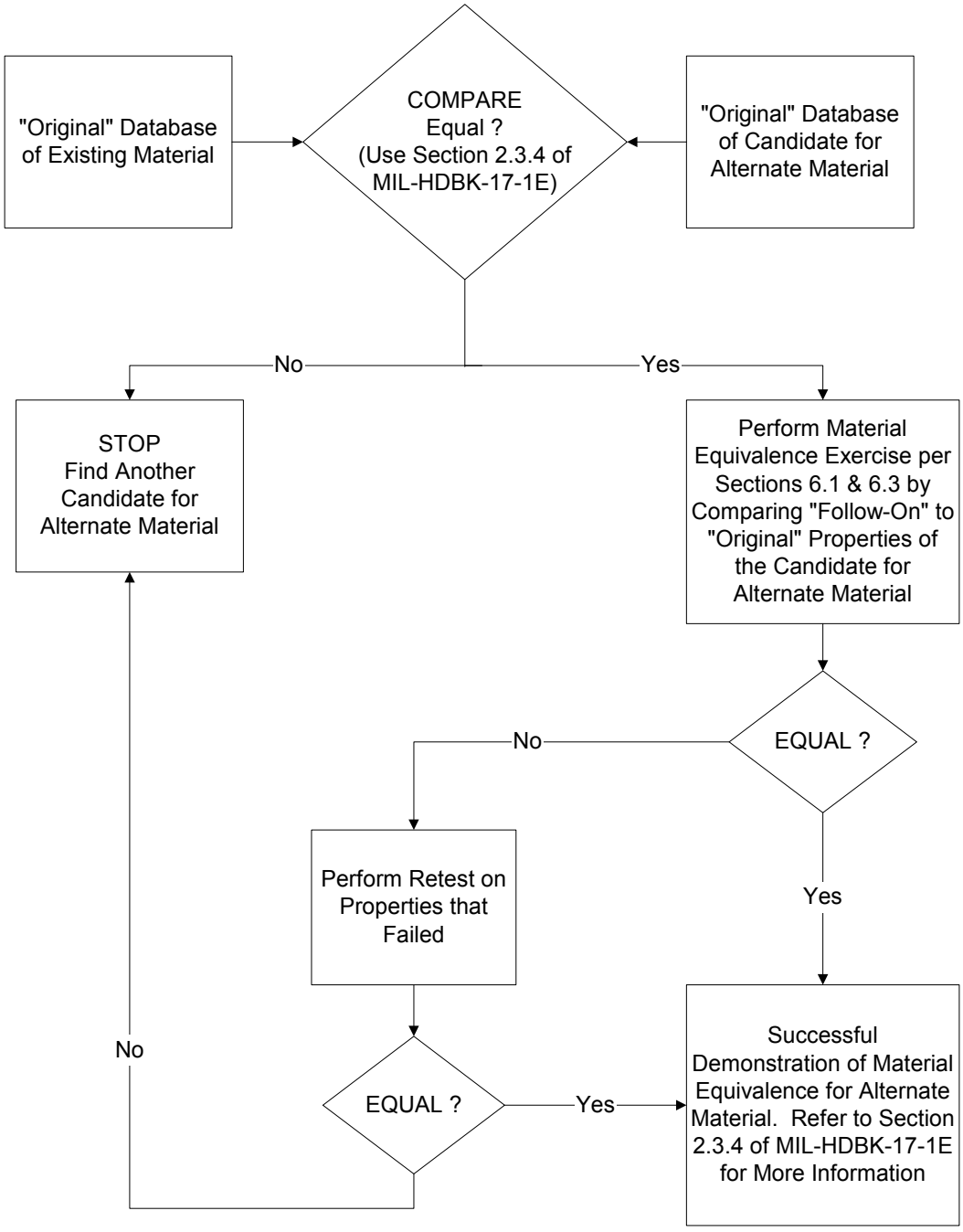


FIGURE 33. PROCEDURES FOR SELECTING AND DEMONSTRATING EQUIVALENCY FOR AN ALTERNATE MATERIAL

In general, the modulus values of the alternate and existing materials must be almost identical. The average strength properties of the alternate material should be equal or slightly higher than that of the existing material. The A- and B-basis properties of the alternate material should also be equal or slightly higher than the existing material. All material systems within the same material and process specification will share the same material design allowables (A-, B-basis, modulus, and Poisson's ratio). The prepreg lot acceptance thresholds and ranges should be based on the original qualification of individual material systems. All laminate, element, component, or full-scale tests should ensure adequate coverage for the lowest structural strengths.

7. CONCLUSIONS.

The qualification plan in this report documents engineering practices for base composite material qualification databases and equivalency testing. Equivalence testing demonstrates that a given material processed by a new user can achieve the properties documented in the original database. This qualification plan provides a good starting point for protocol needed to share composite databases between multiple users. The practice of shared databases is routinely used within the metals industry for numerous materials used in aircraft products (e.g., aluminum alloys). To achieve the same status for composites, the accepted engineering practices must take into account that a user processes the material to a finished state for a composite structure. As a result, equivalency testing is needed to ensure sufficient understanding of the materials and process controls behind a shared composite database. A number of other advances within the industry could further stabilize composite materials to support the engineering community in the safe and efficient deployment of composite materials to aircraft products. This section provides some recommendations in this area.

Well-defined material and process specifications are needed to support shared composite material databases. Such specifications should be documented and provided to all candidate users as a means of transferring the technology behind a given qualification database. This suggests a mechanism such as the SAE Aerospace Materials Specification process currently used for metallic materials used in aircraft products. Some composite materials have successfully pursued this path, but a more rigorous national or international effort is needed. A new working group within MIL-Handbook-17, called Data Utilization, is pursuing such a direction. Without the material and process insights, composite qualification databases have little benefit to new users. The specifications are also needed to ensure a high level of success in users demonstrating equivalency.

To evolve consistent and mature specifications, composite materials and processes must be rigorously studied to identify the key characteristics that will ensure invariance over time. Concerns over changes in the raw material processes traditionally led to a need for multiple batches used in original material qualification, as well as continuous monitoring by receiving inspections currently used by the industry. Both the upper and lower bounds of properties need to be more closely controlled to avoid issues of property drift over time. A more complete assessment of the final composite processing parameters is also needed. For example, the effects of composite processing windows should be incorporated into the supporting databases. The current engineering practices documented in this report have made some advances in this direction by including multiple process runs as a variable in the qualification database.

However, more rigorous assessment of the complete processing space may be needed to capture the full variation in properties allowed within the specifications.

Additional levels of building block tests are also candidates for shared databases. To be useful for a wide range of applications, shared databases should be limited to information that is non-product-specific. Such data might include some standard joints and notched material testing that can be helpful in design. Some data on the effects of defects and damage would also serve multiple users. Similarly, the basic data used for the repair of a composite material would help smaller users who are in dire need of such shared databases. Not only would the higher levels of building block data provide engineering efficiency through shared databases, but it would promote its use in controlling material and process invariance over time. Such a practice is currently not routinely followed within the industry (i.e., tests used to control material and processes often do not include some of the higher-level data thought to be essential to structural applications).

In summary, the qualification plan, material database, and equivalency to the original database presented in this report is the first step in development of shared databases. Higher-level tests and databases will be needed for complete interchange of data and its usefulness in the design and manufacturing process.

8. REFERENCES.

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3. McCarvill, W., Ward, S., Bogucki, G., Tomblin, J., "Guidelines and Recommended Criteria for the Development of A Material Specification for Carbon Fiber/Epoxy Unidirectional Prepreg," FAA report DOT/FAA/AR-02/109, March 2003.

4. Shyprykevich, P., "The Role of Statistical Data Reduction in the Development of Design Allowables for Composites," *Test Methods for Design Allowables for Fibrous Composites: 2nd Volume, ASTM STP 1003,* C.C. Chamis, ed., American Society for Testing and Materials, Philadelphia, PA, 1989, pp. 111-135.

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6. Scholz, F. W. and Stephens, M. A., "*K*-Sample Anderson-Darling Tests," Journal of the American Statistical Association, September 1987, Vol. 82, No. 399, Theory and Methods.

7. Vangel M. G., "Lot Acceptance and Compliance Testing Using the Sample Mean and An Extremum," *Technometrics*, 2002; 44:242-249.

9. GLOSSARY.

A-Basis—95% lower confidence limit on the first population percentile.

Acceptance Testing—The testing of incoming material to ensure that it meets requirements.

B-Basis—95% lower confidence limit on the tenth population percentile.

Follow-on—The applicant, material, process, or testing of material equivalence or acceptance testing.

Material Equivalence—The testing of a material to ensure that the follow-on applicant, material, or process will produce material properties equal to those of original material qualification/ certification.

Prepreg Batch—A production run of prepreg material that is preimpregnated using one batch of resin and fiber form under one set of operating conditions. Scheduled interruptions (e.g., overnight plant shutdowns) or short maintenance downtimes in the production run to create material in this batch are permitted, provided there is no interim run. When defined in a material qualification program, no fiber or resin lot duplication is allowed in any two prepreg batches.

Prepreg Lot—One batch of prepreg material or a portion of one batch that is shipped to a purchaser for acceptance at one time. Scheduled interruptions (e.g., overnight plant shutdowns) or short maintenance downtimes in the production run to create material in this lot are permitted, provided there is no interim run.

Reduced Sampling—Specimen sampling technique that requires three prepreg batches.

Robust Sampling—Specimen sampling technique that requires five prepreg batches.

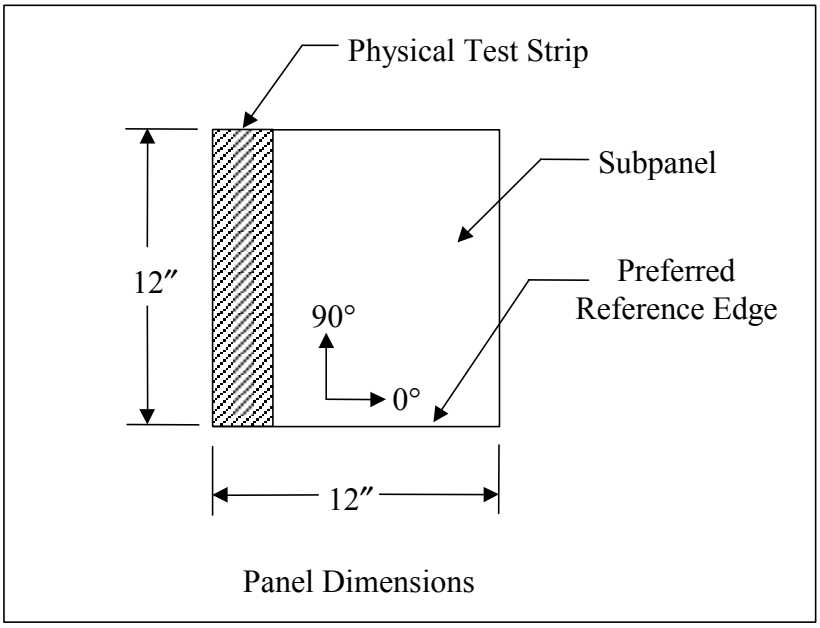
APPENDIX A—ROBUST SAMPLING PANEL REQUIREMENTS

ASTM D 3039-95—0^{o} Unidirectional Tape Tensile Strength, Modulus, and Poisson's Ratio

For robust sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength, Modulus, and Poisson's Ratio	5 x 11	5 x 11	5 x 11	5 x 11

Recommended panel size:



Panel Dimensions

Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.040″
Required Thickness: 0.035″ - 0.060″

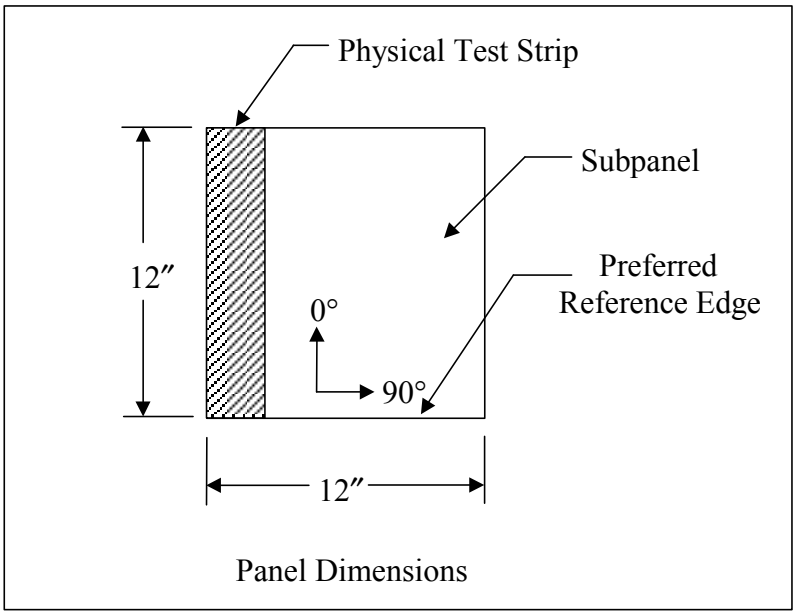
Minimum Number of Panels per Batch: 5
Number of Subpanels per Panel: 1

ASTM D 3039-95—90° Unidirectional Tape Tensile Strength and Modulus

For robust sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength and Modulus	5 x 11	5 x 11	5 x 11	5 x 11

Recommended panel size:



Panel Dimensions

Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.100″
Required Thickness: 0.090″ - 0.120″

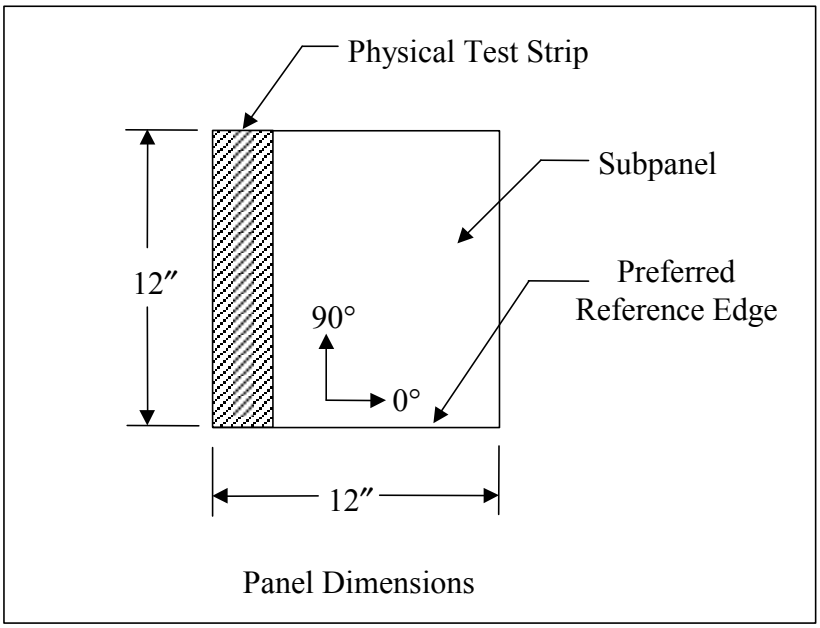
Minimum Number of Panels per Batch: 8
Number of Subpanels per Panel: 1

ASTM D 3039-95—0^{o} (warp) Fabric Tensile Strength, Modulus, and Poisson's Ratio

For robust sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength, Modulus, and Poisson's Ratio	5 x 11	5 x 11	5 x 11	5 x 11

Recommended panel size:



Panel Dimensions

Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.100″
Required Thickness: 0.090″ - 0.120″

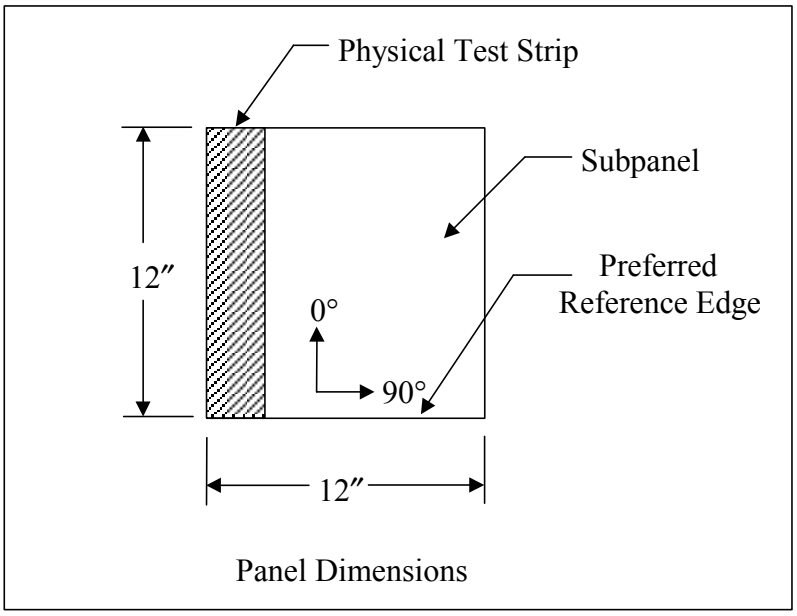
Minimum Number of Panels: 8
Number of Subpanels per Panel: 1

ASTM D 3039-95—90° (fill) Fabric Tensile Strength, Modulus, and Poisson's Ratio

For robust sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength, Modulus, and Poisson's Ratio	5 x 11	5 x 11	5 x 11	5 x 11

Recommended panel size:



Panel Dimensions

Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.100″
Required Thickness: 0.090″ - 0.120″

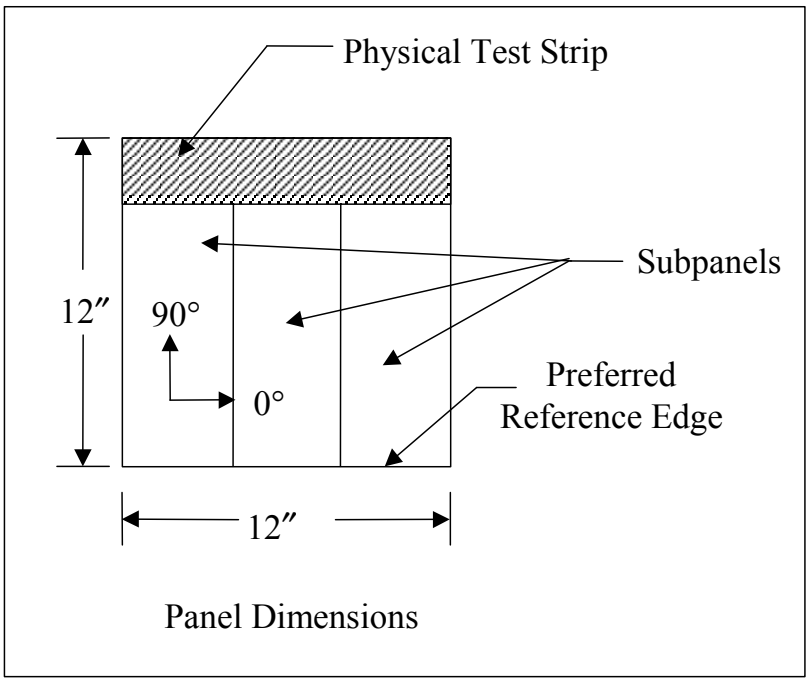
Minimum Number of Panels per Batch: 8
Number of Subpanels per Panel: 1

SACMA SRM 1-94—0^{o} Unidirectional Tape Compressive Strength and Modulus

For robust sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength	5 x 11	5 x 11	5 x 11	5 x 11
Modulus	5 x 11	5 x 11	5 x 11	5 x 11

Recommended Panel Size:



Panel Dimensions

Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.040″
Required Thickness: 0.035″ - 0.050″

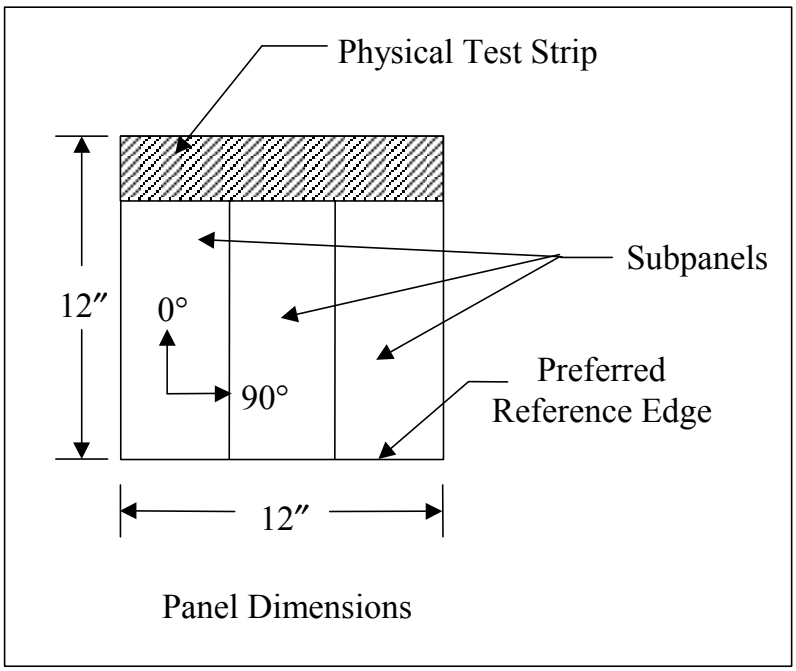
Minimum Number of Panels per Batch: 4
Number of Subpanels per Panel: 3

SACMA SRM 1-94—90° Unidirectional Tape Compressive Strength and Modulus

For robust sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength	5 x 11	5 x 11	5 x 11	5 x 11
Modulus	5 x 11	5 x 11	5 x 11	5 x 11

Recommended Panel Size:



Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.100″
Required Thickness: 0.090″ - 0.120″

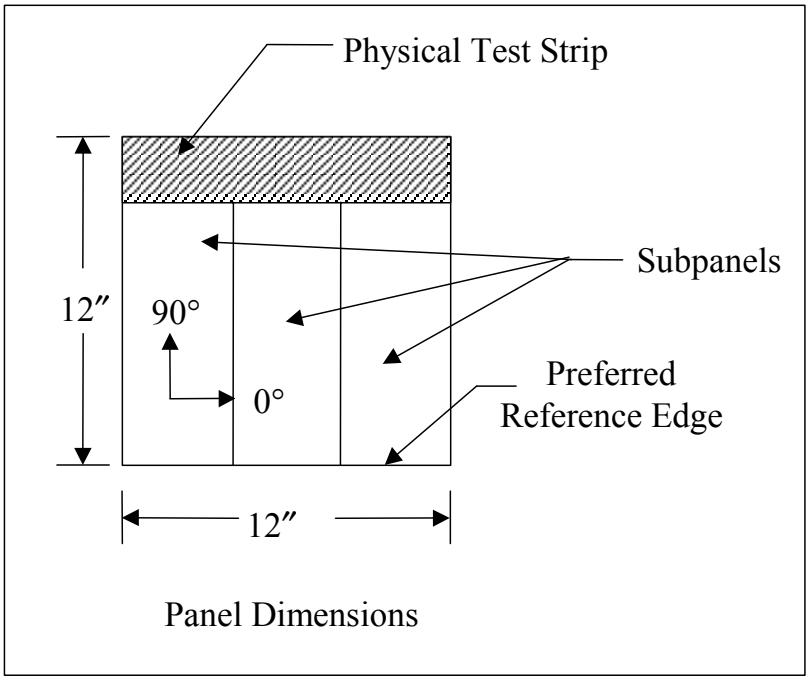
Minimum Number of Panels per Batch: 4
Number of Subpanels per Panel: 3

SACMA SRM 1-94—0^{o} (warp) Fabric Compressive Strength and Modulus

For robust sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength	5 x 11	5 x 11	5 x 11	5 x 11
Modulus	5 x 11	5 x 11	5 x 11	5 x 11

Recommended Panel Size:



Panel Dimensions

Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.120″
Required Thickness: 0.100″ - 0.140″

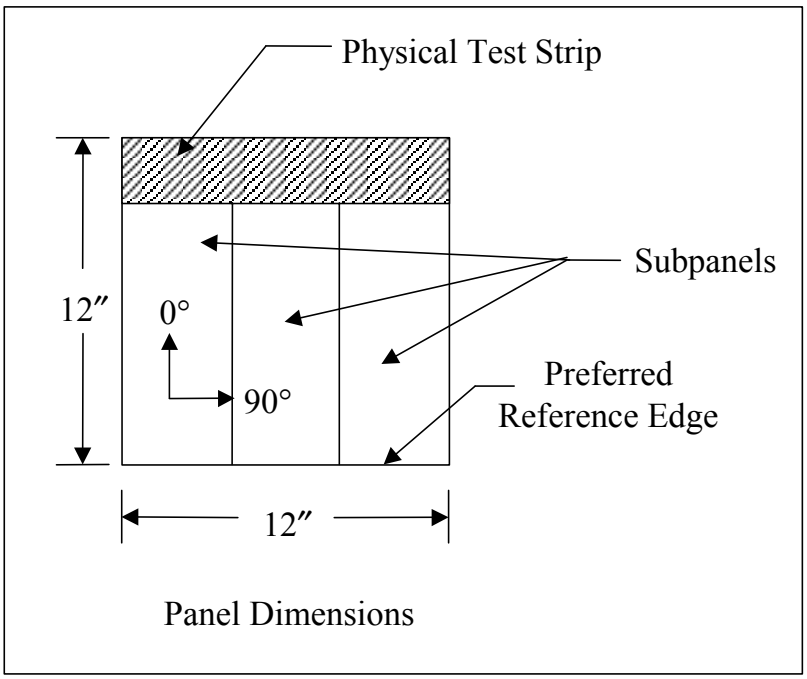
Minimum Number of Panels per Batch: 4
Number of Subpanels per Panel: 3

SACMA SRM 1-94—90° (fill) Fabric Compressive Strength and Modulus

For robust sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength	5 x 11	5 x 11	5 x 11	5 x 11
Modulus	5 x 11	5 x 11	5 x 11	5 x 11

Recommended Panel Size:



Panel Dimensions

Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.120″
Required Thickness: 0.100″ - 0.140″

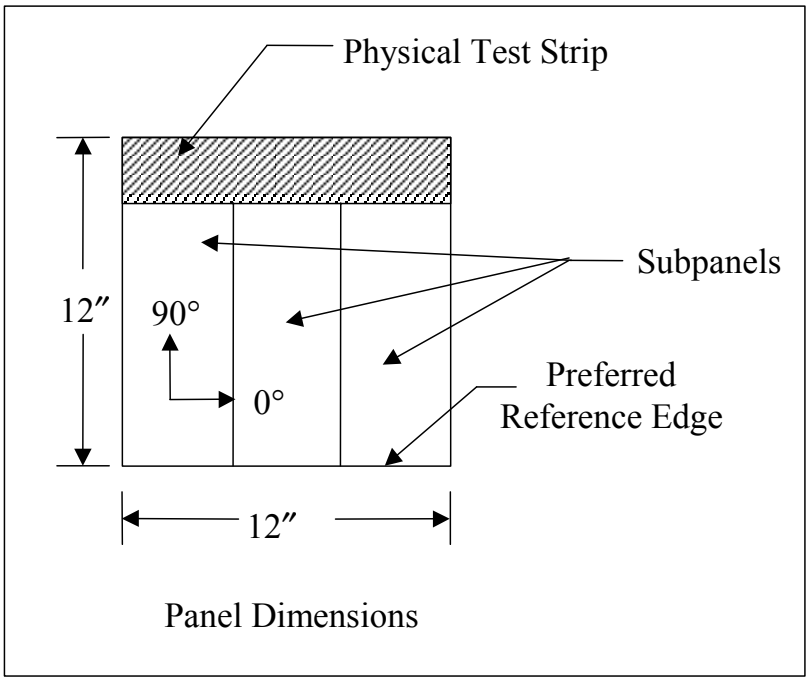
Minimum Number of Panels per Batch: 4
Number of Subpanels per Panel: 3

ASTM D 5379-93—In-Plane Shear Strength and Modulus (Unidirectional Tape and Fabric)

For robust sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength and Modulus	5 x 11	5 x 11	5 x 11	5 x 11

Recommended Panel Size:



Lay-Up Configuration: $[0/90]_{ns}$ with a recommended thickness of 0.140″
Required Thickness: 0.120″ - 0.160″

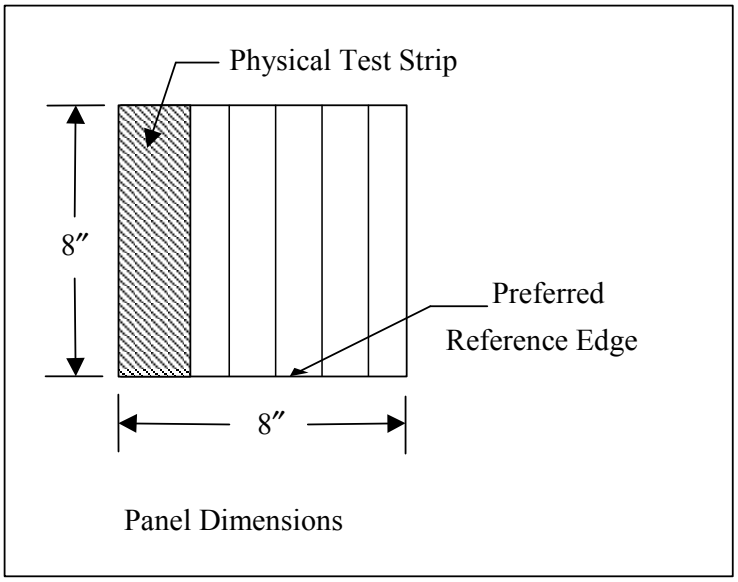
Minimum Number of Panels per Batch: 4
Number of Subpanels per Panel: 3

ASTM D 2344-89 or SACMA SRM 8-94—Short-Beam Shear Strength (Unidirectional Tape and Fabric)

For robust sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength		5 x 11		

Recommended Panel Size:



Panel Dimensions

Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.100″
Required Thickness: 0.080″ - 0.120″

Minimum Number of Panels per batch: 2
Number of Subpanels per Panel: 5

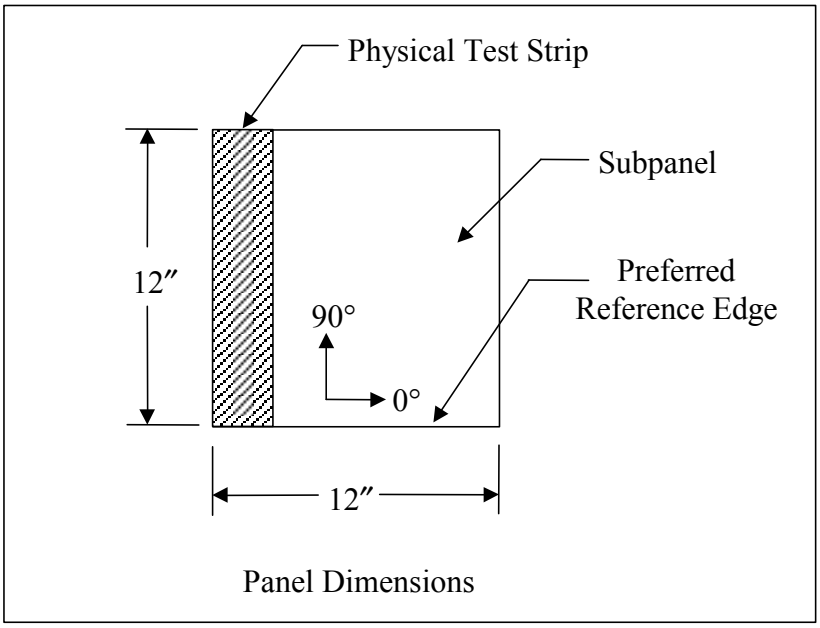
APPENDIX B—REDUCED SAMPLING PANEL REQUIREMENTS

ASTM D 3039-95—0^{o} Unidirectional Tape Tensile Strength, Modulus, and Poisson's Ratio

For reduced sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength, Modulus, and Poisson's Ratio	3 x 6	3 x 6	3 x 6	3 x 6

Recommended panel size:



Panel Dimensions

Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.04″
Required thickness: 0.035″ - 0.060″

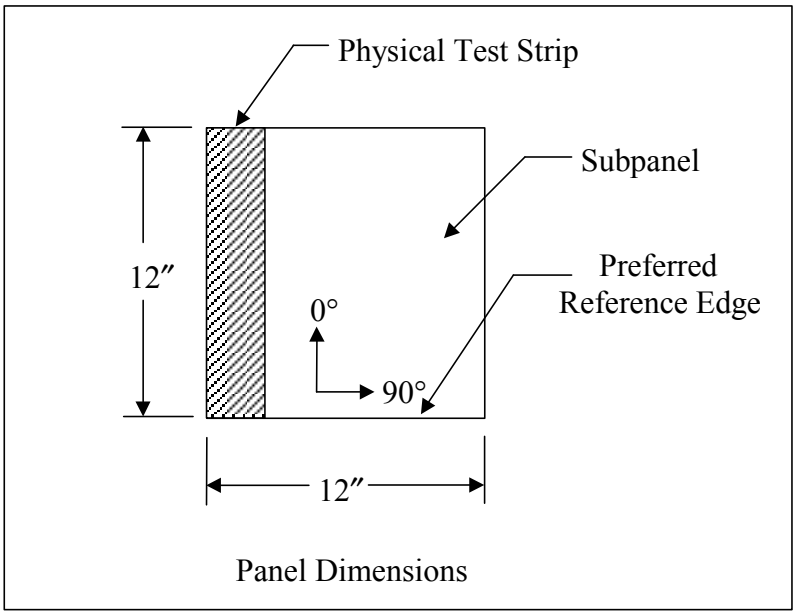
Minimum Number of Panels per Batch: 4
Number of Subpanels per Panel: 1

ASTM D 3039-95—90° Unidirectional Tape Tensile Strength and Modulus

For reduced sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength and Modulus	3 x 6	3 x 6	3 x 6	3 x 6

Recommended panel size:



Panel Dimensions

Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.100″
Required thickness: 0.090″ - 0.120″

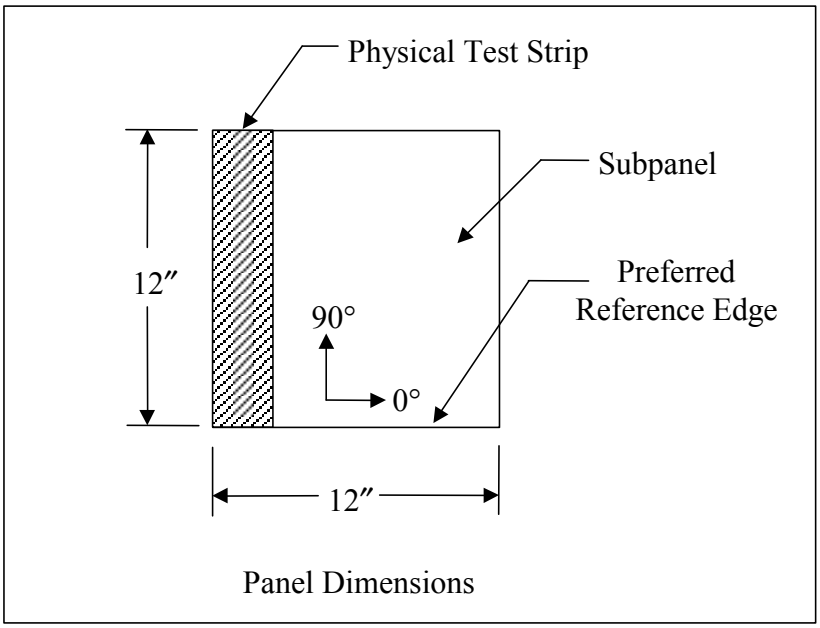
Minimum Number of Panels per Batch: 5
Number of Subpanels per Panel: 1

ASTM D 3039-95—0^{o} (warp) Fabric Tensile Strength, Modulus, and Poisson's Ratio

For reduced sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength, Modulus, and Poisson's Ratio	3 x 6	3 x 6	3 x 6	3 x 6

Recommended panel size:



Panel Dimensions

Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.100″
Required Thickness: 0.090″ - 0.120″

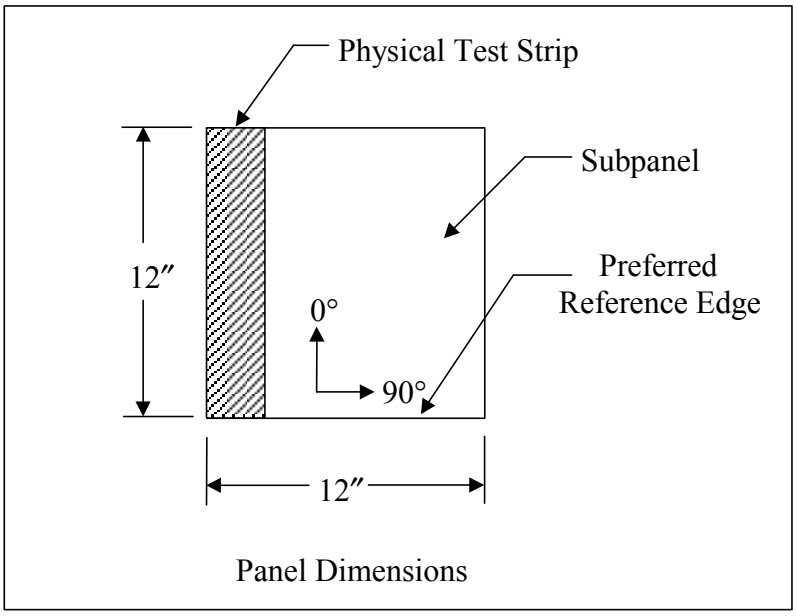
Minimum Number of Panels per Batch: 5
Number of Subpanels per Panel: 1

ASTM D 3039-95—90° (fill) Fabric Tensile Strength, Modulus, and Poisson's Ratio

For reduced sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength, Modulus, and Poisson's Ratio	3 x 6	3 x 6	3 x 6	3 x 6

Recommended panel size:



Panel Dimensions

Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.100″
Required Thickness: 0.090″ - 0.120″

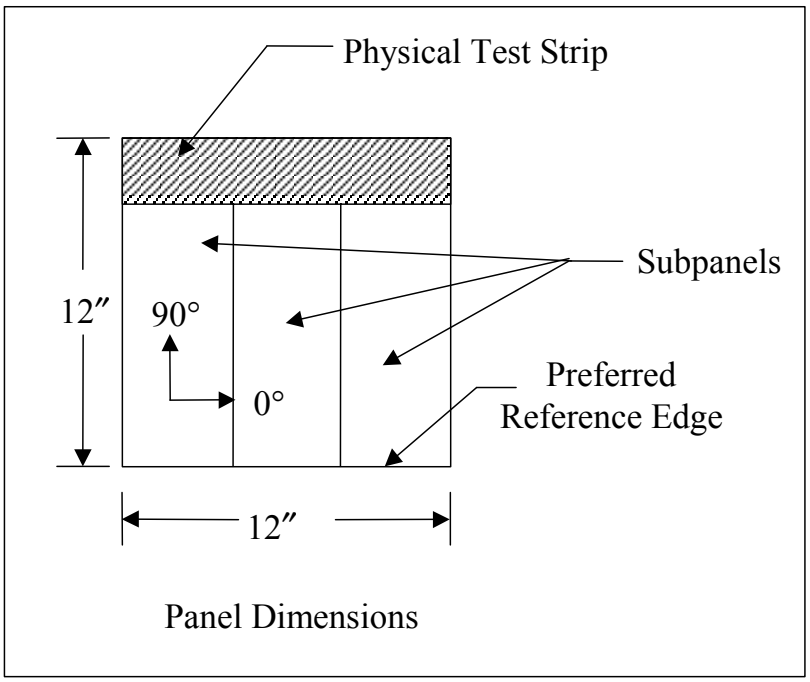
Minimum Number of Panels per Batch: 5
Number of Subpanels per Panel: 1

SACMA SRM 1-94—0° Unidirectional Tape Compressive Strength and Modulus

For reduced sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength	3 x 6	3 x 6	3 x 6	3 x 6
Modulus	3 x 6	3 x 6	3 x 6	3 x 6

Recommended Panel Size:



Panel Dimensions

Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.040″
Required Thickness: 0.035″ - 0.050″

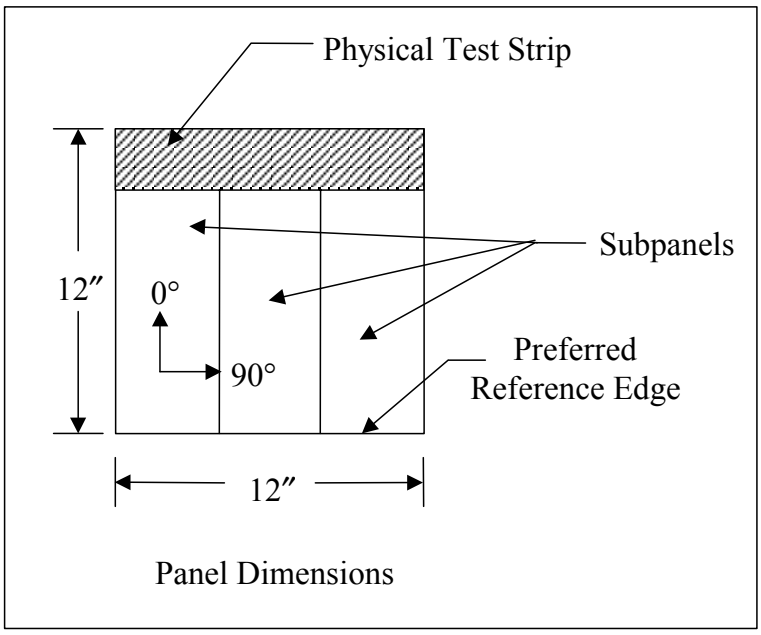
Minimum Number of Panels per Batch: 4
Number of Subpanels per Panel: 3

SACMA SRM 1-94—90° Unidirectional Tape Compressive Strength and Modulus

For reduced sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength	3 x 6	3 x 6	3 x 6	3 x 6
Modulus	3 x 6	3 x 6	3 x 6	3 x 6

Recommended Panel Size:



Panel Dimensions

Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.040″
Required Thickness: 0.035″ - 0.050″

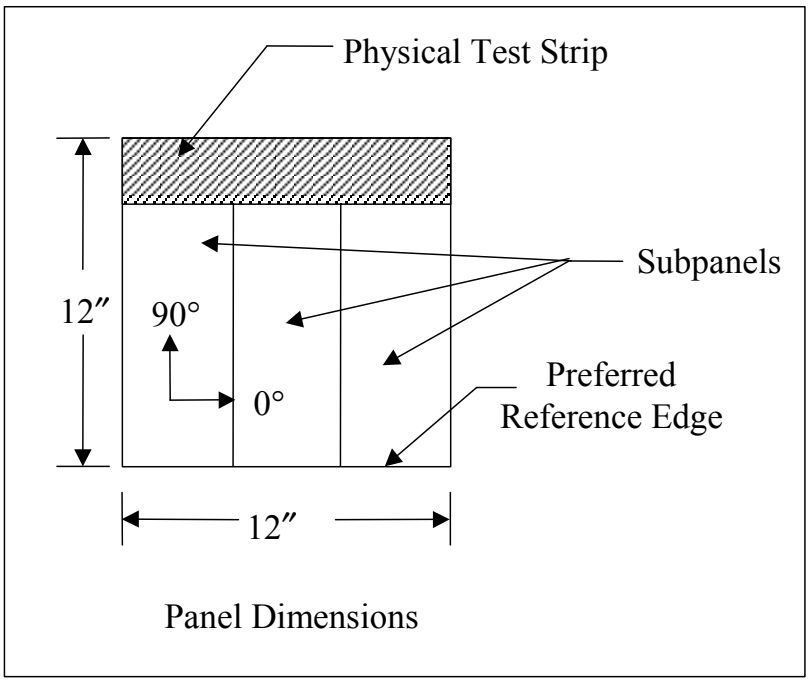
Minimum Number of Panels per Batch: 4
Number of Subpanels per Panel: 3

SACMA SRM 1-94—0° (warp) Fabric Compressive Strength and Modulus

For reduced sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength	3 x 6	3 x 6	3 x 6	3 x 6
Modulus	3 x 6	3 x 6	3 x 6	3 x 6

Recommended Panel Size:



Panel Dimensions

Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.120″
Required Thickness: 0.100″ - 0.140″

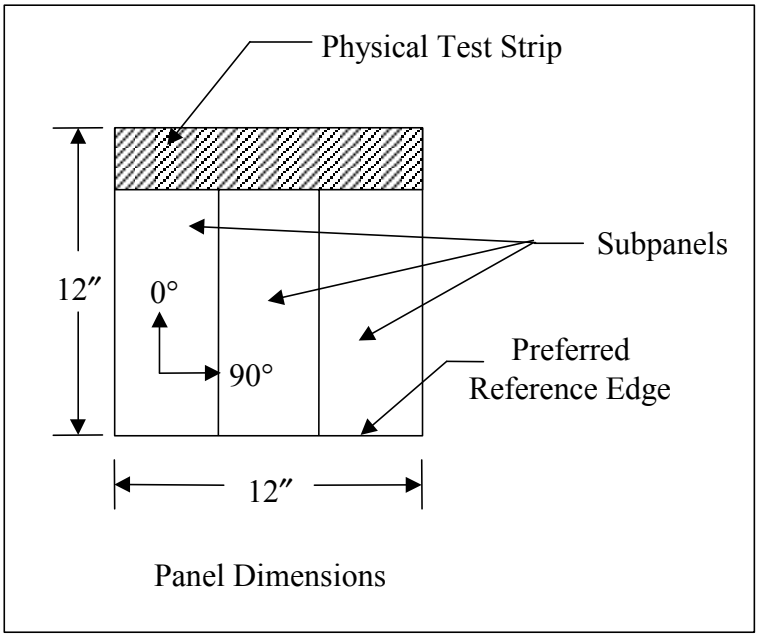
Minimum Number of Panels per Batch: 4
Number of Subpanels per Panel: 3

SACMA SRM 1-94—90° (fill) Fabric Compressive Strength and Modulus

For reduced sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength	3 x 6	3 x 6	3 x 6	3 x 6
Modulus	3 x 6	3 x 6	3 x 6	3 x 6

Recommended Panel Size:



Panel Dimensions

Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.120″
Required Thickness: 0.100″ - 0.140″

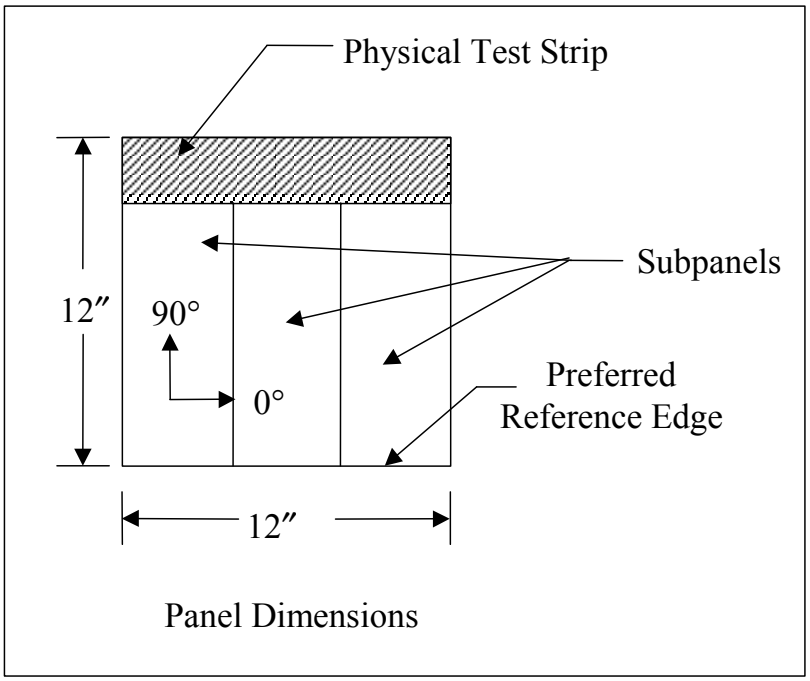
Minimum Number of Panels per Batch: 4
Number of Subpanels per Panel: 3

ASTM D 5379-93—In-Plane Shear Strength and Modulus (Unidirectional Tape and Fabric)

For reduced sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength and Modulus	3 x 6	3 x 6	3 x 6	3 x 6

Recommended Panel Size:



Panel Dimensions

Lay-Up Configuration: $[0/90]_{ns}$ with a recommended thickness of 0.140″
Required Thickness: 0.120″ - 0.160″

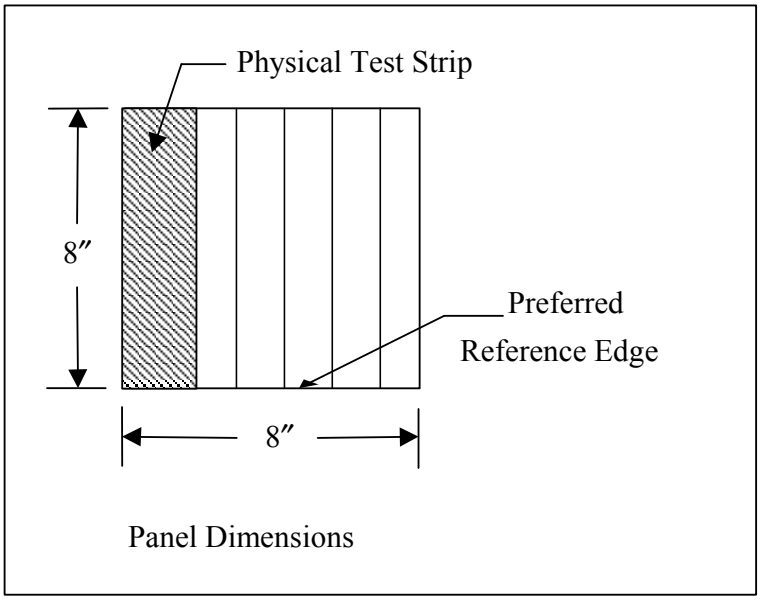
Minimum Number of Panels per Batch: 2
Number of Subpanels per Panel: 3

ASTM D 2344-89 or SACMA SRM 8-94—Short-Beam Shear Strength (Unidirectional Tape and Fabric)

For reduced sampling, the required specimens are:

	CTD	RTD	ETW	ETD
Strength		3 x 6		

Recommended Panel Size:



Panel Dimensions

Lay-Up Configuration: $[0]_n$ with a recommended thickness of 0.100″
Required Thickness: 0.080″ - 0.120″

Minimum Number of Panels per batch: 2
Number of Subpanels per Panel: 5

APPENDIX C—LAMINATE LAY-UP AND BAGGING GUIDE

This appendix provides guidelines for manufacturing panels of acceptable quality for mechanical, thermal, and physical tests described in this report. Figures C-1 and C-2 show two recommended bagging techniques. In the top views, air breather, TFE film (release or separator film), vacuum bag, and sealant are not shown. The plies should be cut such that the edges of the lamina are parallel/perpendicular to the warp or 0° direction. During the lay-up process, the edge of each ply of prepreg should be placed firmly against a straight metal edge dam, which has been coated with mold release agent and secured in place with tape. The metal edge dam is used to produce a straight reference edge on the panel. The reference edge will be used in machining and tabbing processes to maintain fiber orientation.

The other three edges of the laminate should be surrounded by a flexible-edge dam to prevent lateral resin bleed-out, as shown in figure C-1. The flexible-edge dam may be made of sealant tape or cured silicon. It is advisable to use a thick caul plate (1/5 inch or thicker aluminum) to prevent bending that would result in uneven laminate thickness near the edges.

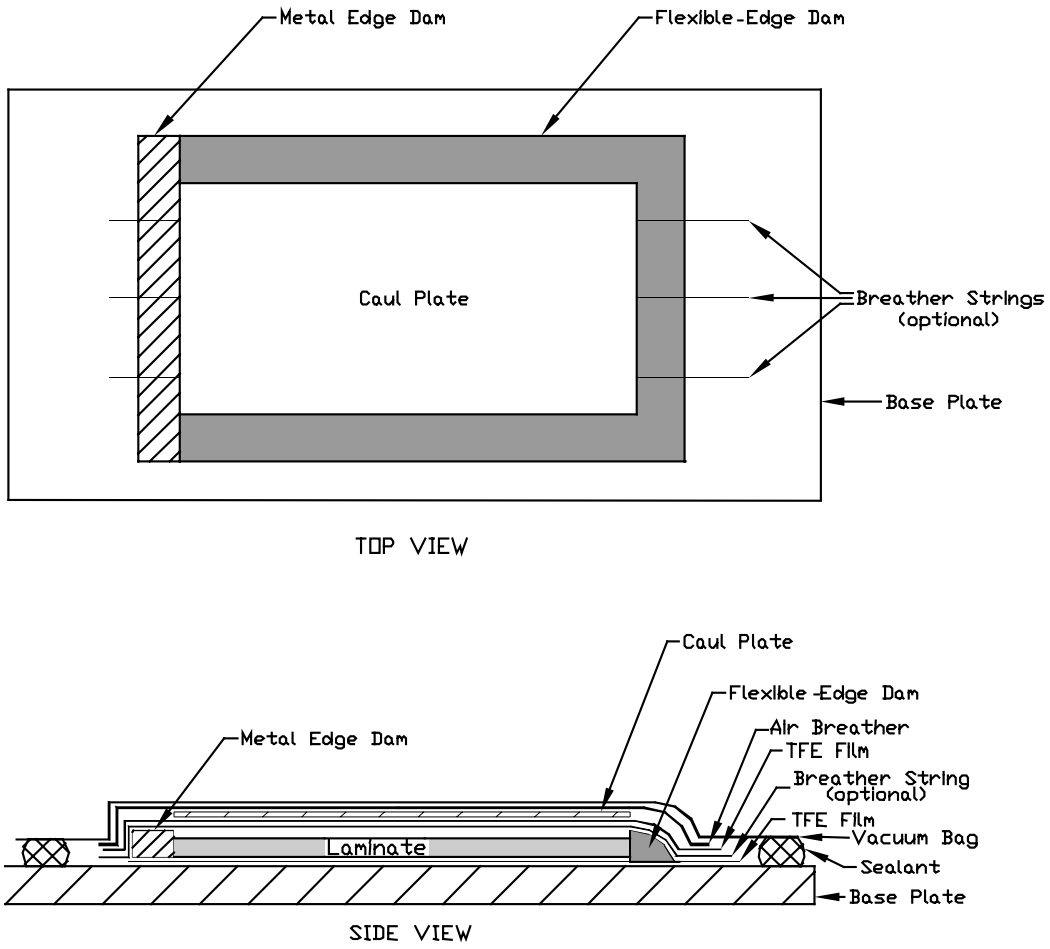


FIGURE C-1. RECOMMENDED LAY-UP TECHNIQUE (WITH FLEXIBLE-EDGE DAM)

Figure C-2 shows the caul plate with respect to the lay-up assembly. Note that the caul plate is smaller than the lay-up with approximately 1 inch of the lay-up exposed on three edges. If this technique is used, the panel size recommendations described in appendices A and B should be considered the caul plate size. The caul plate can be made of aluminum sheet as thin as 0.040 inch, since this technique is not prone to produce laminate with uneven thickness near the edges.

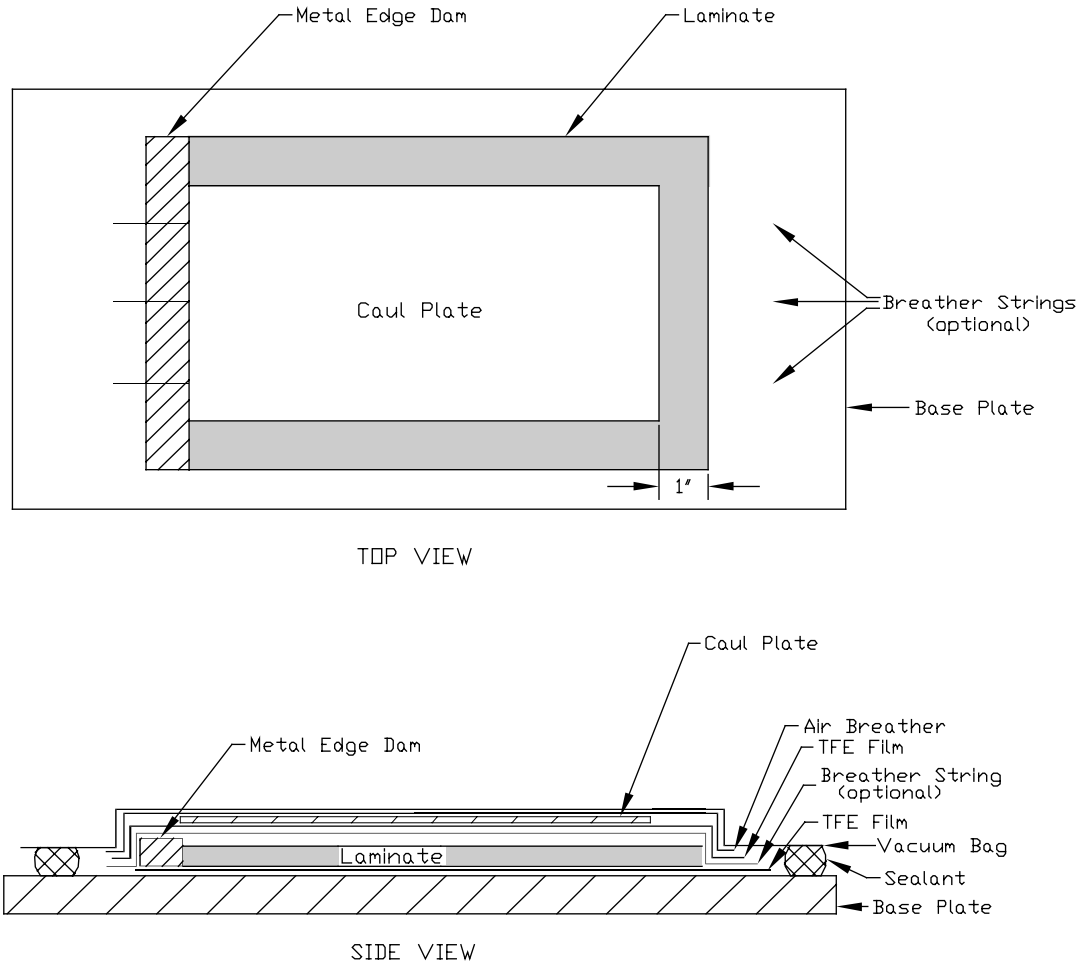


FIGURE C-2. RECOMMENDED LAY-UP TECHNIQUE (WITHOUT FLEXIBLE-EDGE DAM)

For fabrics without tracer yarns, the warp/fill direction should be clearly marked on the lay-up before the bagging process. Two methods of marking direction are:

1. Use an engraved caul plate to indicate the warp/fill direction.

2. Place a small piece of tape with indication of warp/fill direction. Make sure that the mark will remain visible after the curing process.

In either method, the direction marks should be placed on the laminate. It is also advisable to label the lay-up with its unique panel identification number or name as soon as the lay-up process is completed. The panel identification number or name should allow traceability to the prepreg name, prepreg lot number, cure or processing cycle number, test method, stacking sequence, and number of plies.

Extreme care should be used when laying up panels using satin weave fabrics (i.e., eight harness and 7781 style) due to the unsymmetrical nature of the weave pattern. See section 3.4.4.2 for more details.

The use of breather strings is optional. Breather strings, if used, should be limited to releasing the entrapped air only and should not be used for releasing volatiles from the prepreg. Note that breather strings will absorb resin, cause waviness in the fibers, and may affect the mechanical properties. For these reasons, breather strings, if used, should be as fine as possible. Fiberglass strands/ends of 1581 or 7781 style that have been pretreated with a release agent have been shown to be successful in releasing entrapped air without releasing volatiles and are quite easily removed after the curing process. The ends of breather strings should be in direct contact with the air breather in the vacuum bag. If breather strings are used on unidirectional lamina, they should be placed 90° to the fiber direction. Breather strings should be removed after the curing process. An alternate method to using breather strings is making tiny holes (perforations) in the TFE film along the edges of the lay-up/laminate.

The use of release fabric must be avoided. The use of peel ply is also discouraged. See section 3.1 for more details.

Vacuum ports should not be placed on the laminate unless the caul plate is rigid enough to avoid marking the laminate.

Thermocouple wires should be used to measure the laminate temperature. There are two methods of installation: (1) place the thermocouple junctions at the mid-plane and near the edge of the laminate, where they will be trimmed off after the panels have been cured and (2) place the thermocouple junctions in between the air breather and caul plate and at the center of the laminate, but this method requires the caul plate to be very thin and have good thermal conductivity (such as a 0.040-inch-thick aluminum sheet). The latter method allows the thermocouple wires to be reused.